



Optimizing In-situ Chemical Oxidation of Residual DNAPL: Geochemical Controls and Sediment Oxidant Demand

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Towards effective source zone remediation

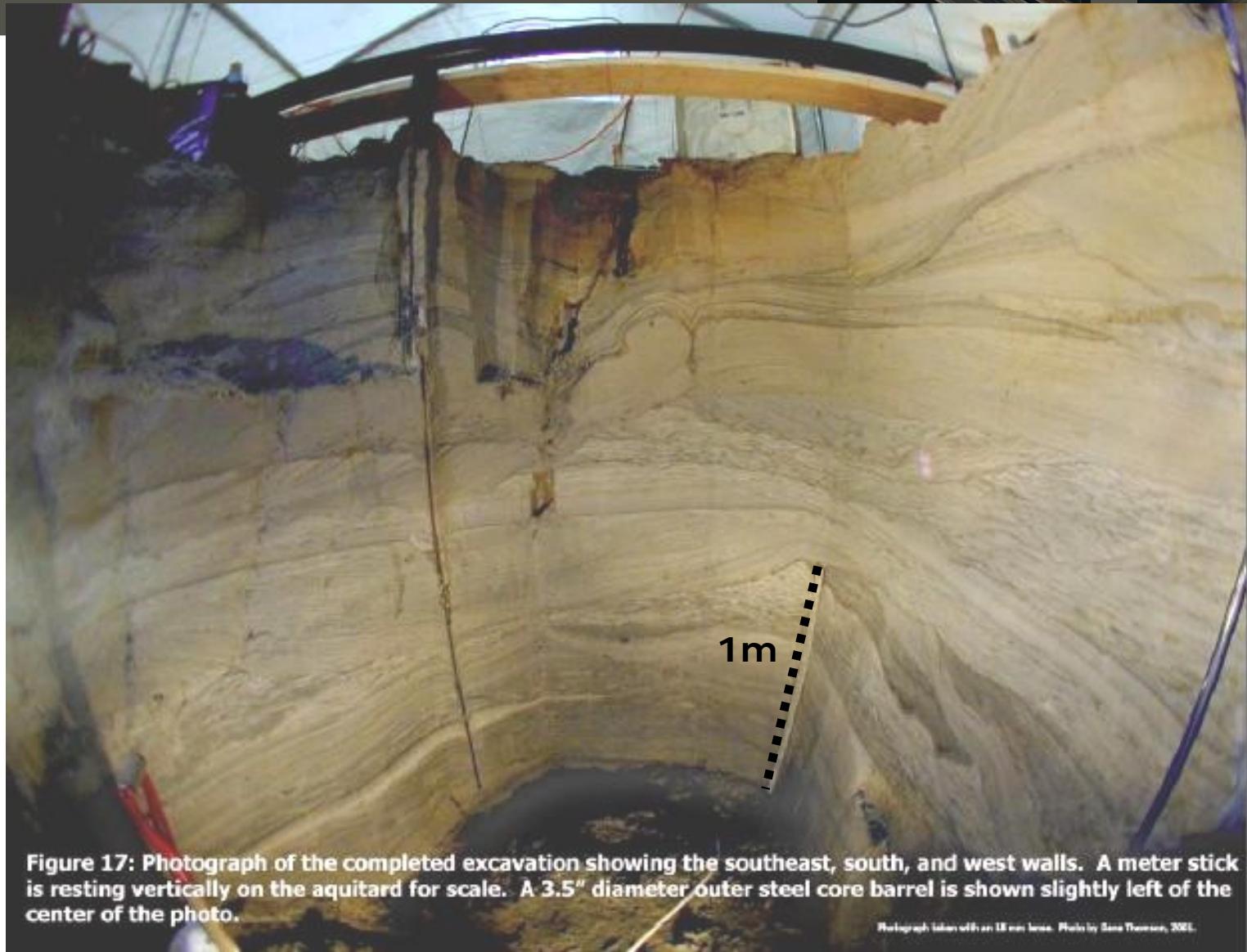
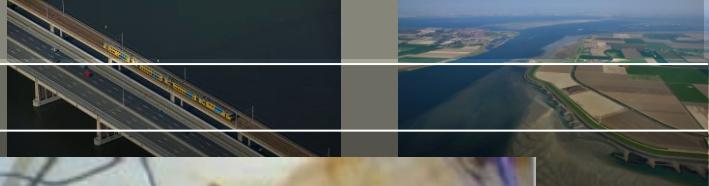


Borden DNAPL Infiltration (BDI) Site

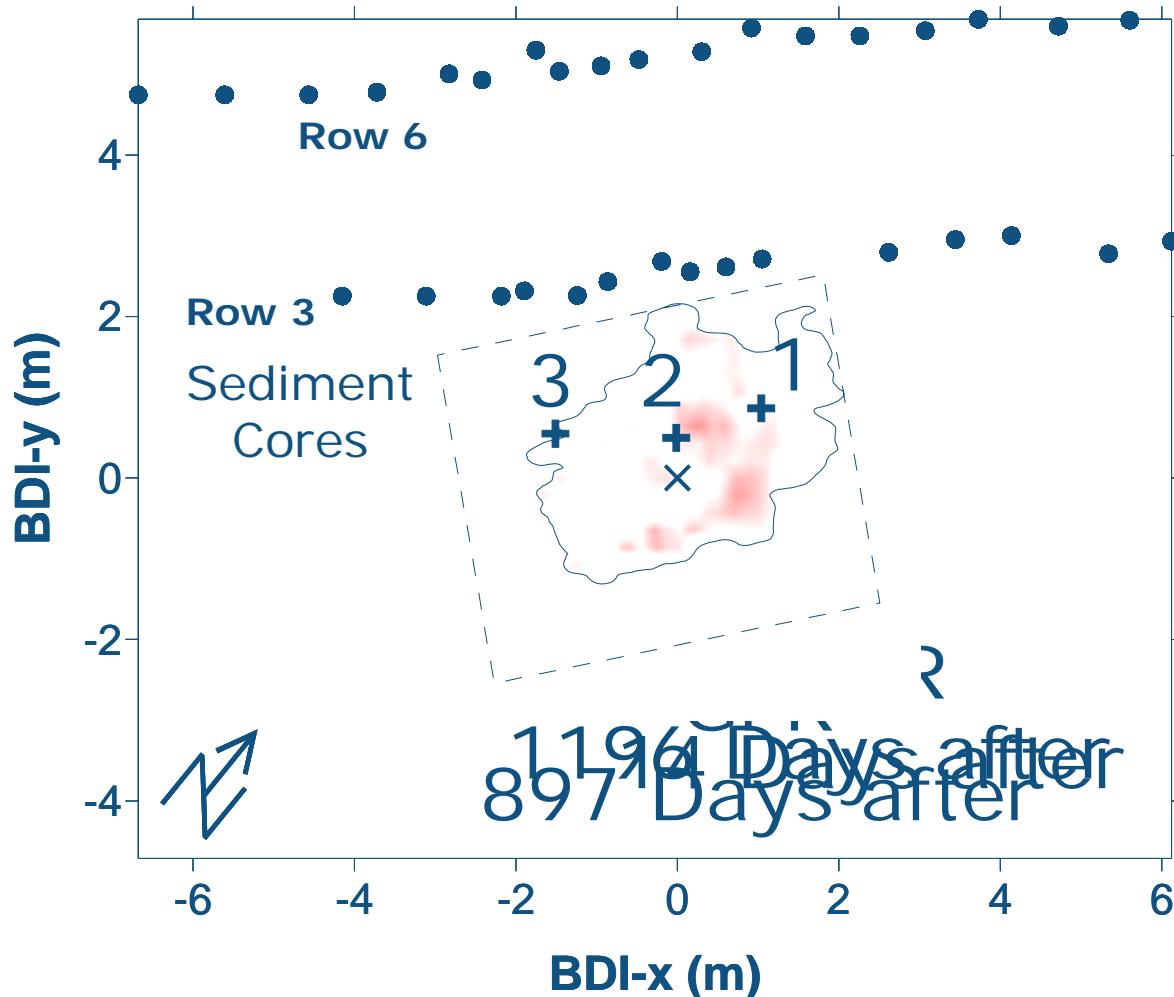
8 April 1999
DNAPL Day: 1

50L DNAPL infiltration

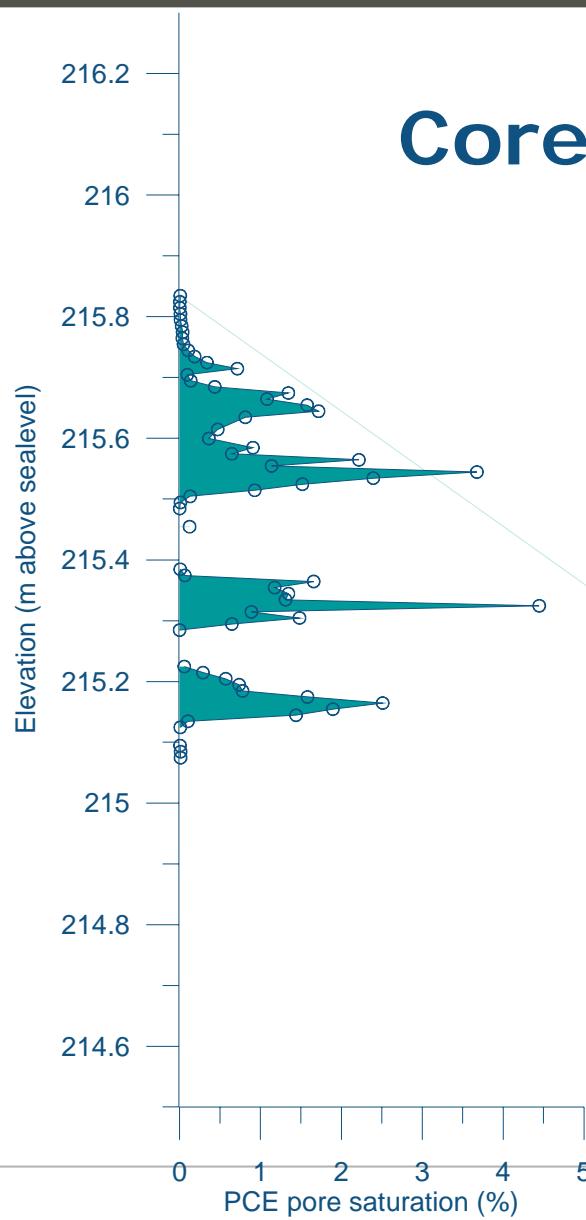
3D “Homogeneous” Aquifer



Remaining Mass in Source Zone



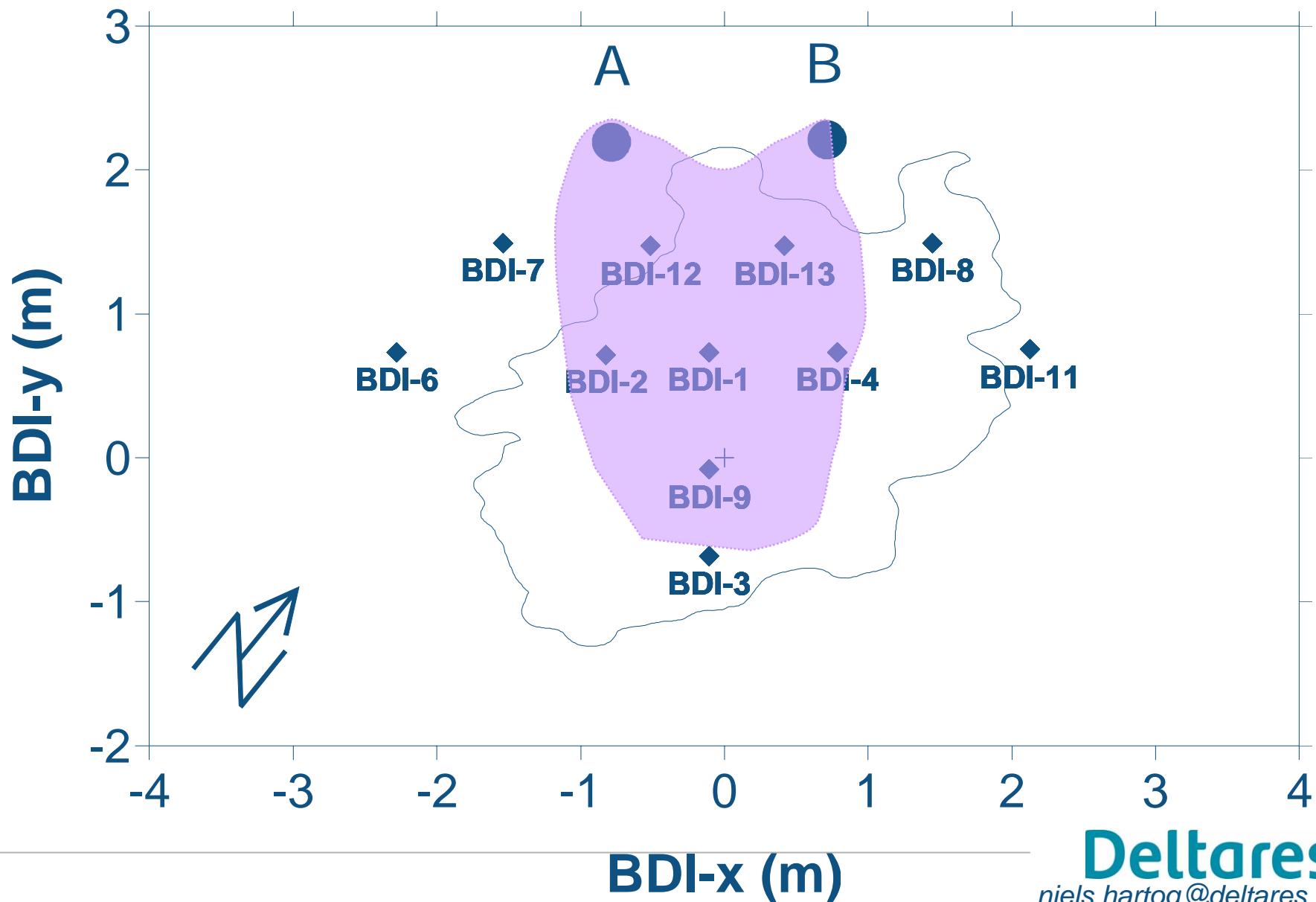
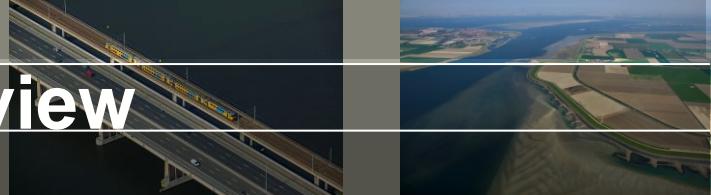
DNAPL pore saturation variability



Core 1



Permanganate Injection Overview

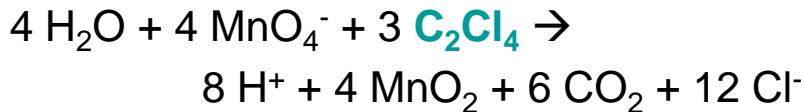


Modeling Permanganate Oxidation Reactions (PHREEQC)

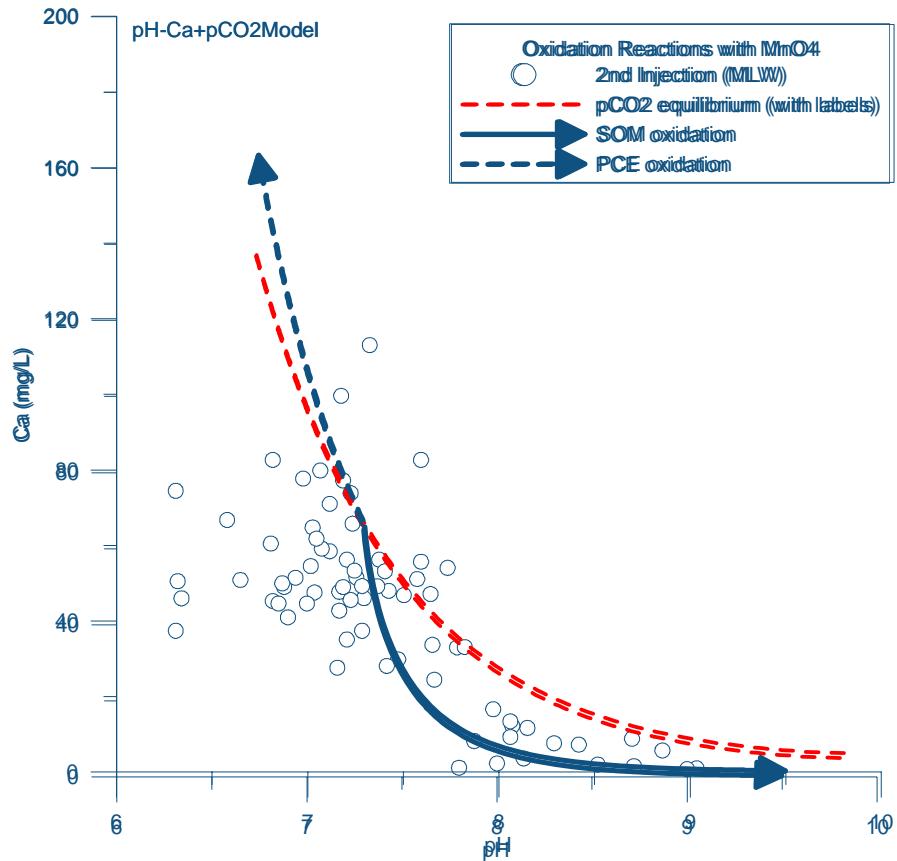
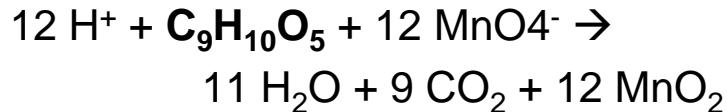


Oxidation Reactions with MnO₄

PCE



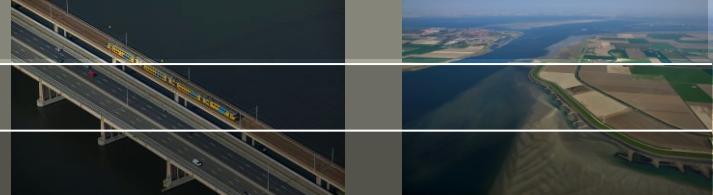
SOM



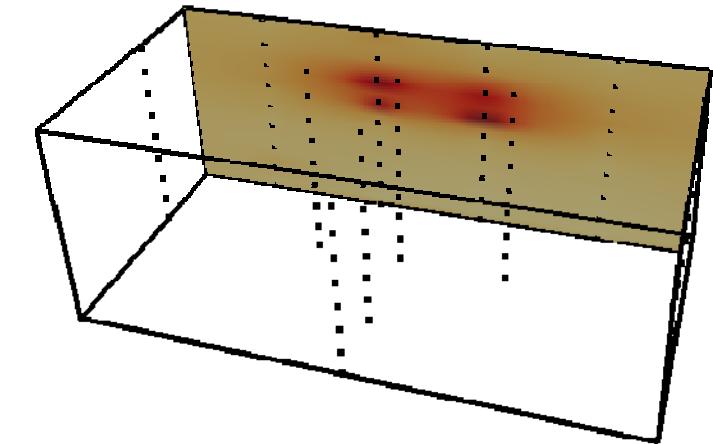
> 95% MnO₄ consumed by sediment!



PCE Concentrations in MLWs



Before 1st Injection



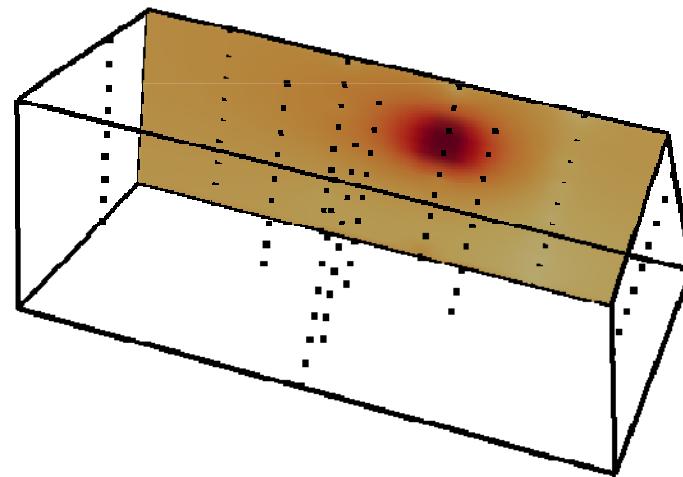
PCE ($\mu\text{g/L}$)

0 10000 20000



After 1st Injection

- Plume size reduction



PCE ($\mu\text{g/L}$)

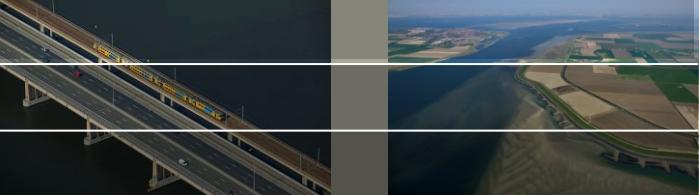
0 1000 2000



- 10-fold reduction [PCE]
- 100-fold reduction PCE flux



Canada ↔ The Netherlands



Overview contaminated Sites in The Netherlands



Site Characteristics		Occurrence % of total)
15,000 most urgent sites		
Contaminant type (C)	C.1 Chlorinated Hydrocarbons	45
	C.2 Aromatics/Oil/MTBE/Cyanide	45
	C.3 Other	10
Geo-hydrology (G)	G.1 Permeable (sandy)	45
	G.2 Layered, permeable and impermeable layers	45
	G.3 Other	10
Built Environment (B)	B.1 Urban	70
	B.2 Industrial	25
	B.3 Other	5

Holland
In-Situ
Proeftuin

hip

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Optimizing the ISCO remediation of Chlorinated Solvents

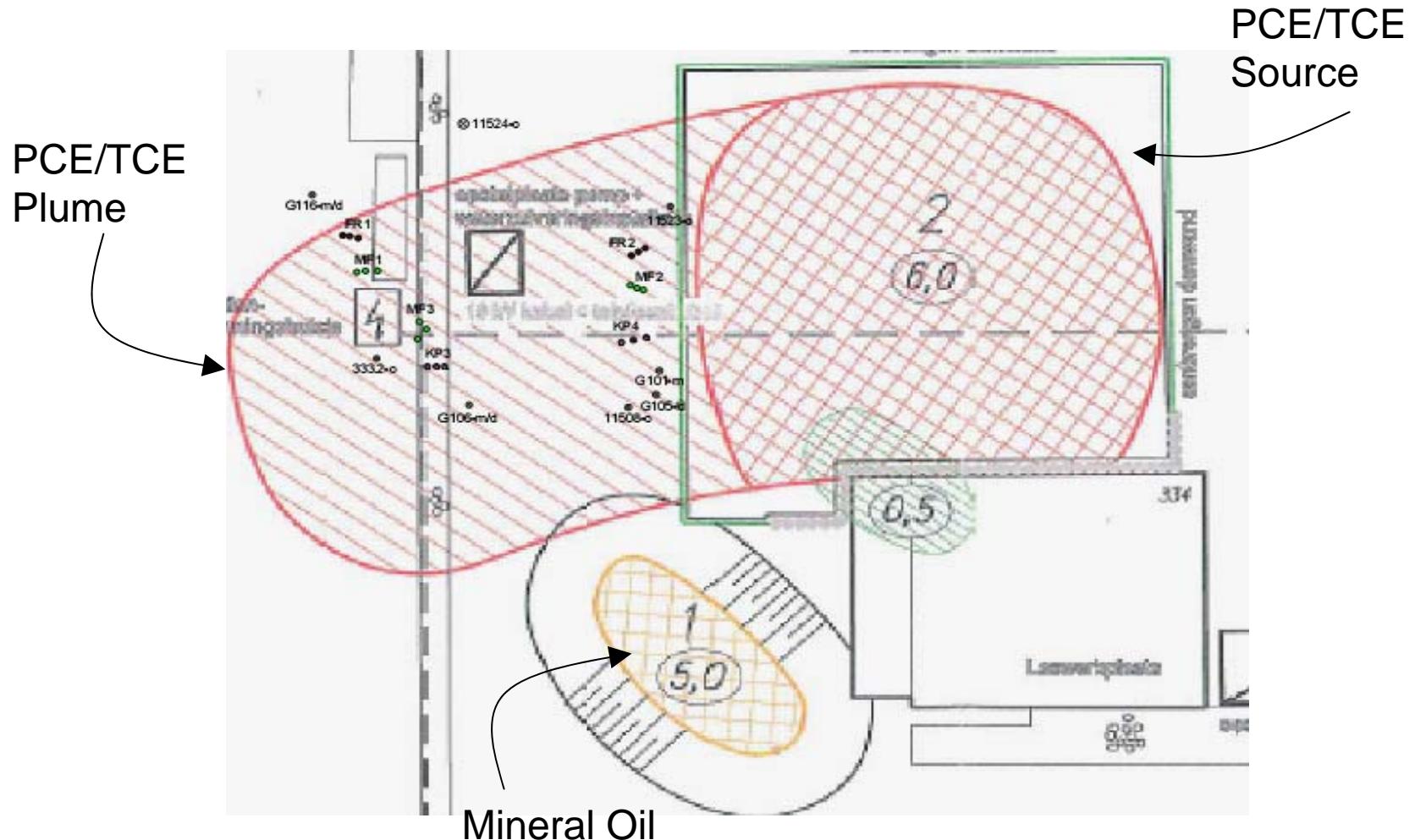
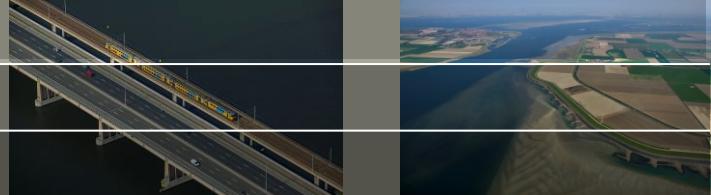


Holland
In-Situ
Proeftuin

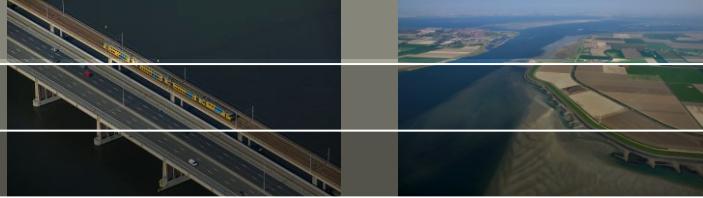
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Overview Contaminated Site



50% : 50%



Fenton's Reagens

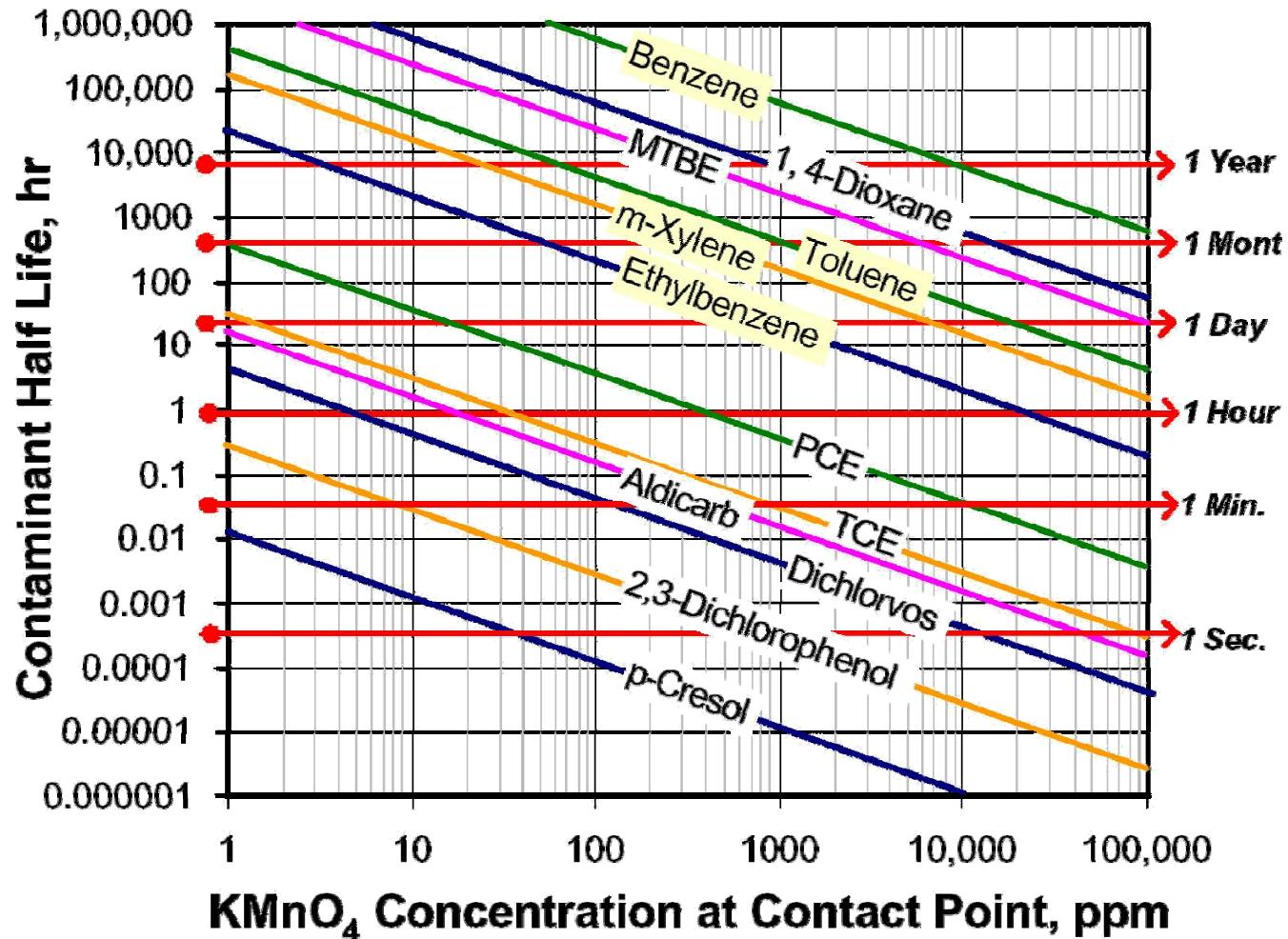


0.001MOL/L

0.1MOL/L

Permanganate

Rates of contaminant oxidation with MnO₄



Ref: Waldemer, R., Determination of the Rate of Contaminant Oxidations by Permanganate: Implications for In Situ Chemical Oxidation (ISCO), M.S. Thesis, Oregon

Natural and Contaminant Oxidant Demand



Factors:

Contaminant Oxidant Demand

- Mass, Volume, Distribution

Sediment Oxidant Demand (SOD, NOD)

- Geochemistry, Heterogeneity

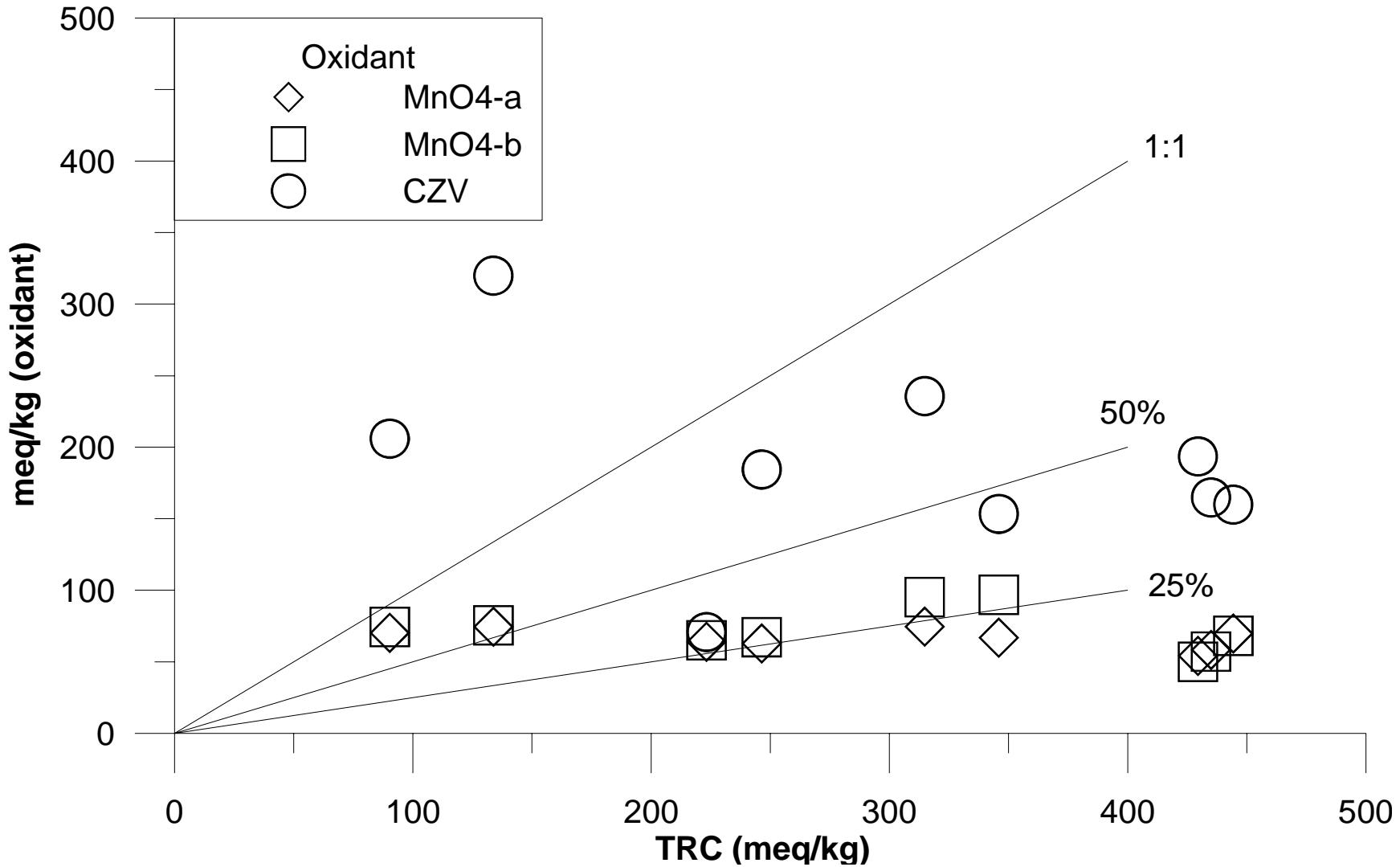
Groundwater Oxidant Demand

- Groundwater composition, Redox status, Groundwater flow

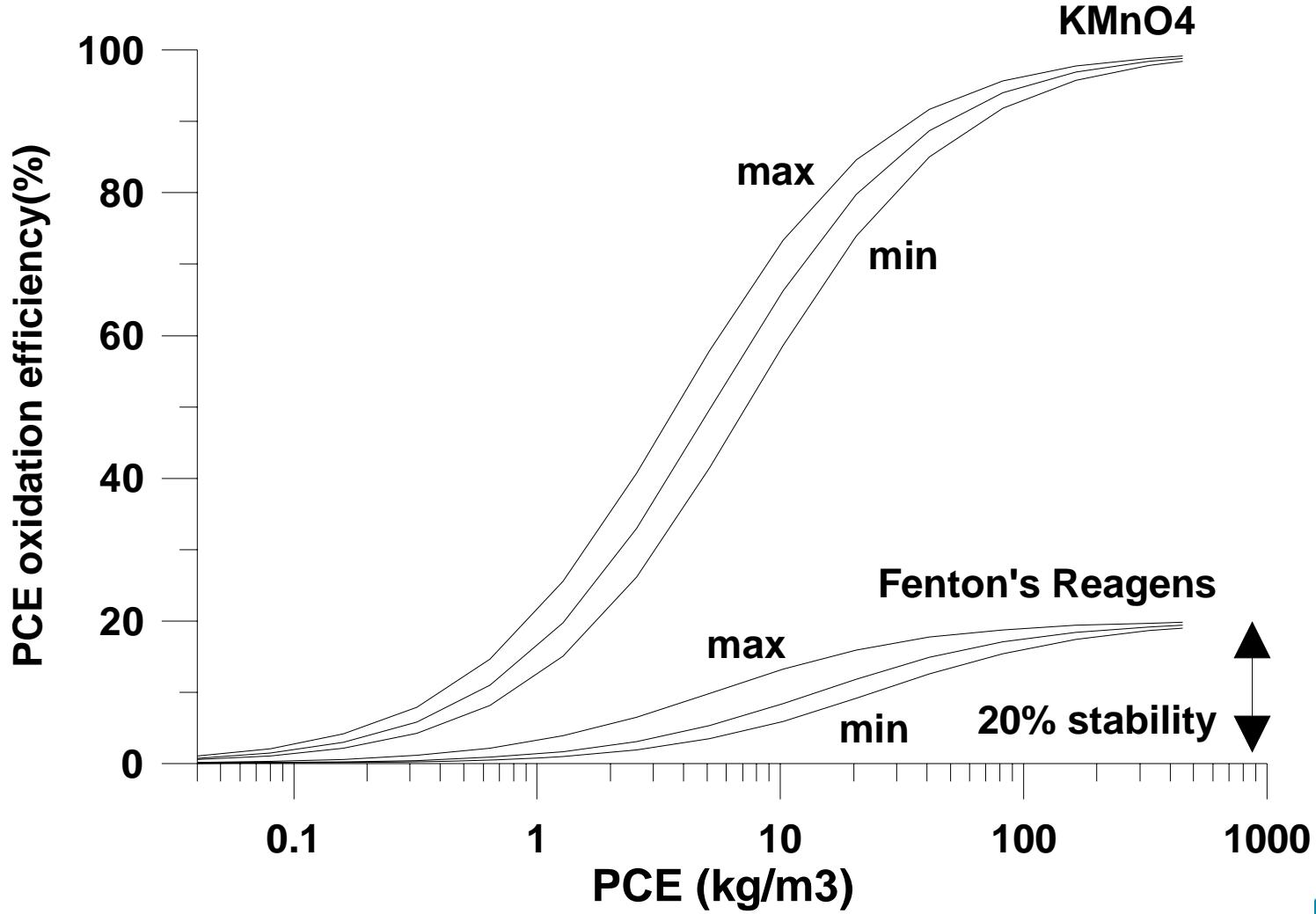
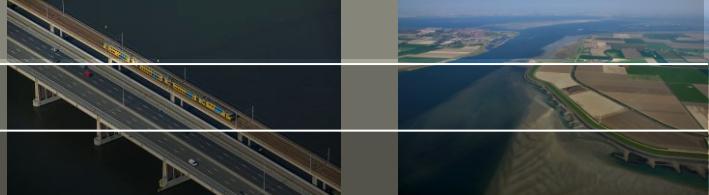
Soil Samples for Geochemistry and Reactivity



Total Reduction Capacity vs. Oxidant Demand



Remediation Efficiency



Assessment of critical parameters: simplified

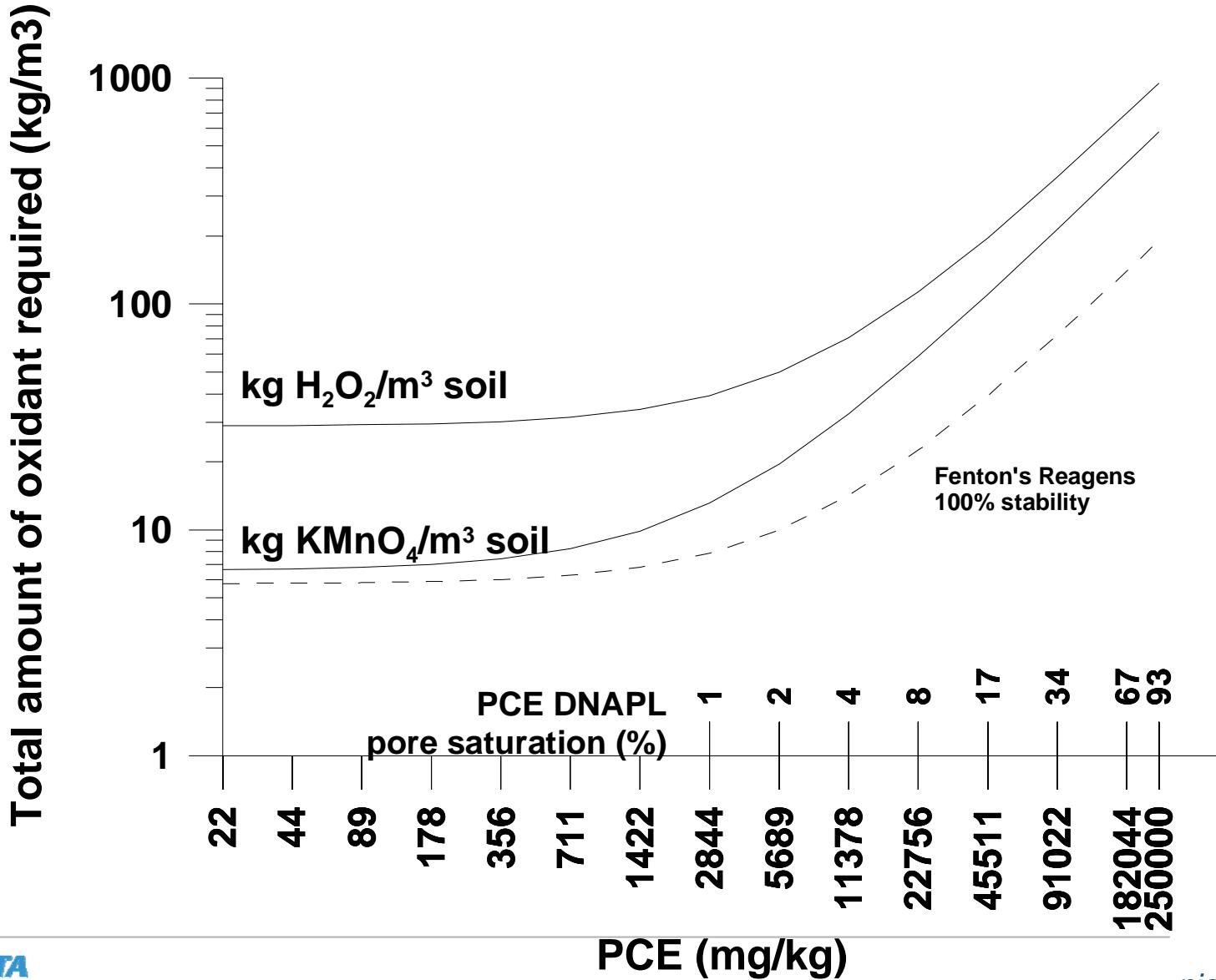
$$Oxidant_{req} = \left(\frac{Oxidant_{cont} + Oxidant_{NOD}}{Oxidant_{stab}} \right)$$

Main Assumptions:

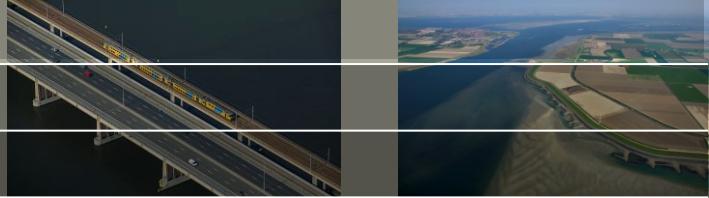
- Direct injection in NAPL zone, no travel
- Oxidant reacts with NOD first, no competition (worst case)
- Constant degree of decomposition

$$Oxidant_{eff} = \frac{Oxidant_{cont}}{\left(\frac{Oxidant_{cont} + Oxidant_{NOD}}{Oxidant_{stab}} \right)}$$

Cost-effectiveness ($\text{kg/m}^3 \times \text{€/kg}$)



Conclusions



- Oxidant specific NOD tests should be performed, due to different reaction mechanisms for different oxidants used in ISCO.
- The influence of NOD on oxidation efficiency is especially important for lower contamination degrees.
- At higher contamination degrees, oxidant stability becomes the dominating factor for ISCO efficiency.
- Remedial ISCO strategies only be based on site-specific cost-effectiveness determinations.
- Source zone characterization crucial for cost-effective optimization of remediation strategy

Videocone: Take a peak in the black box

