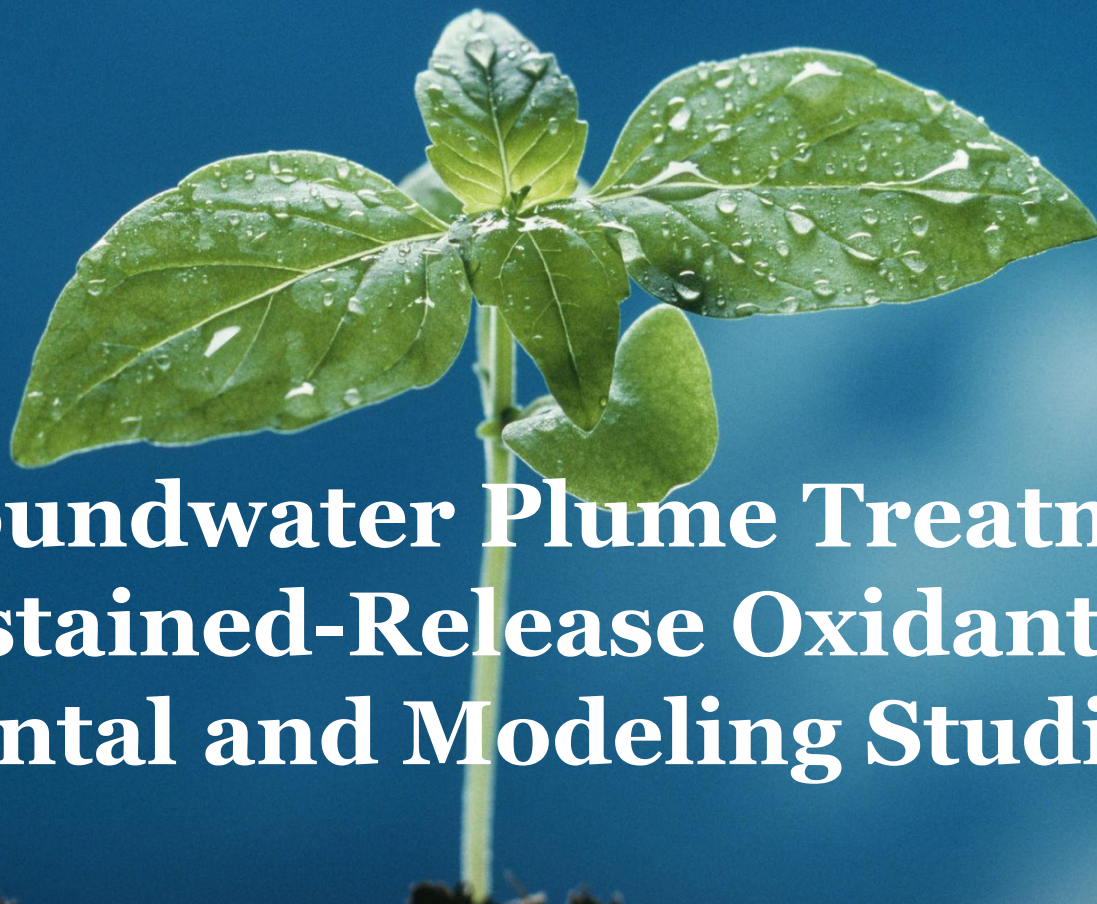


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Passive Groundwater Plume Treatment using Sustained-Release Oxidants: Experimental and Modeling Studies

Pamela J Dugan, Ph.D





Agenda

- Technology Description
- Laboratory Experiments
- Pilot-Scale Studies
- Design Tool Development
- Conclusions/Questions

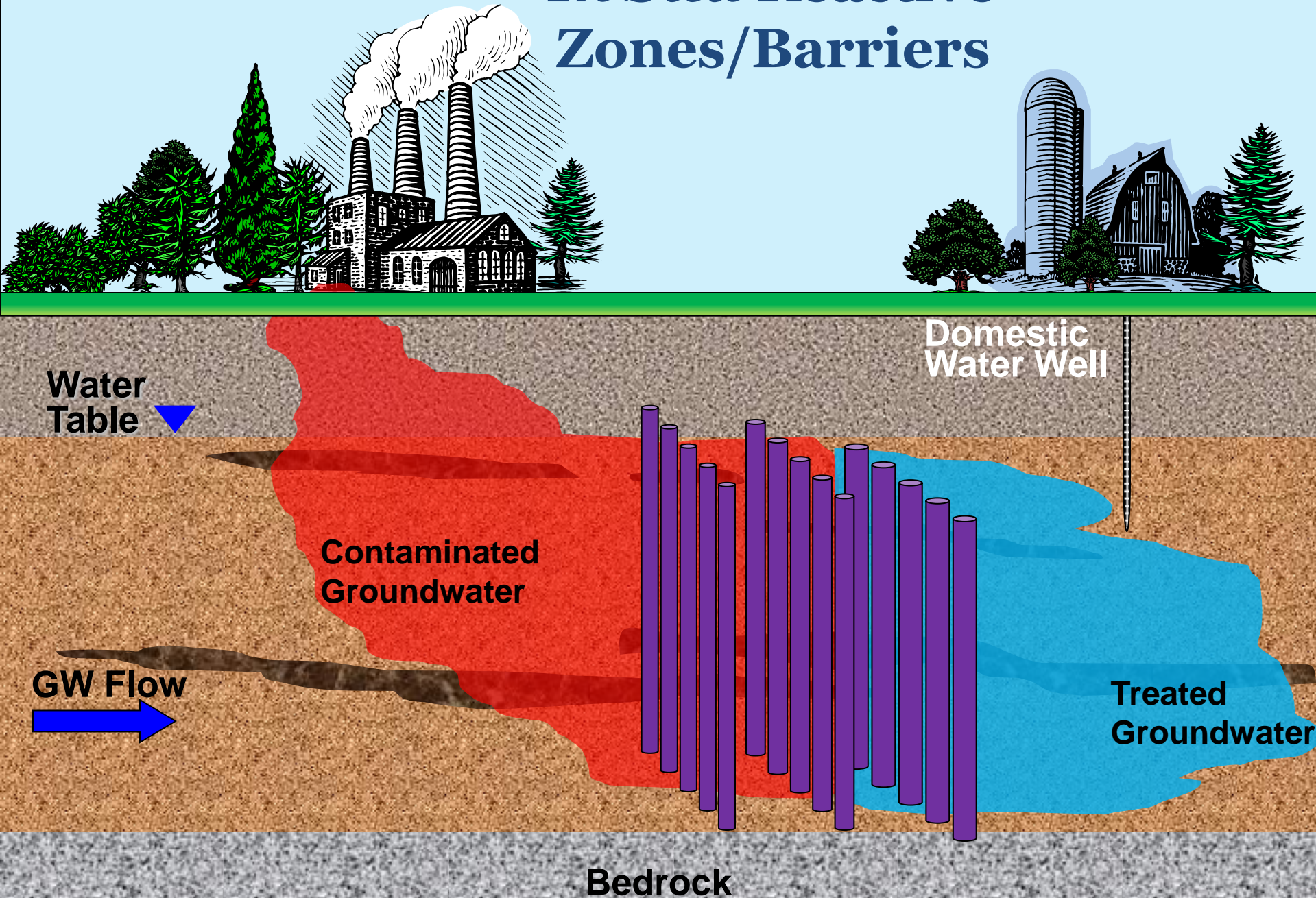


The Challenge...

- All remedial technologies have an impact...
 - Electricity/fossil fuel to power equipment
 - Aboveground treatment of extracted fluids
 - Site disruption/landfill disposal
- Reactive materials used successfully to remove contaminants in soil and groundwater
 - Do not require continued supply of electrical/fossil fuel energies
 - Serve as long-term, low-cost passive treatment



In Situ Reactive Zones/Barriers



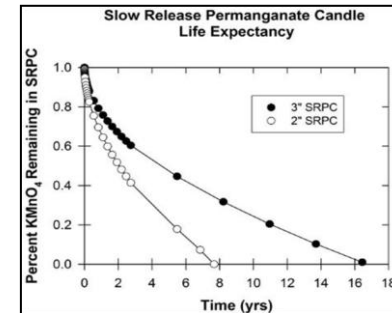
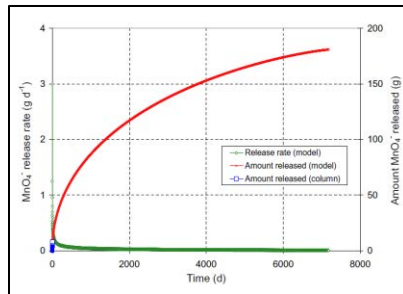
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Technology Development – Sustained-Release (SR) Oxidants

- Promising slow-release permanganate modeling, lab, pilot-scale field studies (e.g., Ohio State University, Clemson, University of Nebraska)

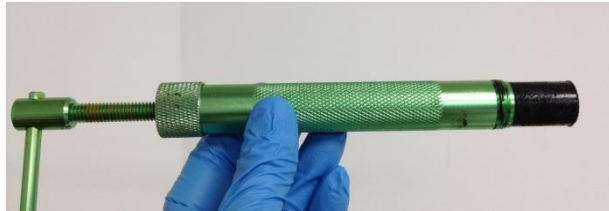


- 2003 Specialty Earth Sciences-patented methods of encapsulation for sustained-release of reactants
- Variety of reactive materials are possible
 - Oxidants, bio-amendments, oxygen release compounds, activators, chelating agents



Technology Development – Sustained-Release Oxidants

- Sustained-release permanganate is a KMnO_4 -based product dispersed in a solid paraffin wax matrix (~80% w/w)



- Sustained-release persulfate is a NaS_2O_8 -based product dispersed in a solid paraffin wax matrix (50-80% w/w)



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SR Technology - Versatility in Form

- Solid product formed as cylinder, chipped for trench/barrier applications or small pellets (1-2 mm) for hydro-fracturing into low permeability media/fractured bedrock
 - 1.35 or 2.5 inch diameter
 - 3.4 cm/6.4 cm
 - 18 inches long (46 cm)
 - DPT emplacement or well installation



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Direct Push Installation

- Direct push installation - 2.25 or 3.25 inch tooling and disposable tip
- Lowering cylinders within inner space of rods provides confirmation that cylinder placed at desired depth
- Rods retracted with cylinders remaining in place within the formation





In-Well “Cylinder Holders”



- Cylinders within stainless steel or plastic mesh candle holders secured to flush mount cover with stainless steel wire and clamp
- Cylinders can be removed and weighed for relative comparison against baseline measurements



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SR Technology - Versatility in Treatment of Contaminants

- Applicable to contaminants oxidized by permanganate (Lee and Schwartz, 2007; Christenson et al., 2012)
- Applicable to contaminants oxidized by persulfate (Kambhu et.al., 2012)
- Emerging contaminants (e.g., 1,4-dioxane)
- Can be applied in tandem or following ISCO or other remedial treatments to mitigate back-diffusion and contaminant desorption

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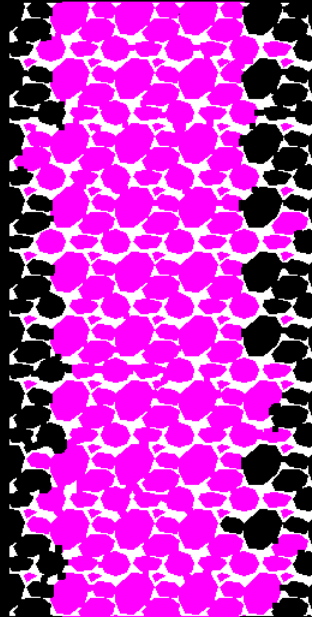


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Conceptual Model for Oxidant Release from Paraffin Wax Matrix



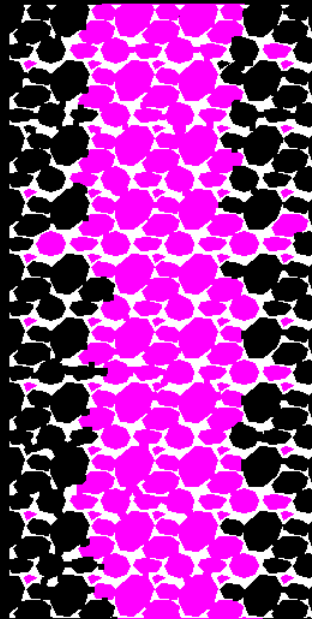
MnO_4^- Release from Wax



- As permanganate solids dissolve void spaces are created



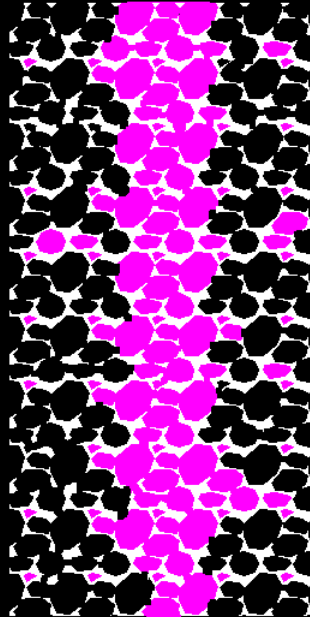
MnO_4^- Release from Wax



- Newly created void spaces expose permanganate solids for dissolution and diffusion
- Process occurs radially from the exterior of the cylinder to the inner core



MnO_4^- Release from Wax



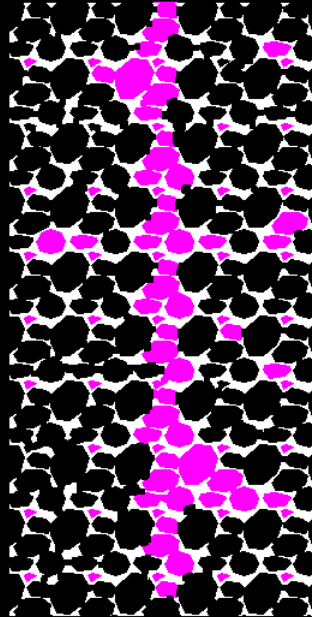
- As permanganate releases/reacts, porosity develops inward to the core of the cylinder
- Diffuses across a greater distance

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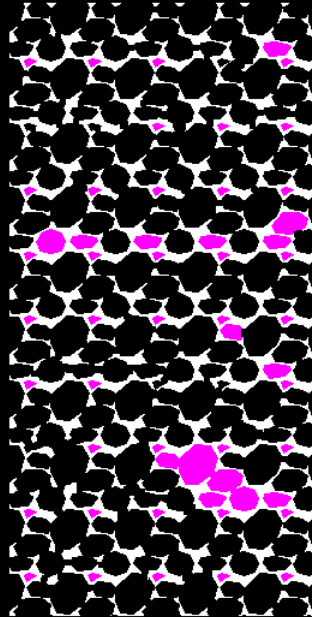
MnO_4^- Release from Wax



- This is why we see an initial spike of permanganate in early time...



MnO_4^- Release from Wax

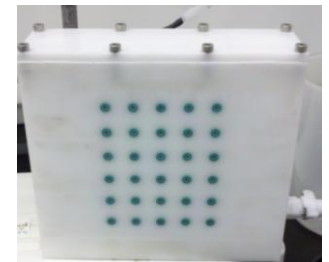
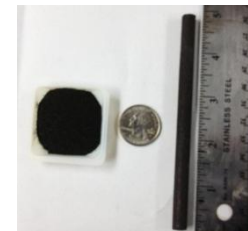
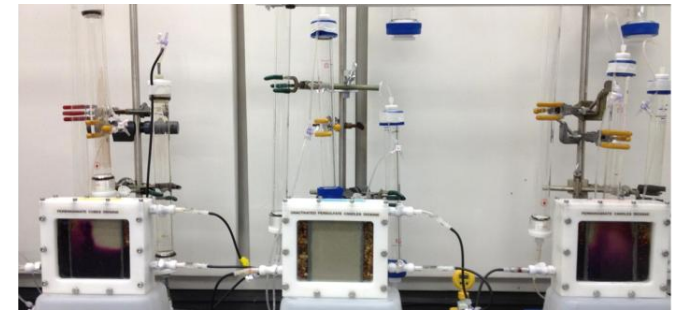
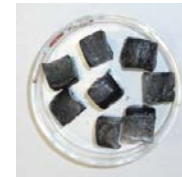


- And a significantly slower and lower release of permanganate at later times



Experimental Approach – 1-D Columns and 2-D Mini-Tanks

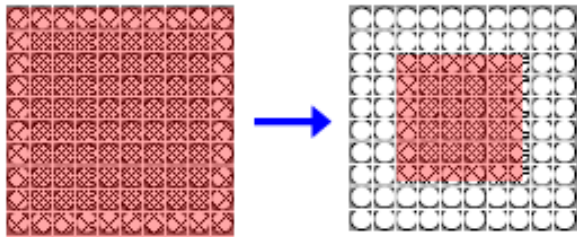
- Columns (30 or 60 cm x 4.8 cm)
 - Cubed material (TCE 0.7-1.5 ppm)
 - **1.35 inch diameter/1 inch long**
 - **2.5 inch diameter/1 inch long**
 - Flow rate (0.6 mL/min), 2 ft/day
- 2-D mini-tanks (14 x 14 x 2.5 cm)
 - 0.27 inch diameter/5 inch long (DI)
 - Permanganate or persulfate mini-cylinders (**10 grams of oxidant**)
- Purpose: evaluate oxidant release from SR material (cylinders, cubed, pellets), spatial distribution, and oxidative treatment of contaminants





Approach - Sustained-Release Design Tool

- Collect oxidant release rates to support modeling of releases from cylinders, cubes, pellets/pastilles
 - Model adapted after Lee and Schwartz (2007)



Lee and Schwartz, 2007

$$Q = \pi h A (r_o^2 - r^2)$$

$$\frac{r^2}{2} \ln \frac{r}{r_o} + \frac{1}{4} (r_o^2 - r^2) = \frac{C_s D_e t}{A}$$

$$D_{et} = \frac{D_e (t-1)}{T}$$

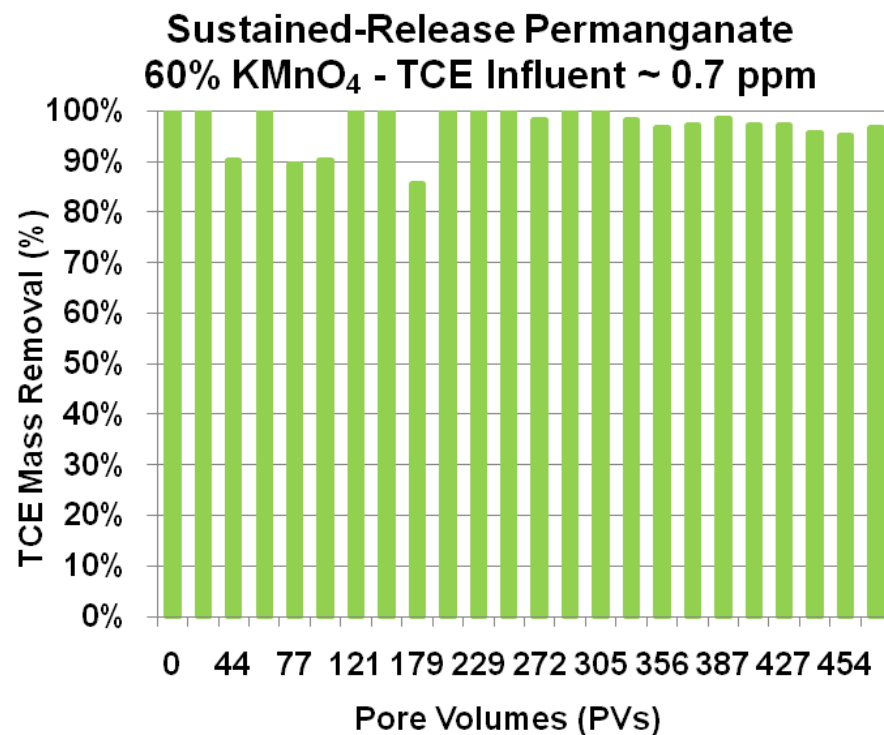
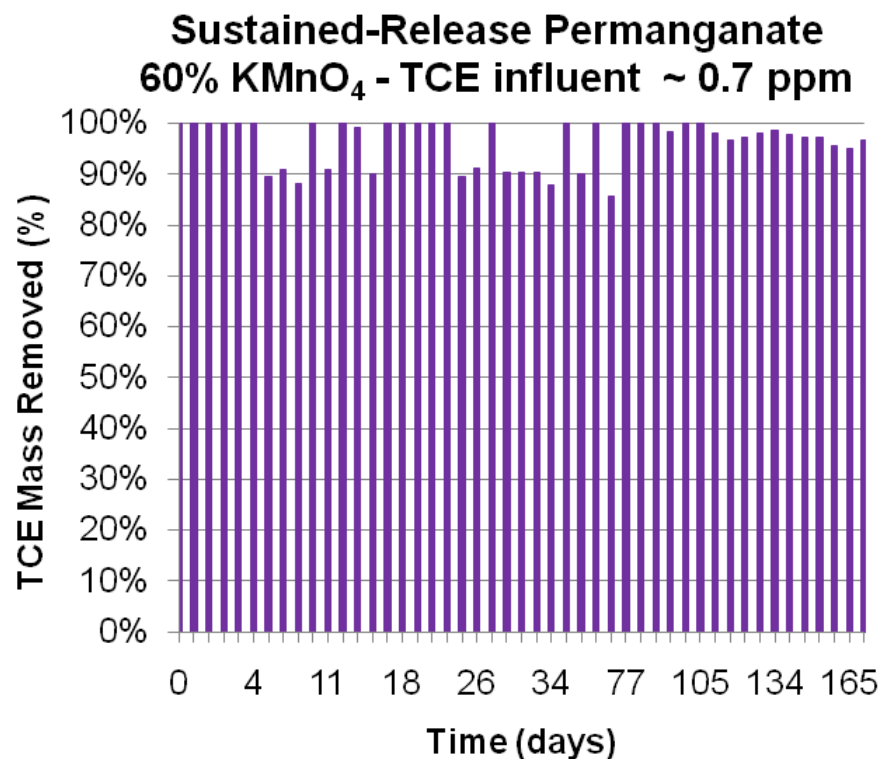
- **Q'** = quantity of MnO_4^- released per unit time
- C_s = MnO_4^- solubility
- A = Amount of MnO_4^- available for release
- D_e = effective diffusion coefficient
- t = time
- h = length of candle
- r_o = radius of candle
- r = radius MnO_4^- diffusion (new porosity development)

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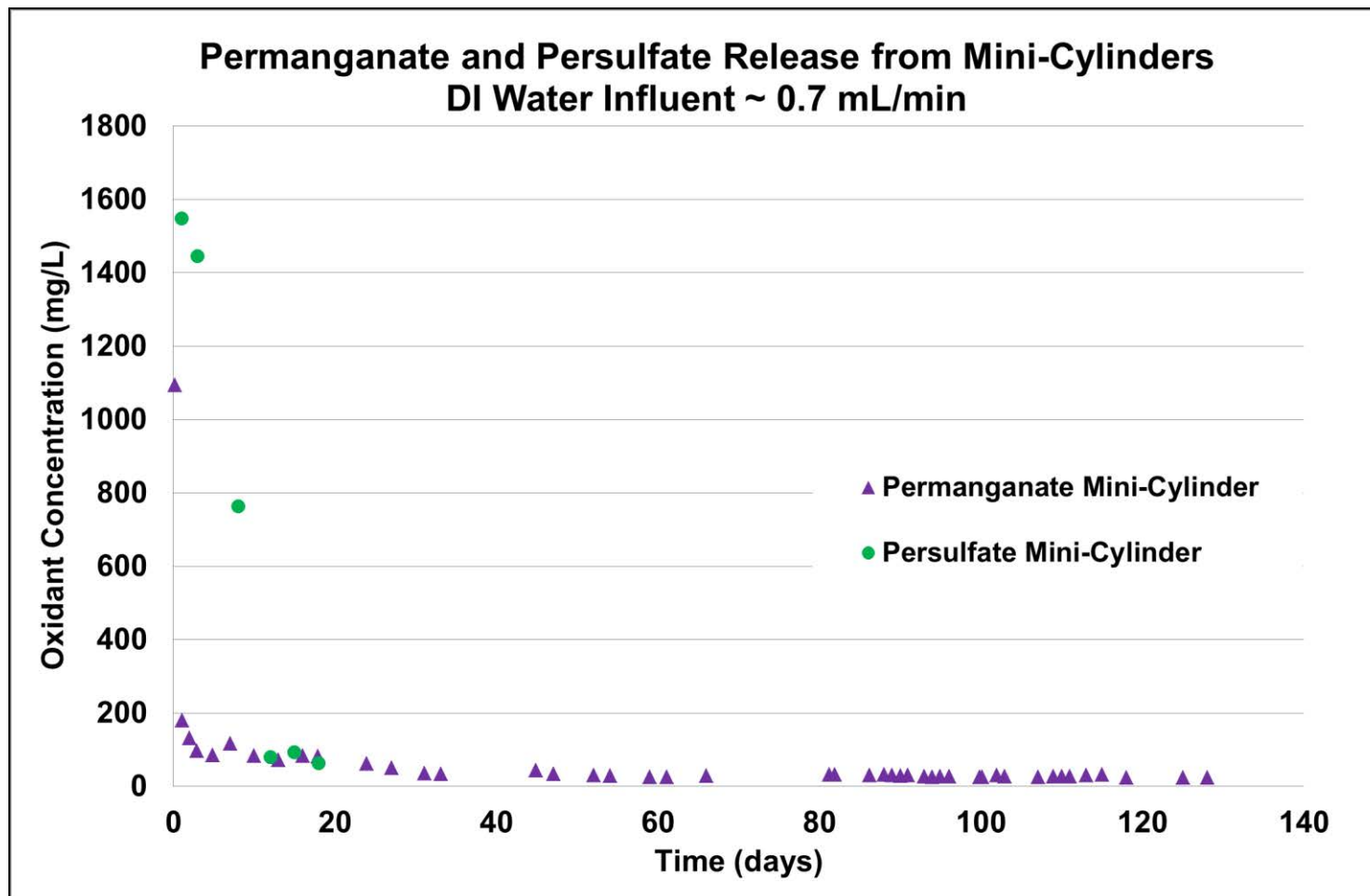
Results – 1D Column with Sustained-Release Cubes



TCE mass removal 86% - 100% over 170 days or > 470 PVs

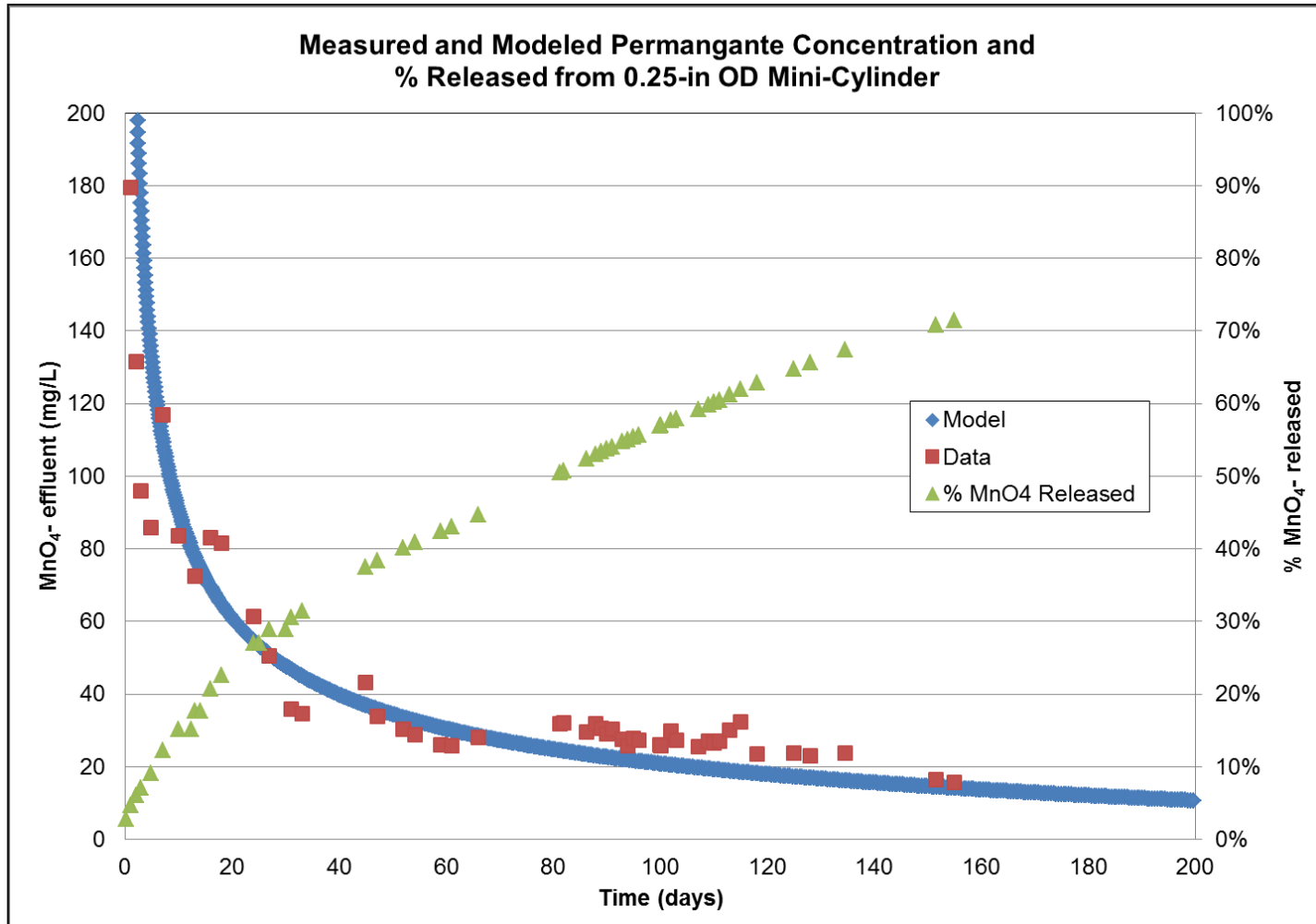


Results – 2-D Tanks (Influent-DI Water)



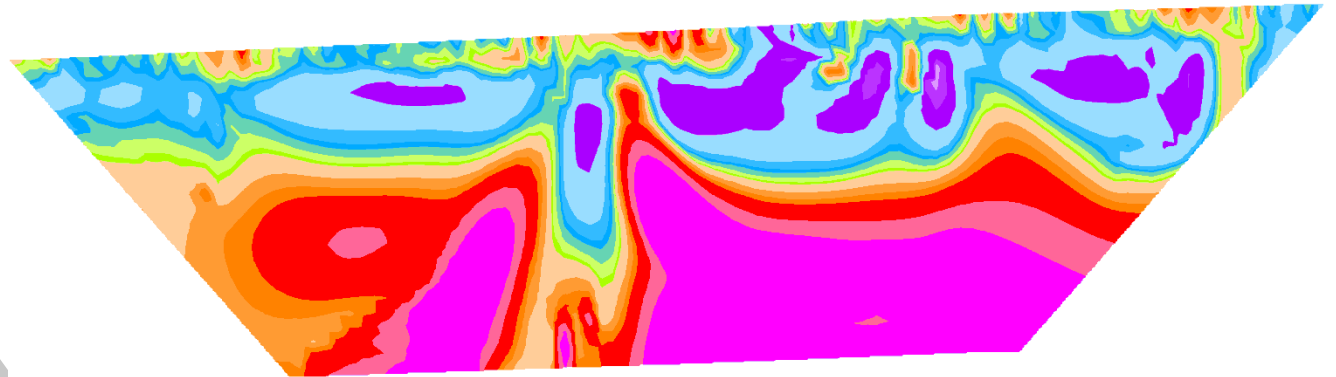


Results – 2D Tank (Influent-DI Water)



Cozad Former Solid Waste Disposal Site

University of Nebraska
Dr. Steve Comfort



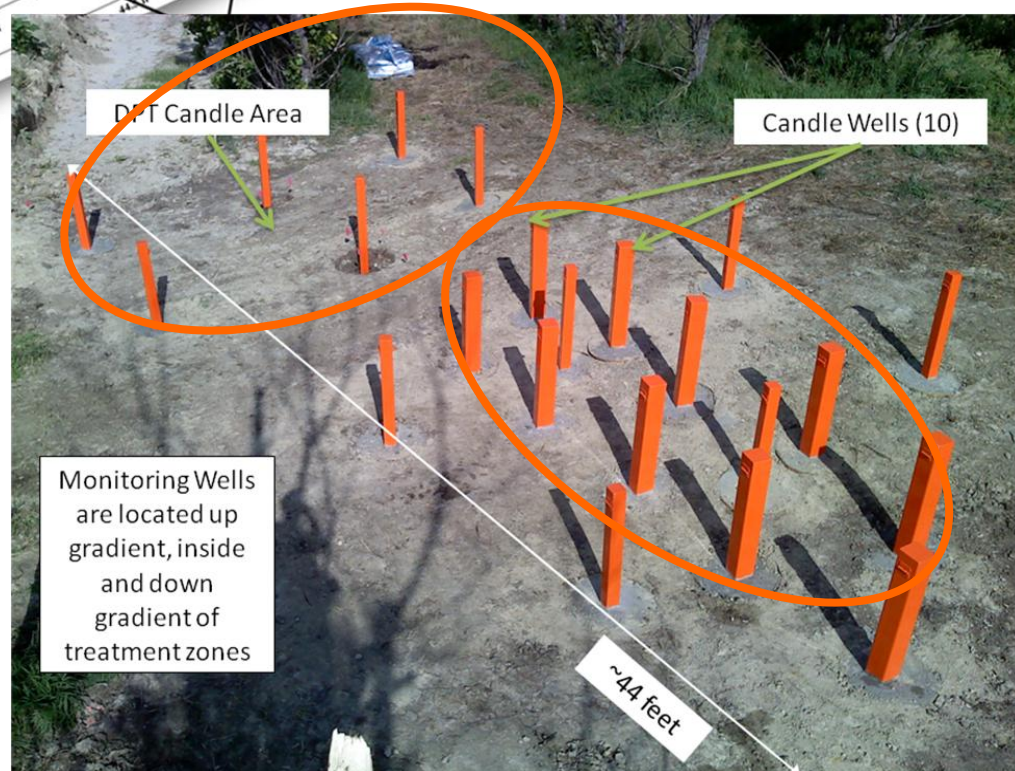
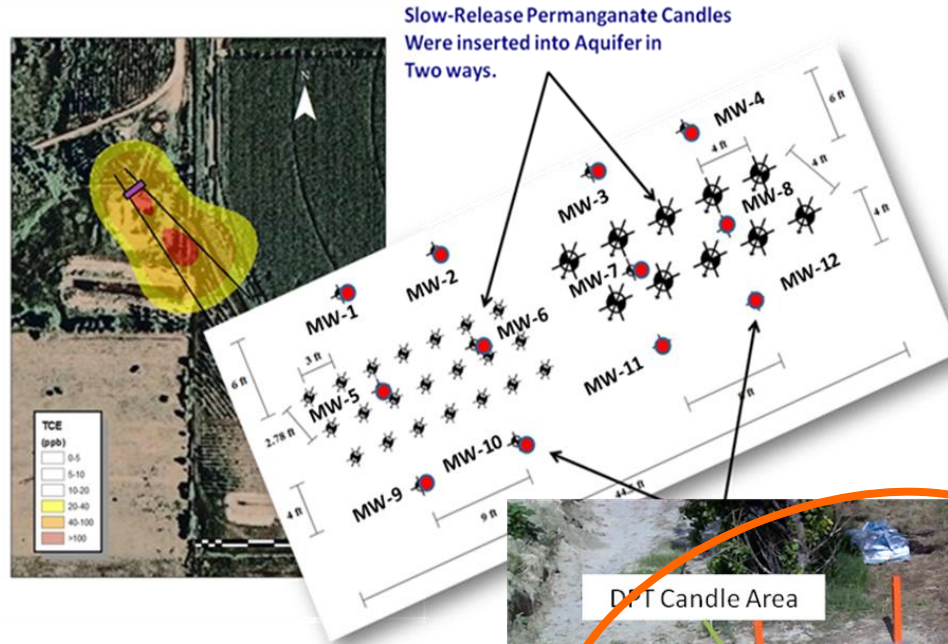
Slow-Release Permanganate Reactive Barrier Installation

105 two
inch DPT
SRPCs

50 three
inch
injection
well SRPCs

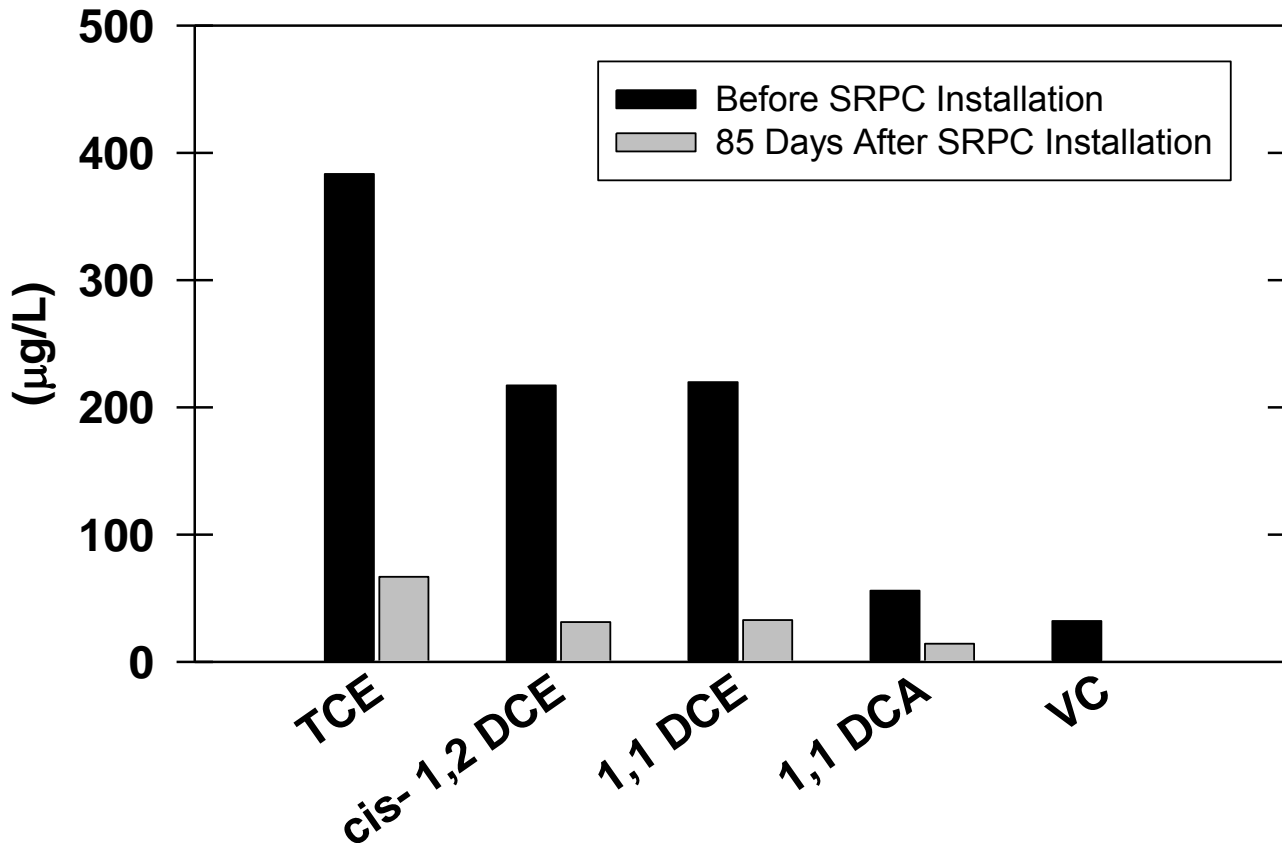


University of Nebraska-Lincoln



Results

Contaminant Concentration in Reactive Barrier
Well MW-8, 11 ft (bgs)



- Barrier installed June 2010
- After 85 days 64%-82% TCE reduction (Christenson et al., 2012)



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Evaluating Oxidant Transport and Release Kinetics

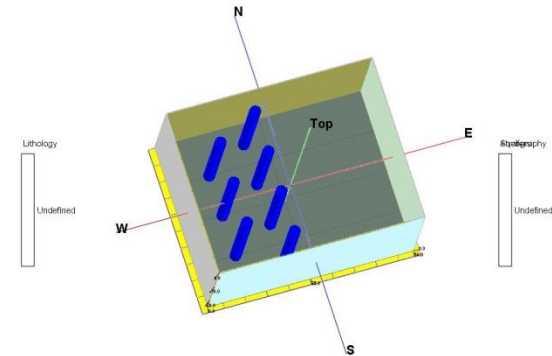
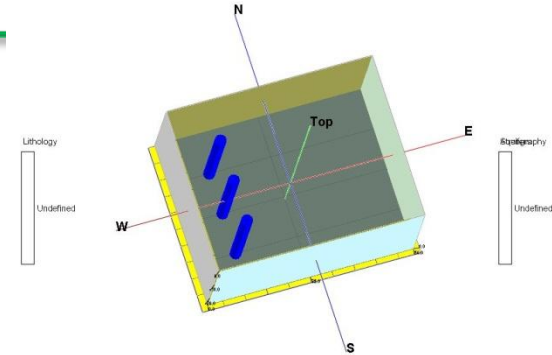
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Sustained-Release Design Tool

- 1D column, 2D and 3-D tank data to develop sustained-release design tool
- Key processes
 - Oxidant release (source)
 - Oxidant type, candle dimensions
 - Oxidant reaction and transport
 - 2nd order NOD
 - 1-D transport with reaction and dispersion
 - Contaminant reaction and transport
 - 2nd order rate constants for TCE, dioxane and co-contaminant(s)
- Output: oxidant and contaminant distribution
 - Can optimize for number and spacing of candles
 - Conceptual design cost estimate



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Sustained-Release Design Tool

Slow Release Oxidant - release, reaction, and transport

Project:

Date:

Prepared by:

Oxidant Release Parameters

Oxidant:

Candle diameter (cm):

Oxidant solubility (mg/l)

Effective diffusion

Amount of av²

Treatment

Treat

(per row):

Dropdown menus

(will autofill)

(will autofill)

(will autofill)

Auto-fill parameters

Site Characteristics*

Primary contaminant:

Concentration (mg/L):

Secondary contaminant:

Concentration (mg/L):

Longitudinal dispersivity:

Transverse dispersivity:

Vertical dispersivity:

Natural oxidant demand (NOD) (mg/kg):

NOD rate (2nd order; $M^{-1}s^{-1}$):

Hydraulic conductivity (cm/s):

Hydraulic gradient (dh/dl):

Porosity:

*guidance provided in 'site characteristics guidance' tab

Dropdown menus

Simulation

Simulation time:

Simulation or compliance

distance downgradient:

Basic project information

Factors affecting oxidant
release rate and resulting
concentration

Contaminant characteristics

Dispersion parameters

**Oxidant demand – rate and
extent**

Flow properties

Simulation **time and
distance** of interest

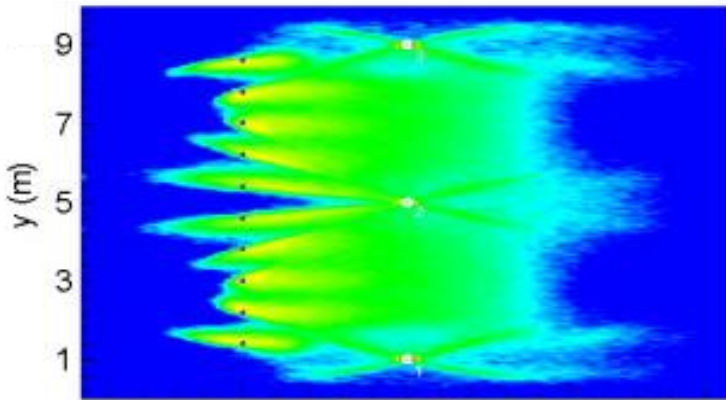
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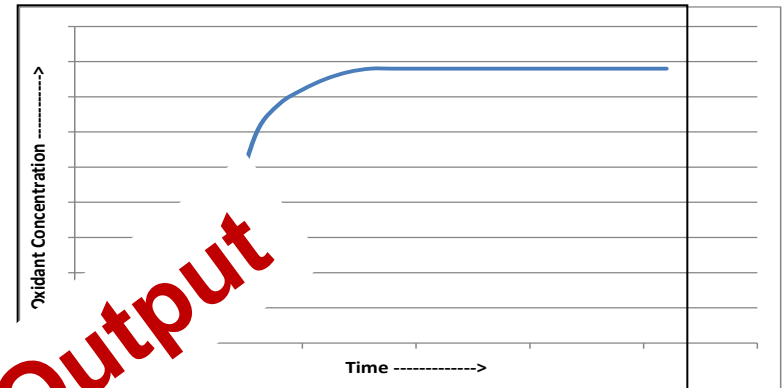
Sustained-Release Design Tool

Oxidant concentrations vs. distance at
a given time

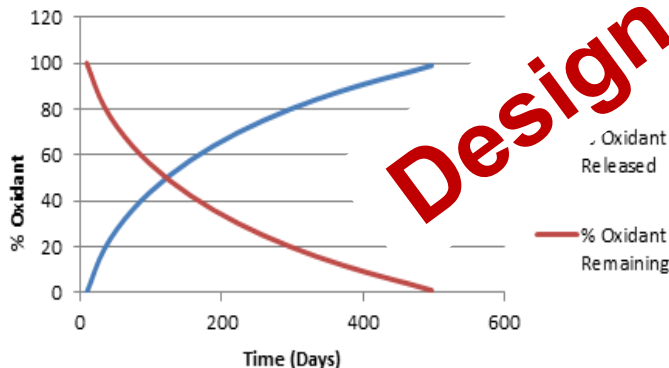
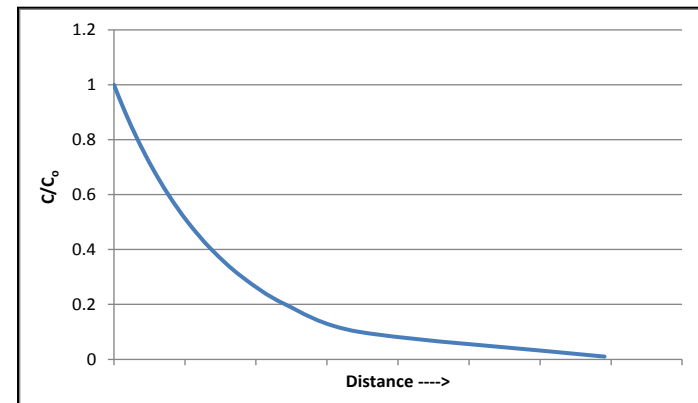


Oxidant release from cylinders

Oxidant concentrations at a given point
over time



Contaminant concentrations
vs. distance at a given time



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Sustained-Release Design Tool

Scenario 1 - minimum required mass flux of MnO₄ required - mg/day (based on 1gTCE:1.8gMnO₄ * 10 SF)

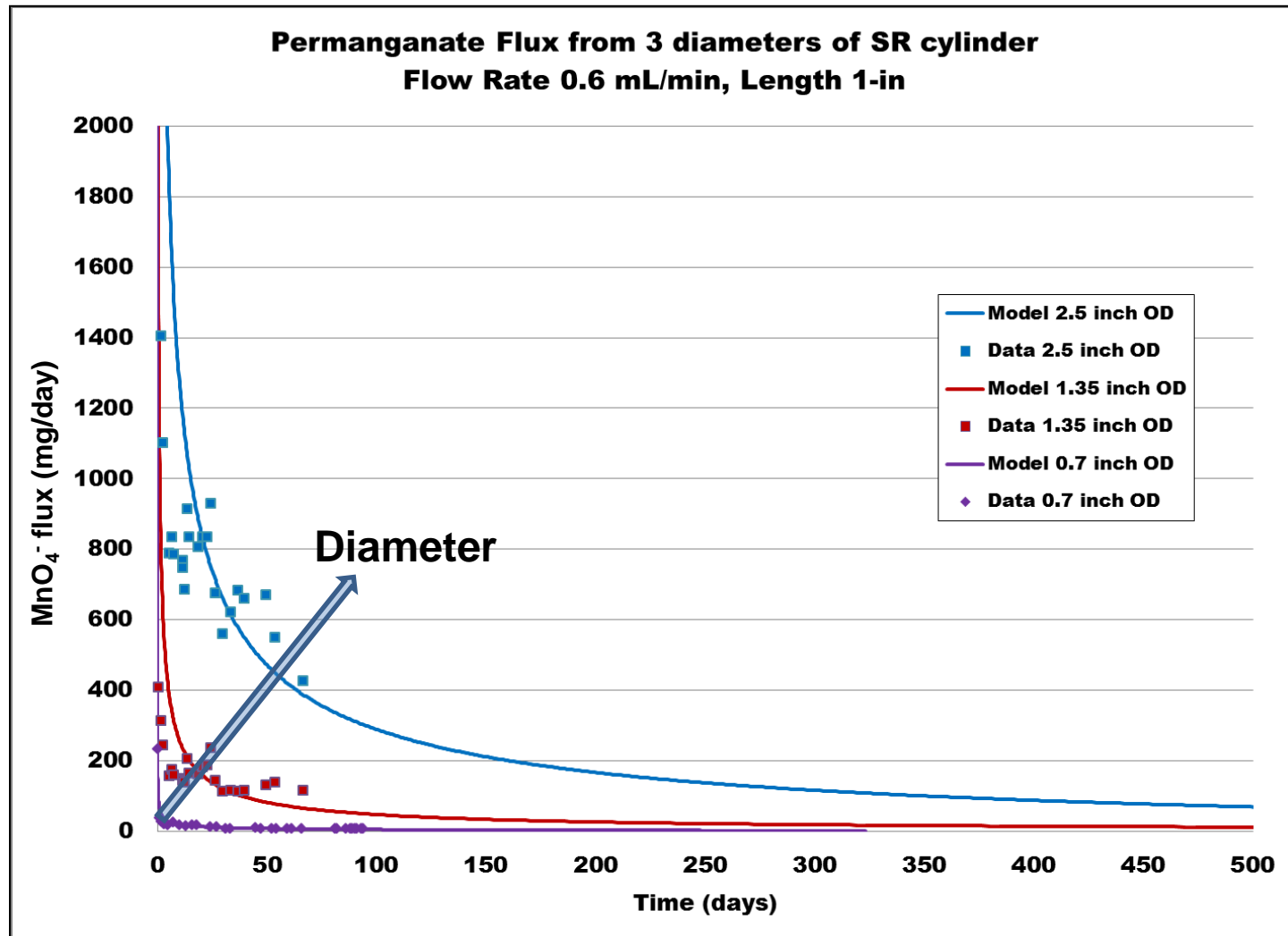
	COC (mg/L)						
Vgw (feet/day)	0.01	0.05	0.1	0.5	1	5	10
0.01	0.046	0.229	0.459	2.294	4.587	22.937	45.873
0.05	0.229	1.147	2.294	11.468	22.937	114.683	229.366
0.1	0.459	2.294	4.587	22.937	45.873	229.366	458.733
0.5	2.294	11.468	22.937	114.683	229.366	1146.832	2293.665
1	4.587	22.937	45.873	229.366	458.733	2293.665	4587.329
5	22.937	114.683	229.366	1146.832	2293.665	11468.323	22936.646
10	45.873	229.366	458.733	2293.665	4587.329	22936.646	45873.291

Scenario 2 - minimum required mass flux of MnO₄ required - mg/day (based on 1gTCE:1.8gMnO₄ * 10 SF)

	COC (mg/L)						
Vgw (feet/day)	0.01	0.05	0.1	0.5	1	5	10
0.01	0.092	0.459	0.917	4.587	9.175	45.873	91.747
0.05	0.459	2.294	4.587	22.937	45.873	229.366	458.733
0.1	0.917	4.587	9.175	45.873	91.747	458.733	917.466
0.5	4.587	22.937	45.873	229.366	458.733	2293.665	4587.329
1	9.175	45.873	91.747	458.733	917.466	4587.329	9174.658
5	45.873	229.366	458.733	2293.665	4587.329	22936.646	45873.291
10	91.747	458.733	917.466	4587.329	9174.658	45873.291	91746.583

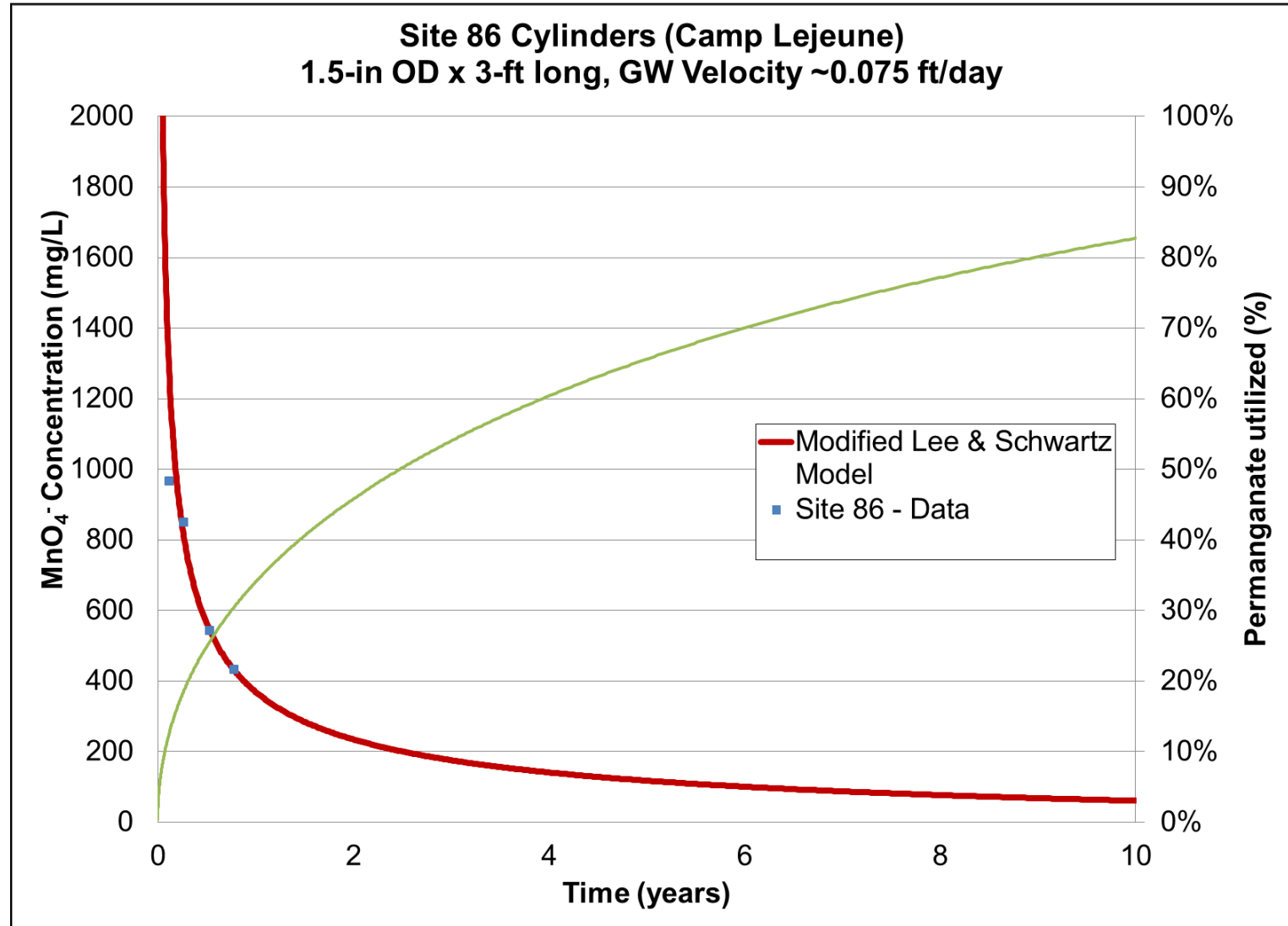


Model Results – 1-in Sections Mini-SRPC, 1.35-in, 2.5-in





Model Results – Preliminary Field Data



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Exploring the Possibilities...

1. Minimal aboveground infrastructure (and site disruption) so can implement quickly at an active site
 - No tanks, water needs, dust, pressurized injection



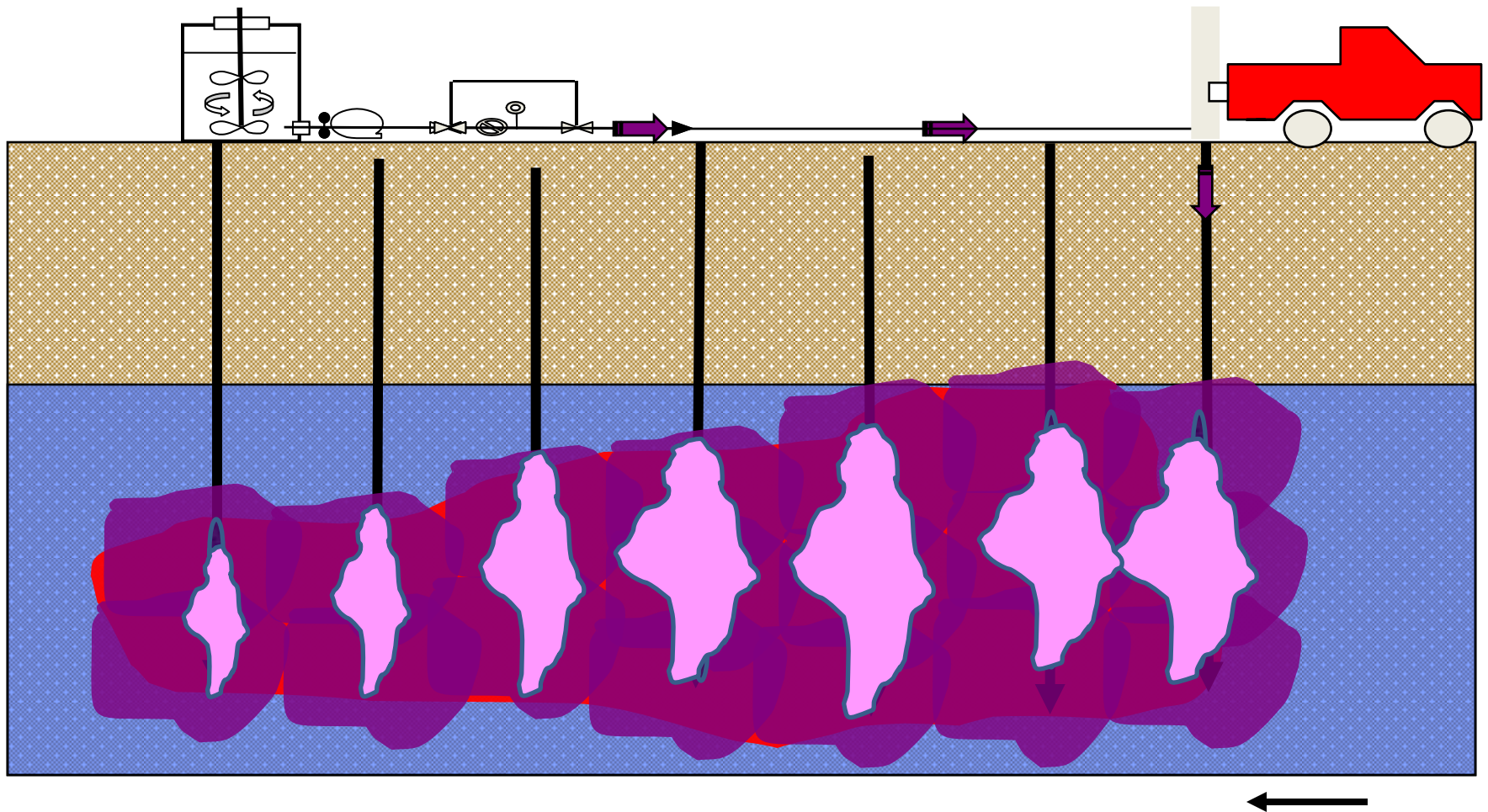
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Exploring the Possibilities...

2. Get two injections for the price of one
 - Long term treatment of residual absorbed material in clay (back diffusion)



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Exploring the Possibilities...

3. No surfacing of liquids



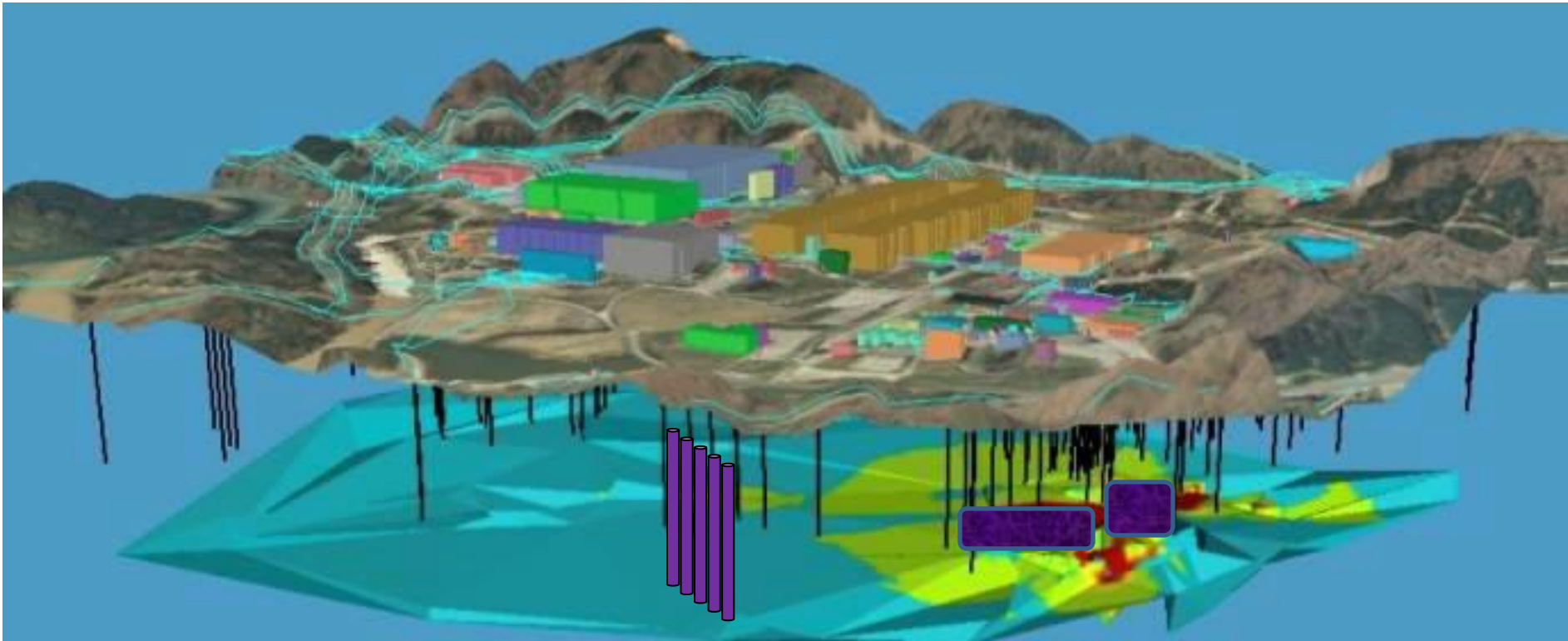
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Exploring the Possibilities...

4. Ability to approach ISCO in an active stepped manner



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Take Home Message

- 5 pilot-scale sites (US), 2 pending (US and Brazil) Canada?
- Direct push/in-well applications for treatment that may last years
 - Potential for application in low permeability soils and fractured bedrock
 - **Address “rebound” and back diffusion**
 - Active industrial and commercial facilities: passive *in situ* treatment without above ground equipment/infrastructure
- Cost savings realized with direct push delivery

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Questions?



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