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**Tidal Implications for
Remediation of a Coal Waste
Pile in Union Bay, BC**

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Tidal Implications - Remediation of a Coal Waste Pile in Union Bay, BC

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Outline

- Site Description and History
- Environmental Investigations
- Detailed Hydrogeological assessments
- Remediation/Reclamation Plan

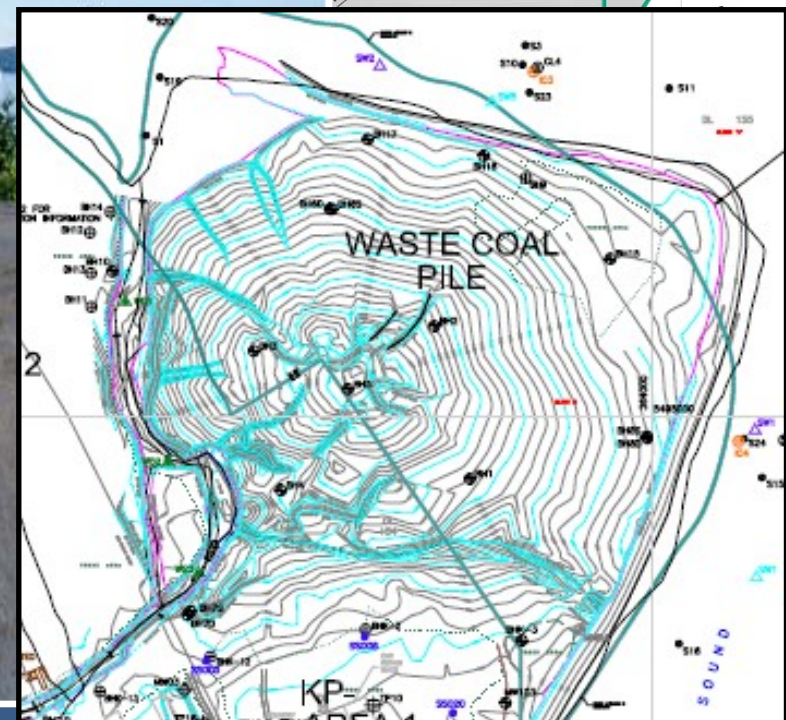
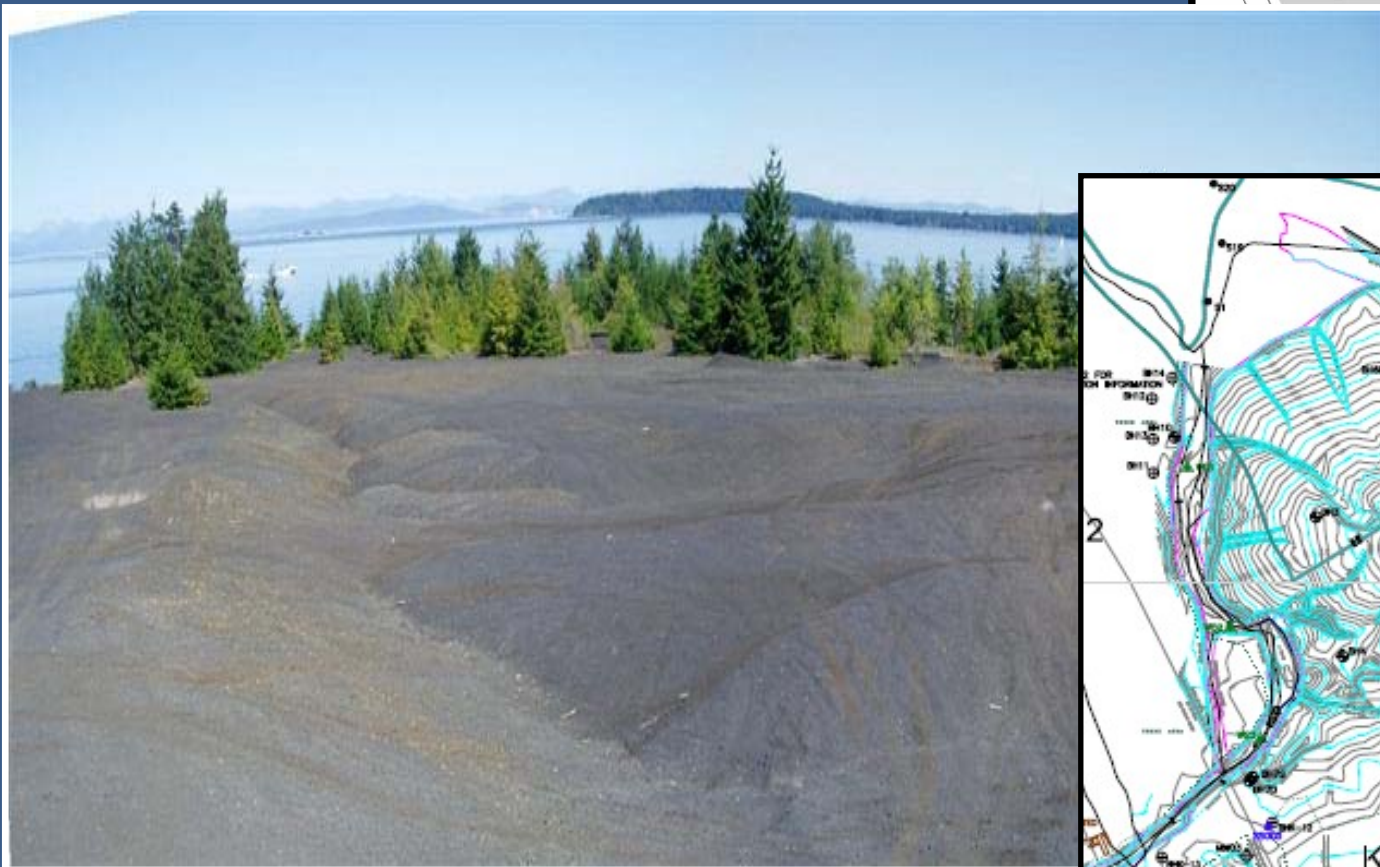


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Site Description

13 ha waste coal pile in Union Bay, BC



Site Description

- 13 ha waste coal pile in Union Bay, BC
- Bounded to north and east by Pacific Ocean



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Site Description

- 13 ha waste coal pile in Union Bay, BC
- Bounded to north and east by Pacific Ocean
- Bounded to west by Hart Creek

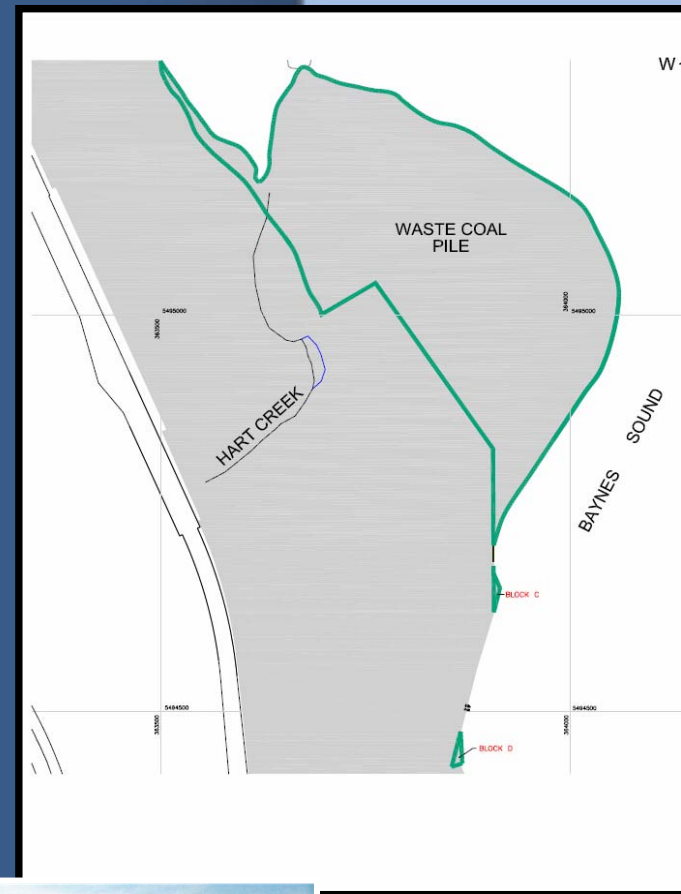


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Site Description

- 13 ha waste coal pile in Union Bay, BC
- Bounded to north and east by Pacific Ocean
- Bounded to west by Hart Creek
- Future land use: golf course



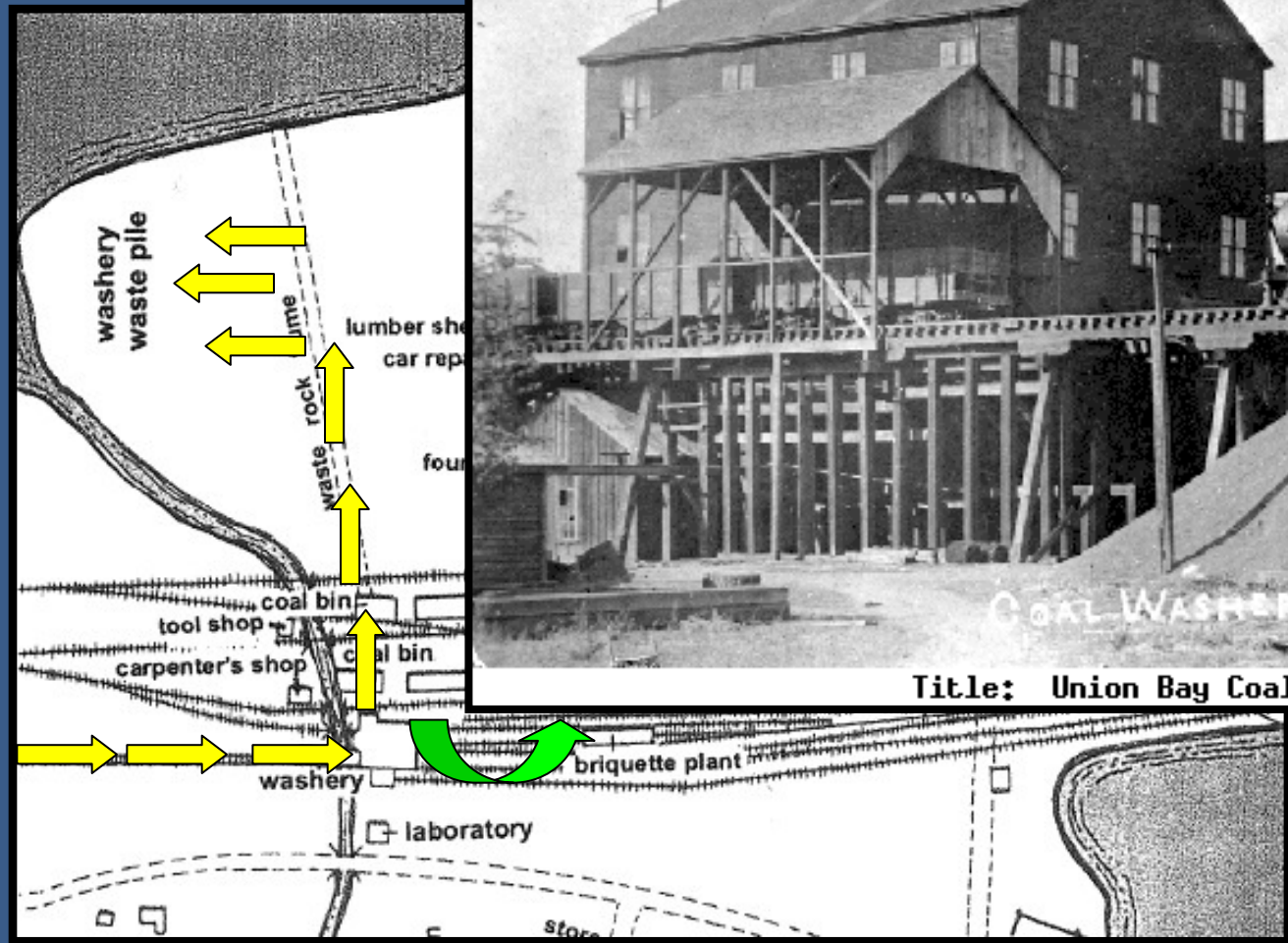
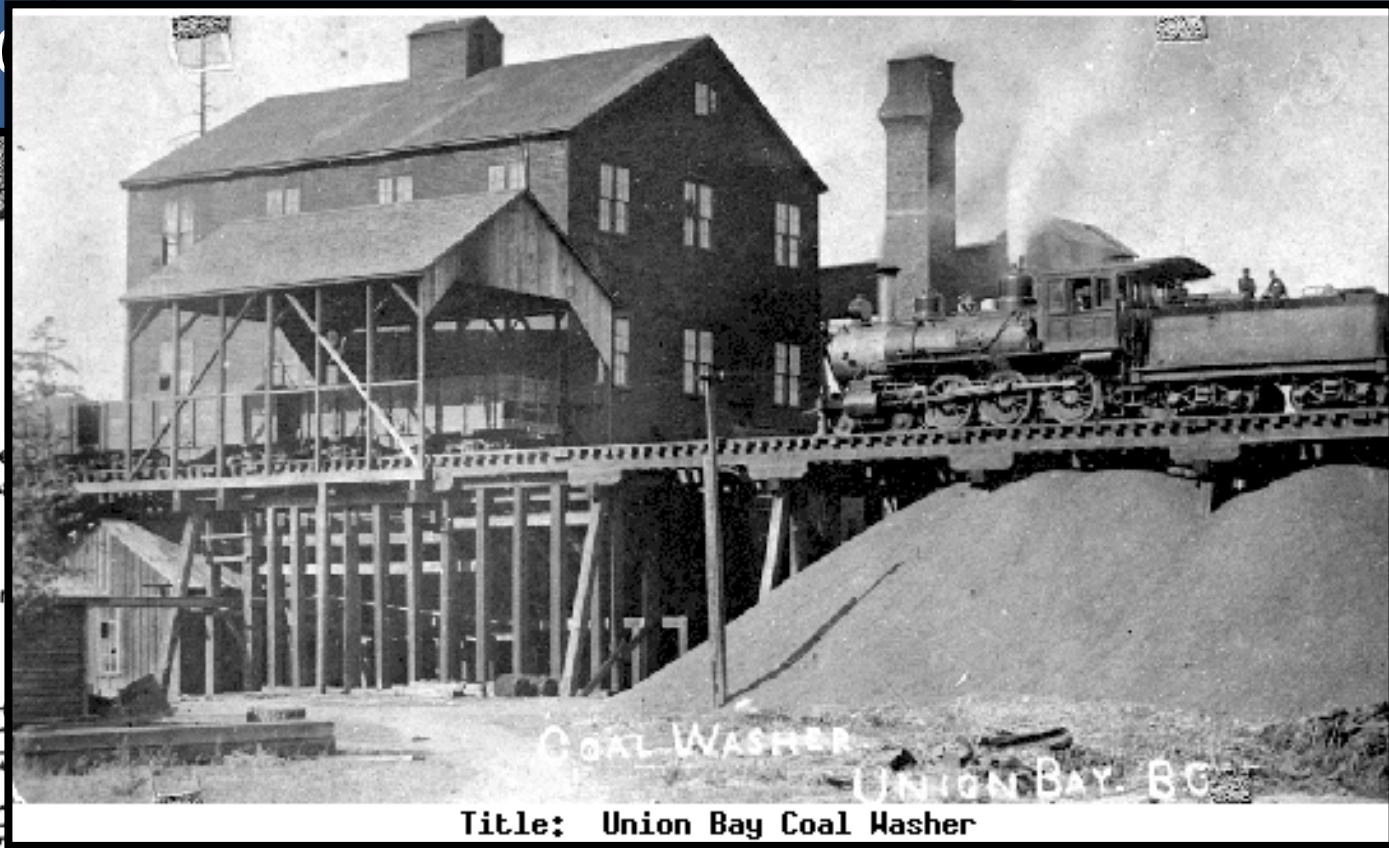
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Site History



- Coal Processing Facility
- 1888 to ~ 1960



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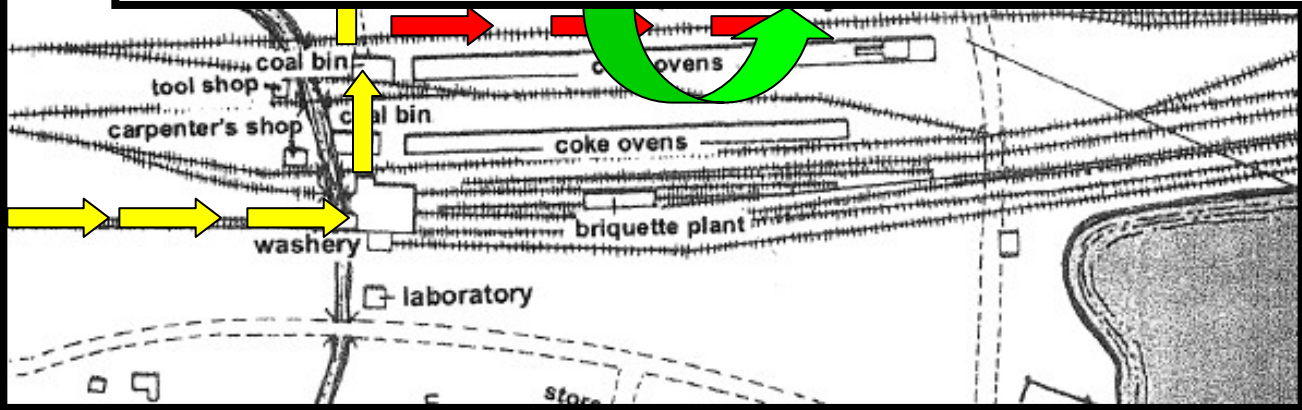
Title: Union Bay Coal Husher



Title: Coal Docks at Union Bay



Title: Coke Ovens at Union Bay.

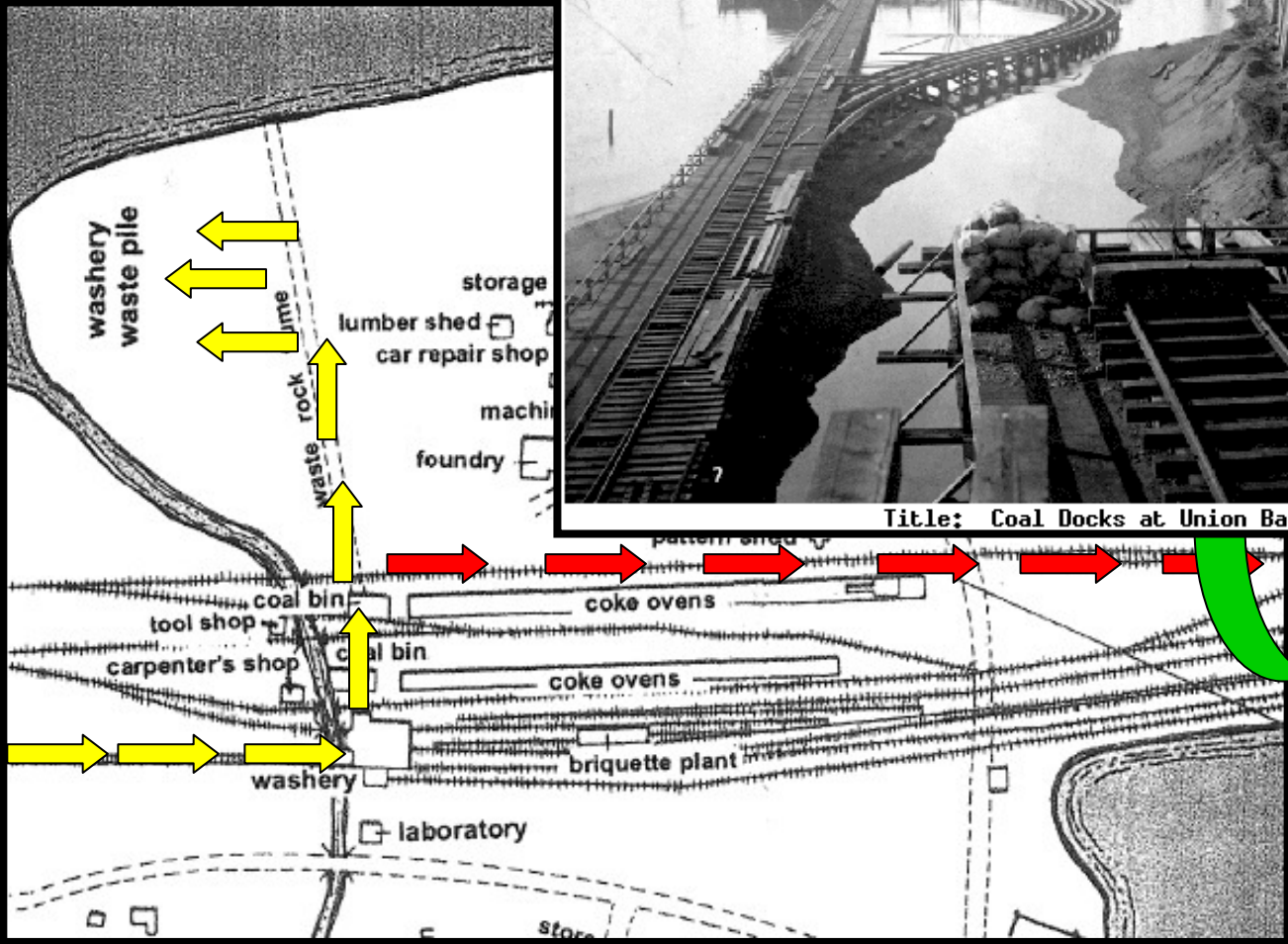
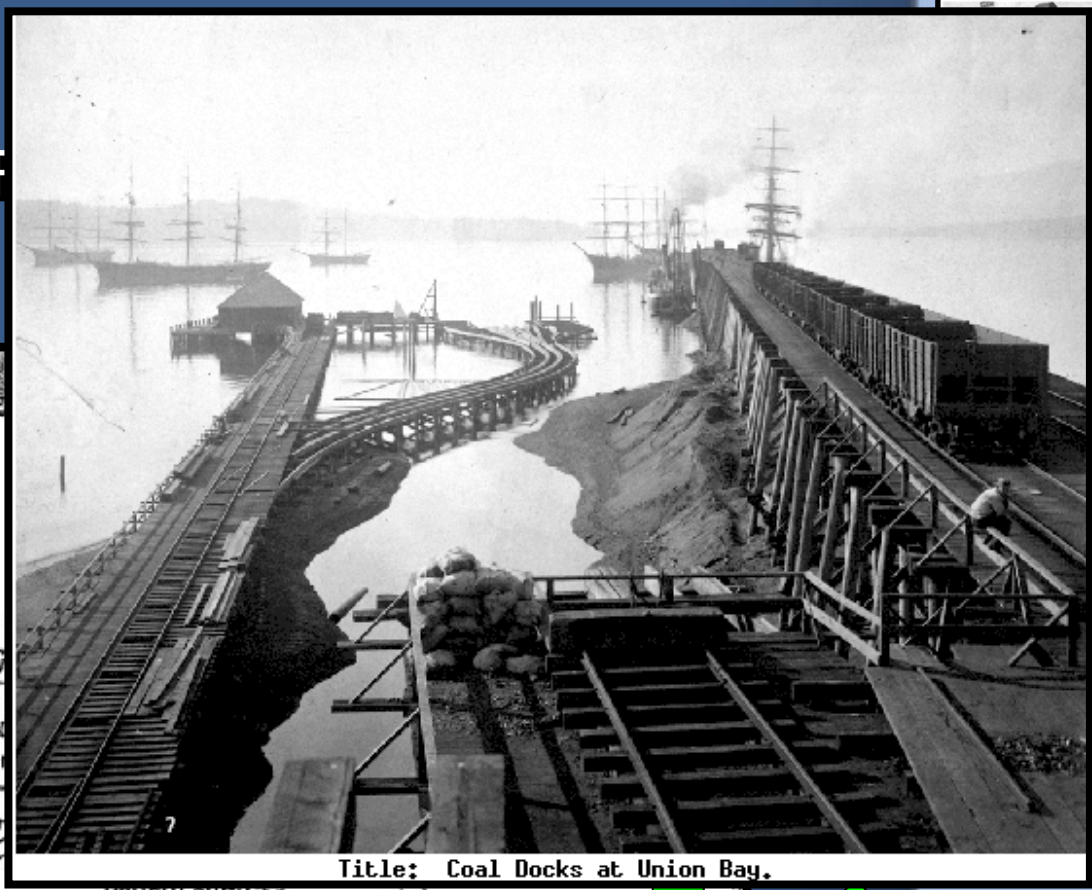


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Site History

- Coal Processing Facility
- 1888 to ~ 1960



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Environmental Investigations

- Waste Coal Pile and adjacent properties, Baynes Sound and Hart Creek
- Samples of waste coal, native soil, groundwater, sediment and surface water analysed for PCOCs
- PCOCs include metals, PAHs, sulphate
- ABA, kinetic testing and other geochemical parameters



Waste Coal Pile - Results

- Waste Coal: arsenic, copper, naphthalene and phenanthrene > standards
- Native soils: < standards
- Groundwater: cadmium, cobalt, copper, nickel, zinc and sulphate > standards for aquatic life; PAHs < standards



Hart Creek - Results

- Surface Water: < criteria
- Sediment: PAHs and metals > criteria in 1 sample



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Baynes Sound - Results

- Waste coal present to > 30 m offshore
- Iron staining present in sediments north and east of coal pile in areas of groundwater discharge
- Sediment: PAHs and metals > criteria
- Seep water: Metals > criteria





A 2

WASTE COAL PILE

SW 9

SW 11

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Geochemistry

- Geochemical characterization conducted by SRK Consulting (Canada) Inc.
- Static and kinetic testing indicated that all material is potentially acid generating and some already acidic
- Geochemical Profile
 - Sulphide sulphur present throughout
 - Accumulation of sulphate within top 2 m
 - Increasing pH and NP with depth
- Under existing conditions, acidification expected to continue for decades to a century



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Detailed Hydrogeology Assessment – Phase 1

- Stratigraphic characterization
- Groundwater chemistry
- Hydraulic Conductivity Tests
- Analysis of tidal effects/gradients
- Groundwater flow assessment
- Infiltration tests at pile surface
- Climate data evaluation
- Numerical modelling (HELP)
- Detailed evaluation of water balance
- Conceptual hydrogeological model



Phase 1 Conclusions

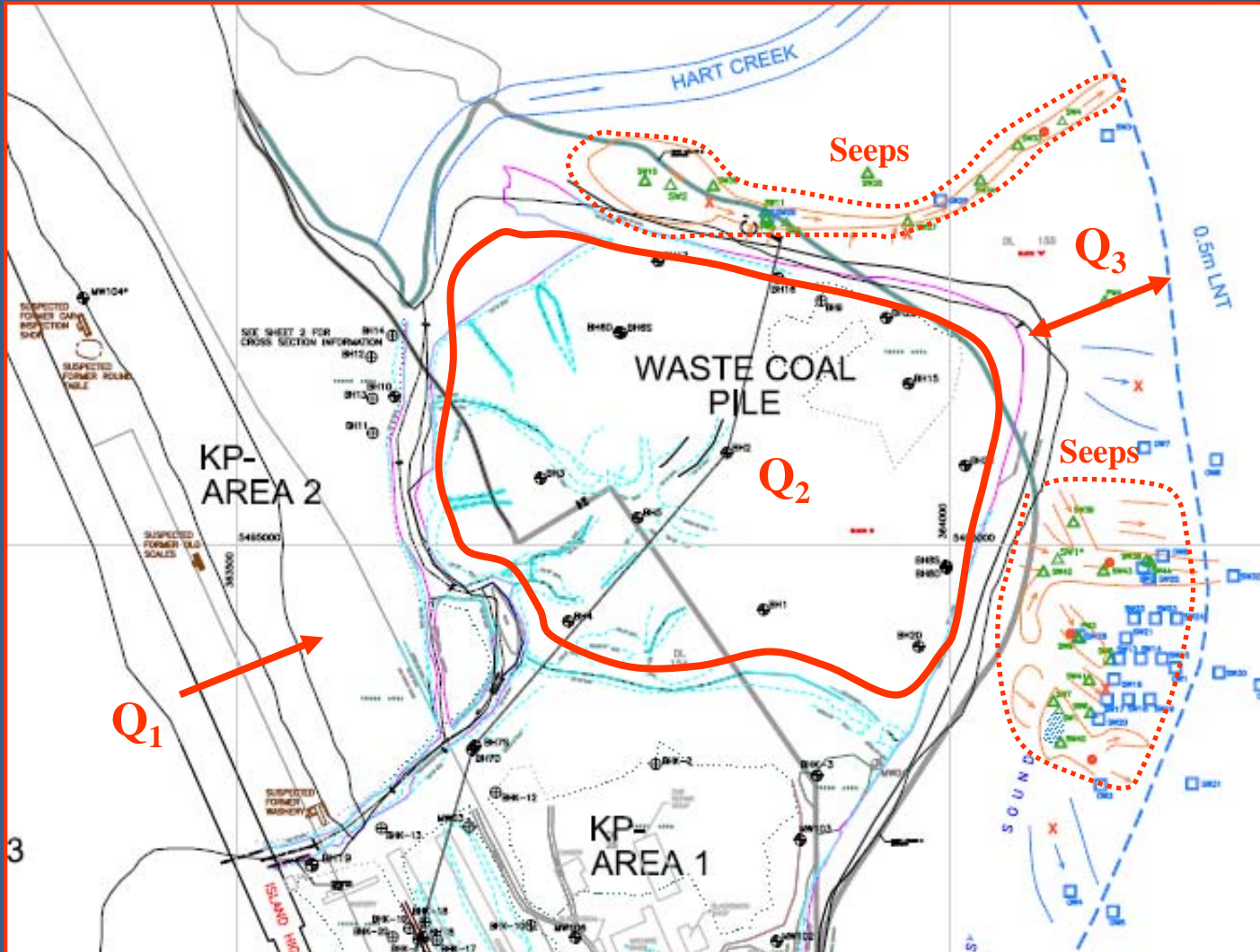
- Waste coal hydraulic conductivity an order of magnitude higher than underlying native soil; promotes seepage at base of pile
- Upgradient side of pile not recharged by Hart Ck.
- Tidal influence extends to back of pile, however mixing of groundwater with saline water limited to 20-75 metres inland from foreshore
- Upgradient groundwater flow through pile is a relatively small component of overall discharge



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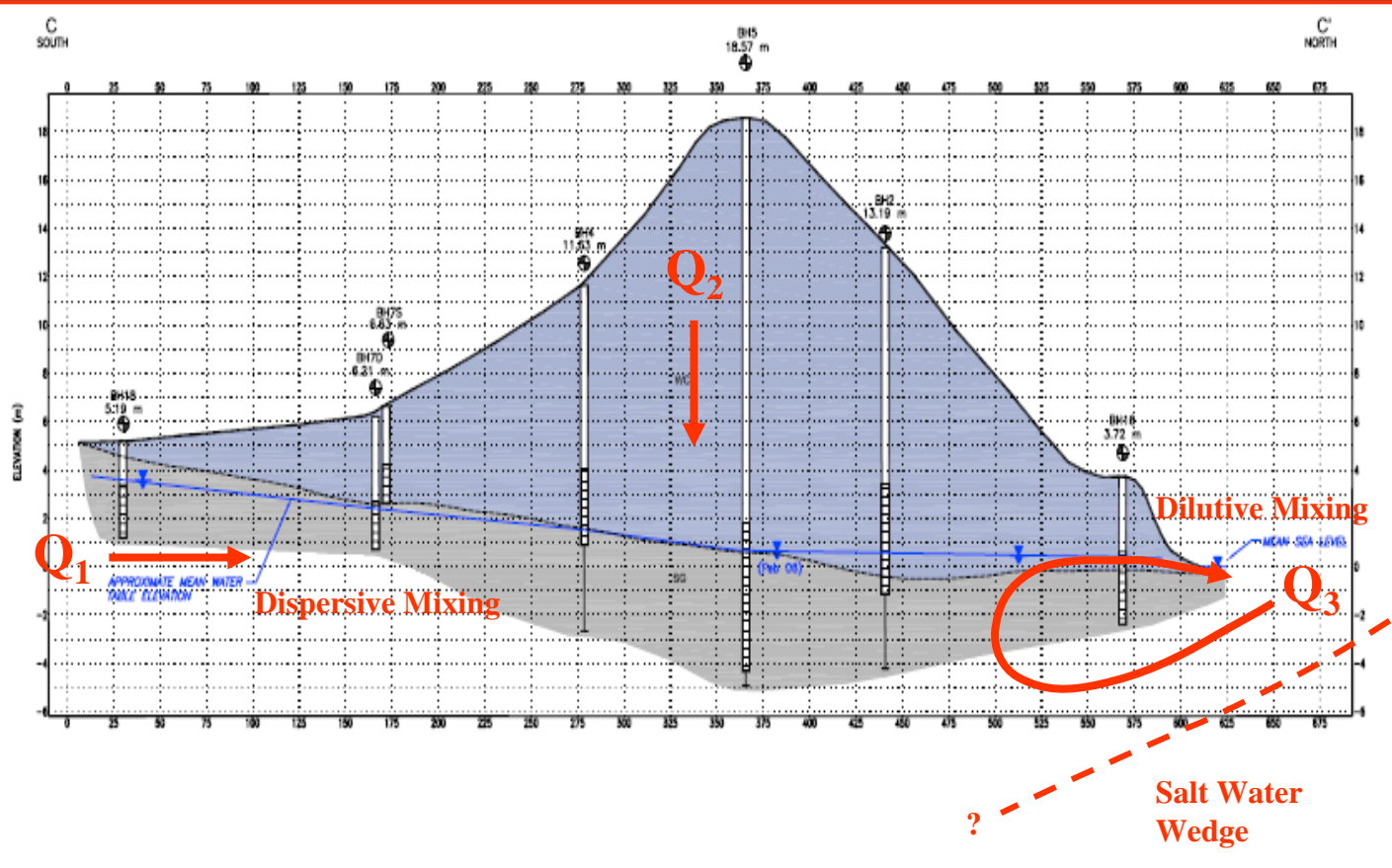
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Conceptual Model



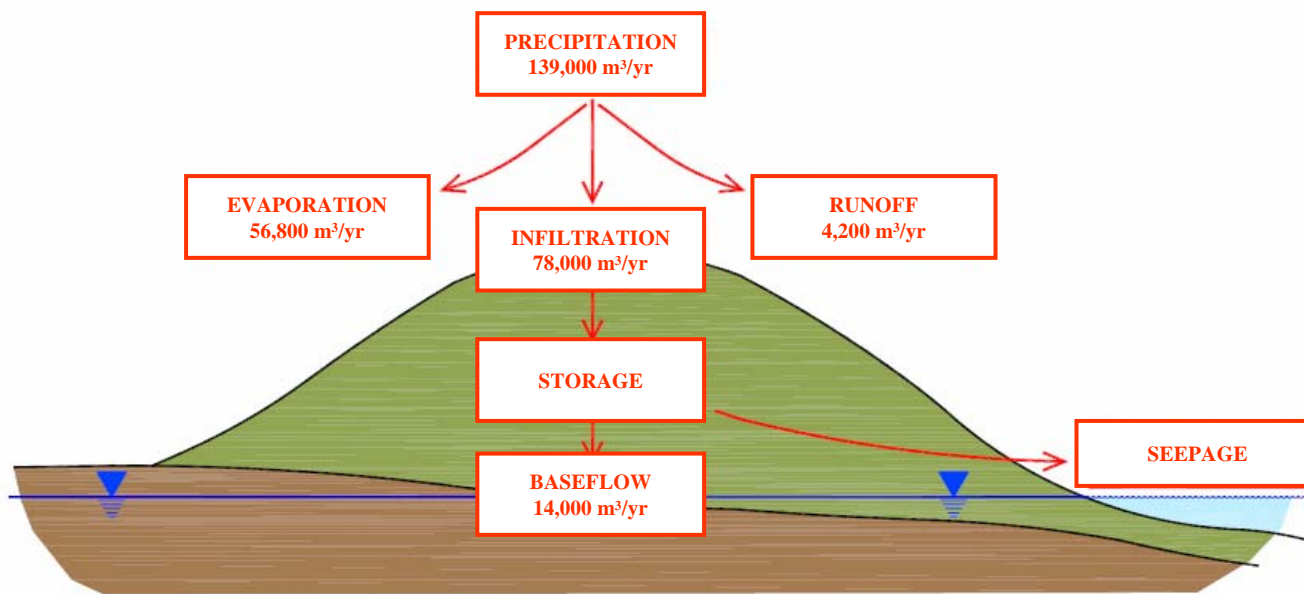
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Conceptual Model



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Water Balance



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Detailed Hydrogeology Assessment – Phase 2

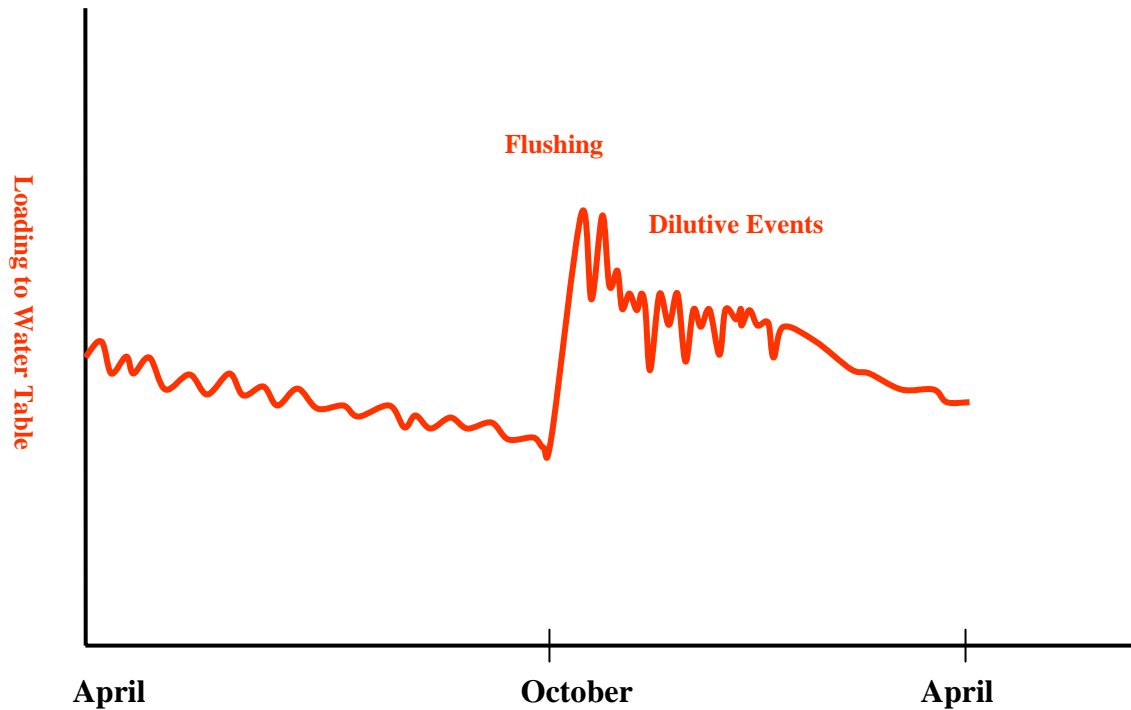
- Literature Review
- Spatial and temporal characterization of seepage chemistry
- Evaluation of seepage flowrates
- Shallow depth porewater profiling in the intertidal zone
- Coastal dispersion modelling
- Seawater dilution evaluation
- Update conceptual hydrogeological model



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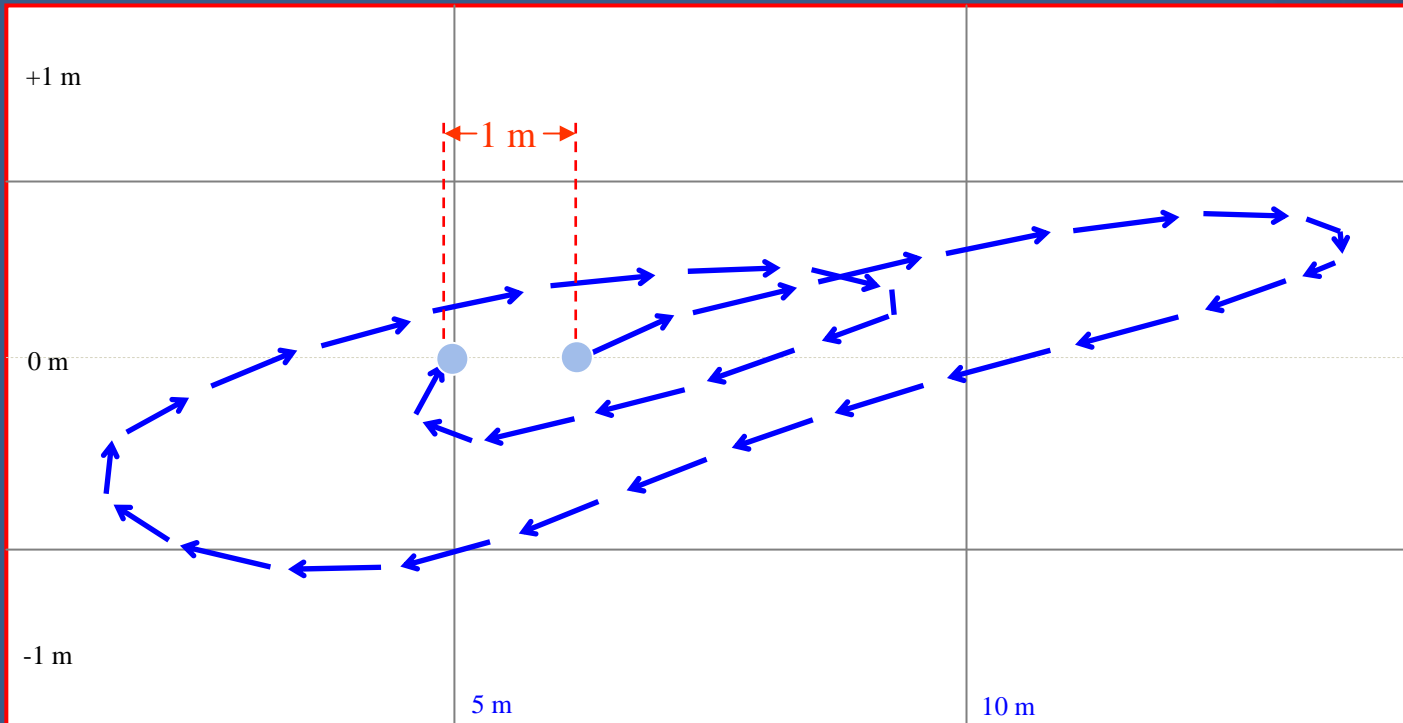
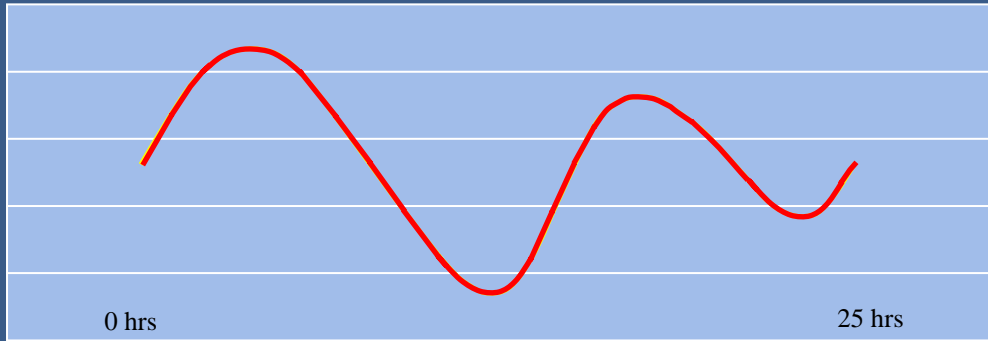
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Conceptual Loadings



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Conceptual Particle Tracking

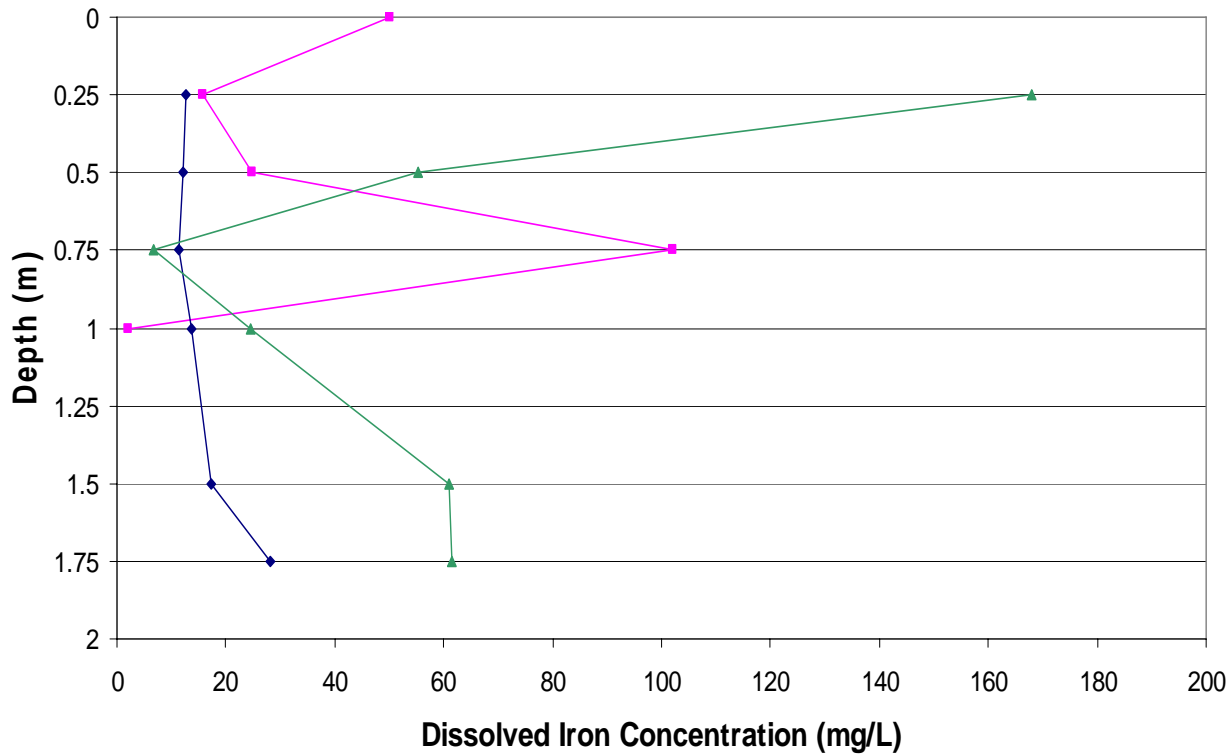


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Porewater Profiling Intertidal Zone



Porewater Dissolved Iron Depth Profiles

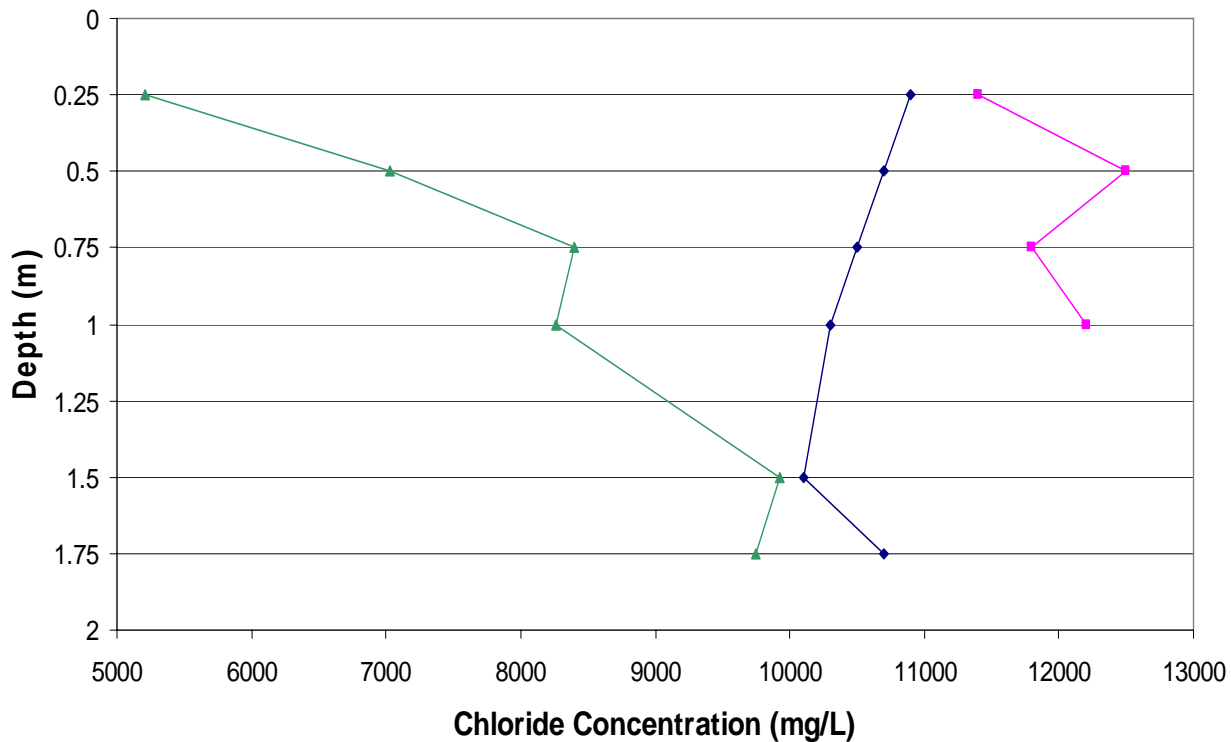


- SW9
- NE PT
- SW11

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Porewater Profiling Intertidal Zone

Porewater Dissolved Chloride Depth Profiles



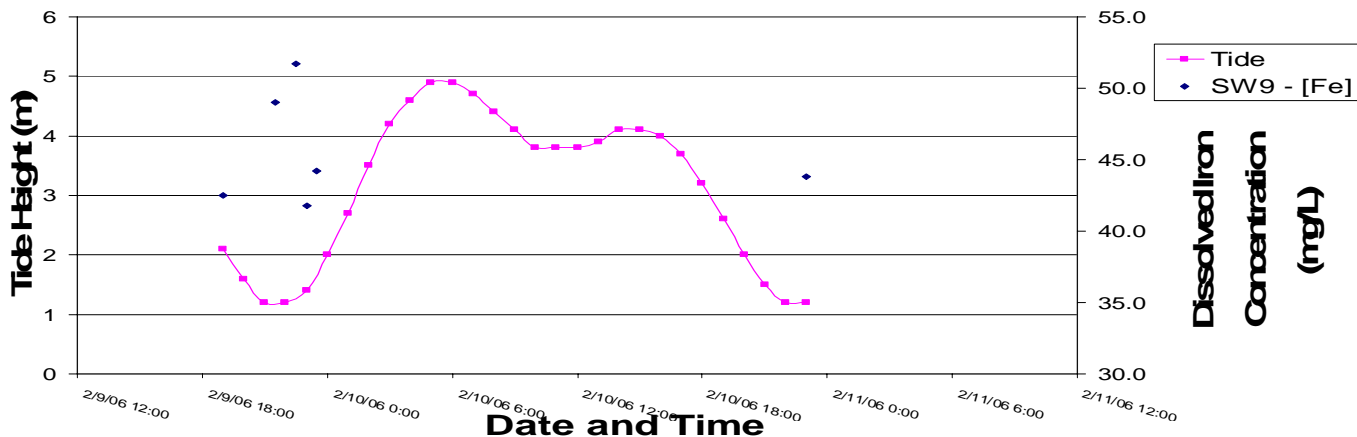
- SW9
- NE PT
- SW11

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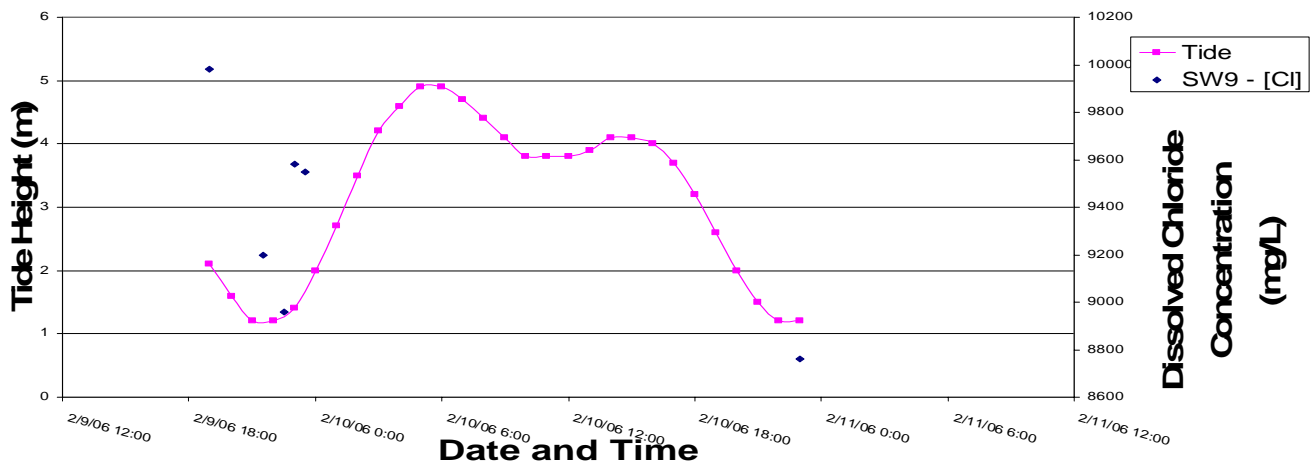
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Iron vs Chloride Seepwater Trend Evaluation

SW9 Dissolved Iron vs Tidal Cycle



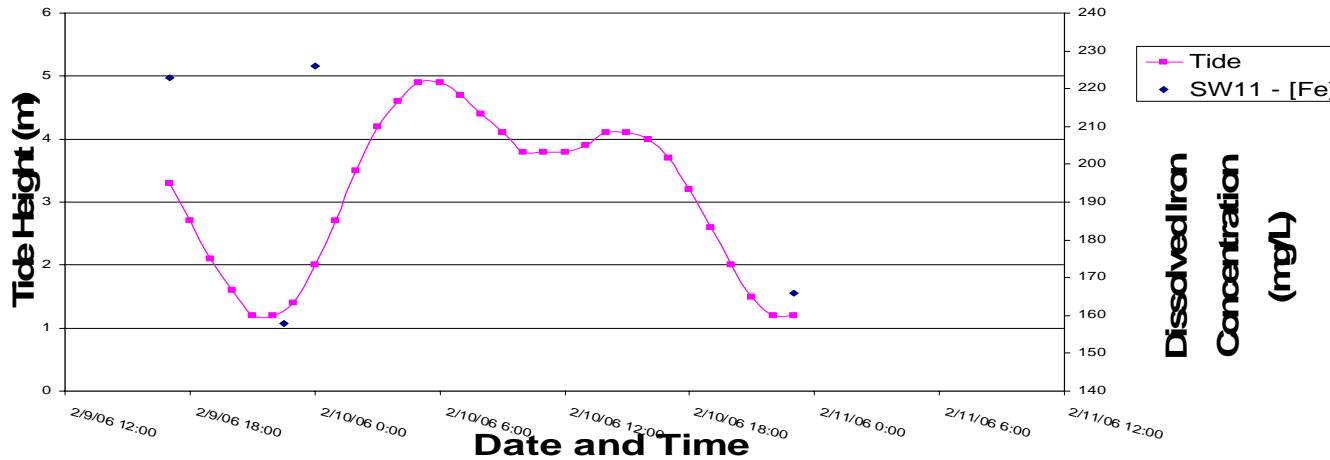
SW9 Dissolved Chloride vs Tidal Cycle



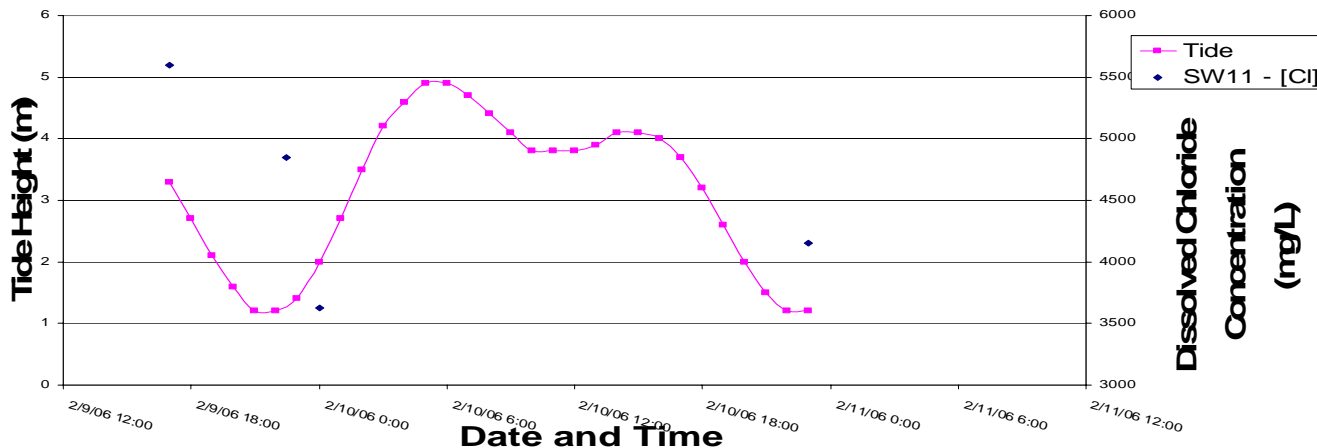
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Iron vs Chloride Seepwater Trend Evaluation

SW11 Dissolved Iron vs Tidal Cycle



SW11 Dissolved Chloride vs Tidal Cycle

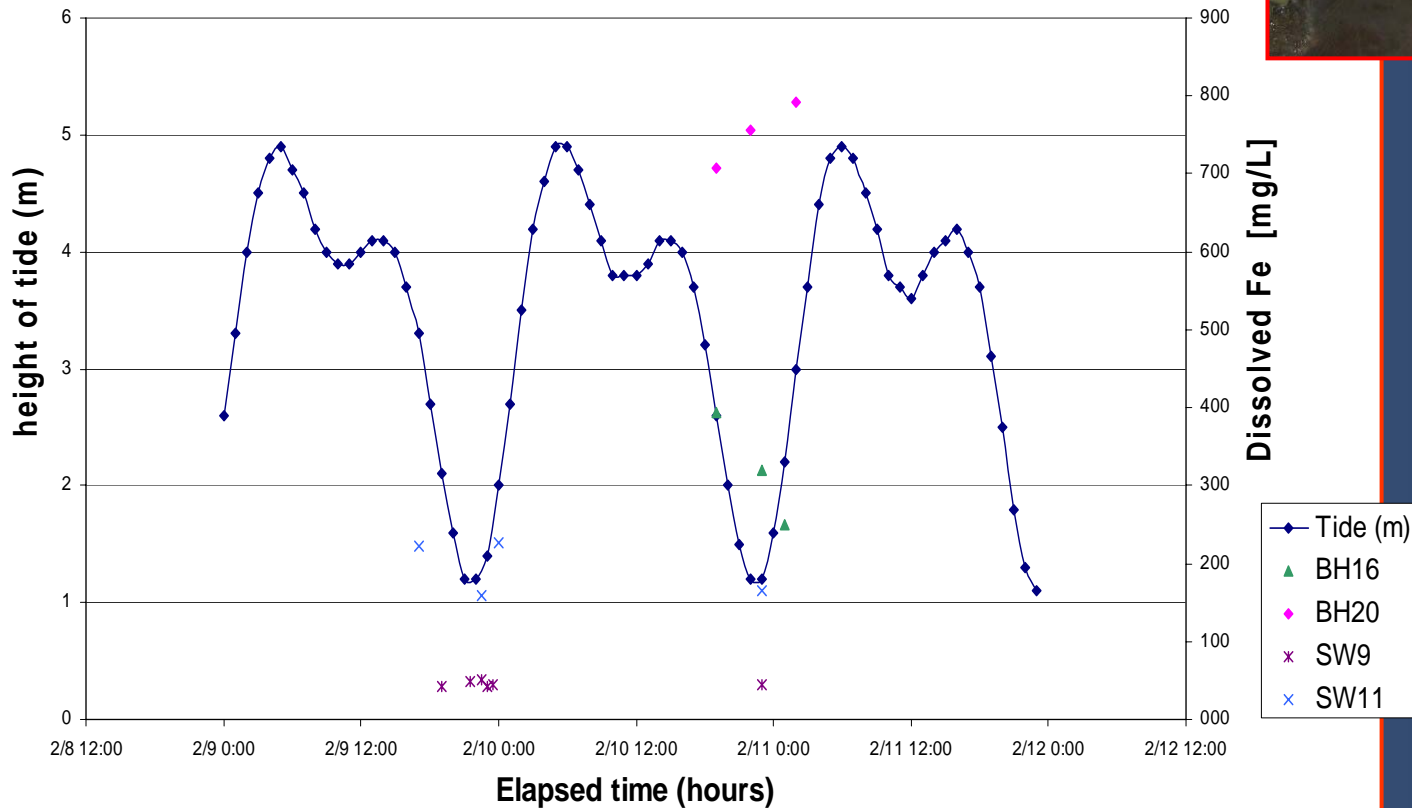


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Groundwater – Seepwater Trend Evaluation



Dissolved Iron Concentration over Tidal Cycle

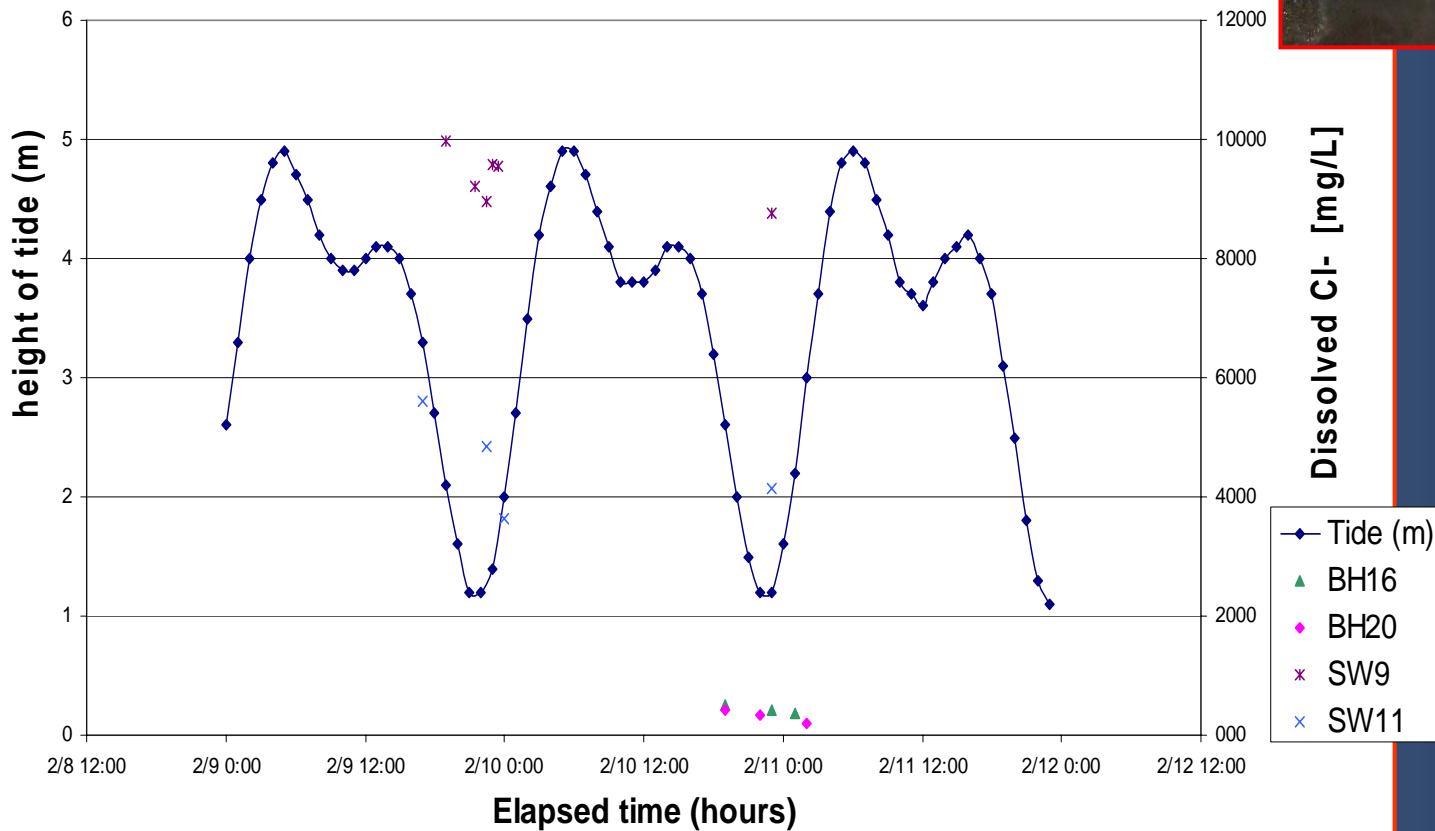


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Groundwater – Seepwater Trend Evaluation

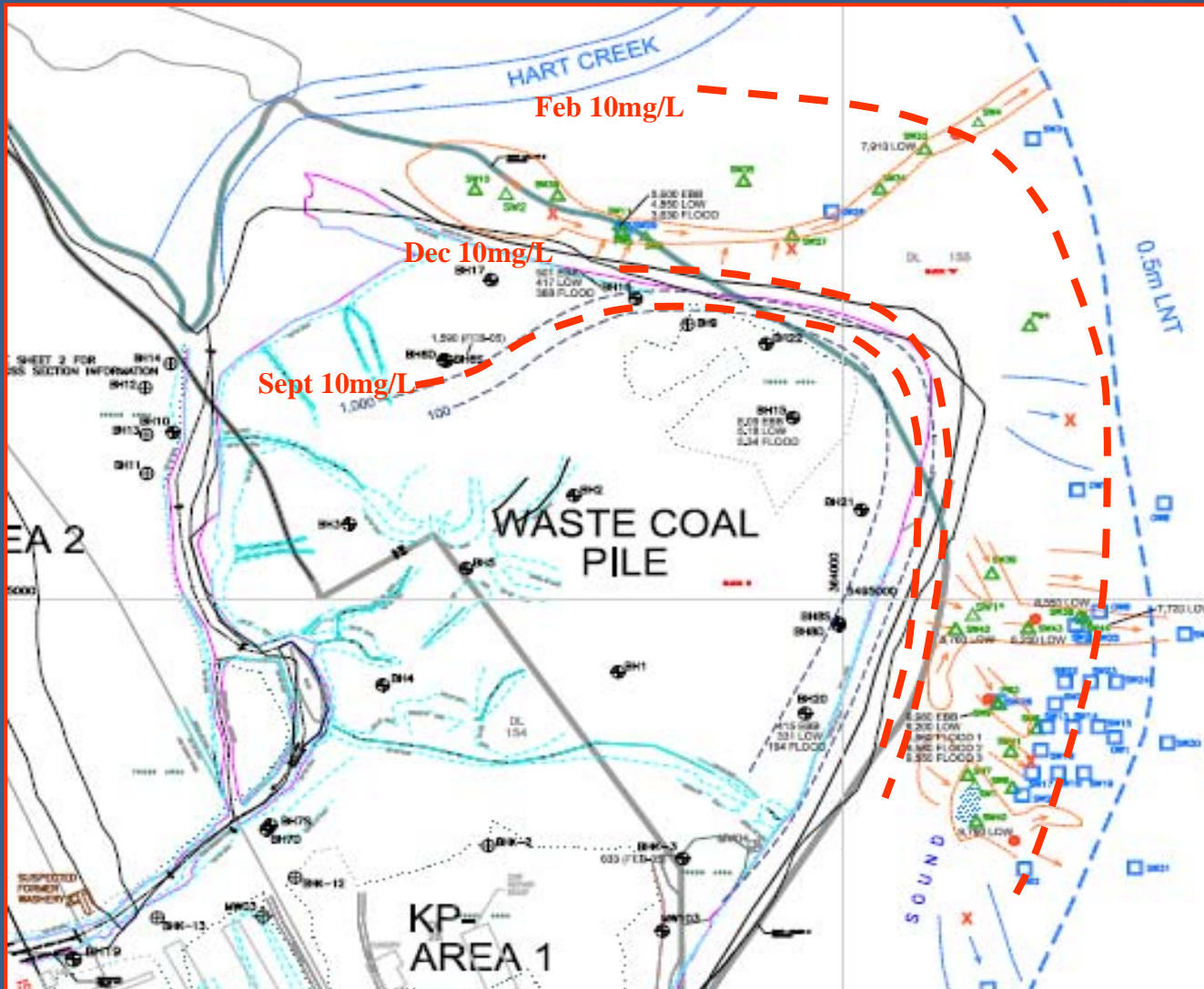


Dissolved Chloride Concentration over Tidal Cycle



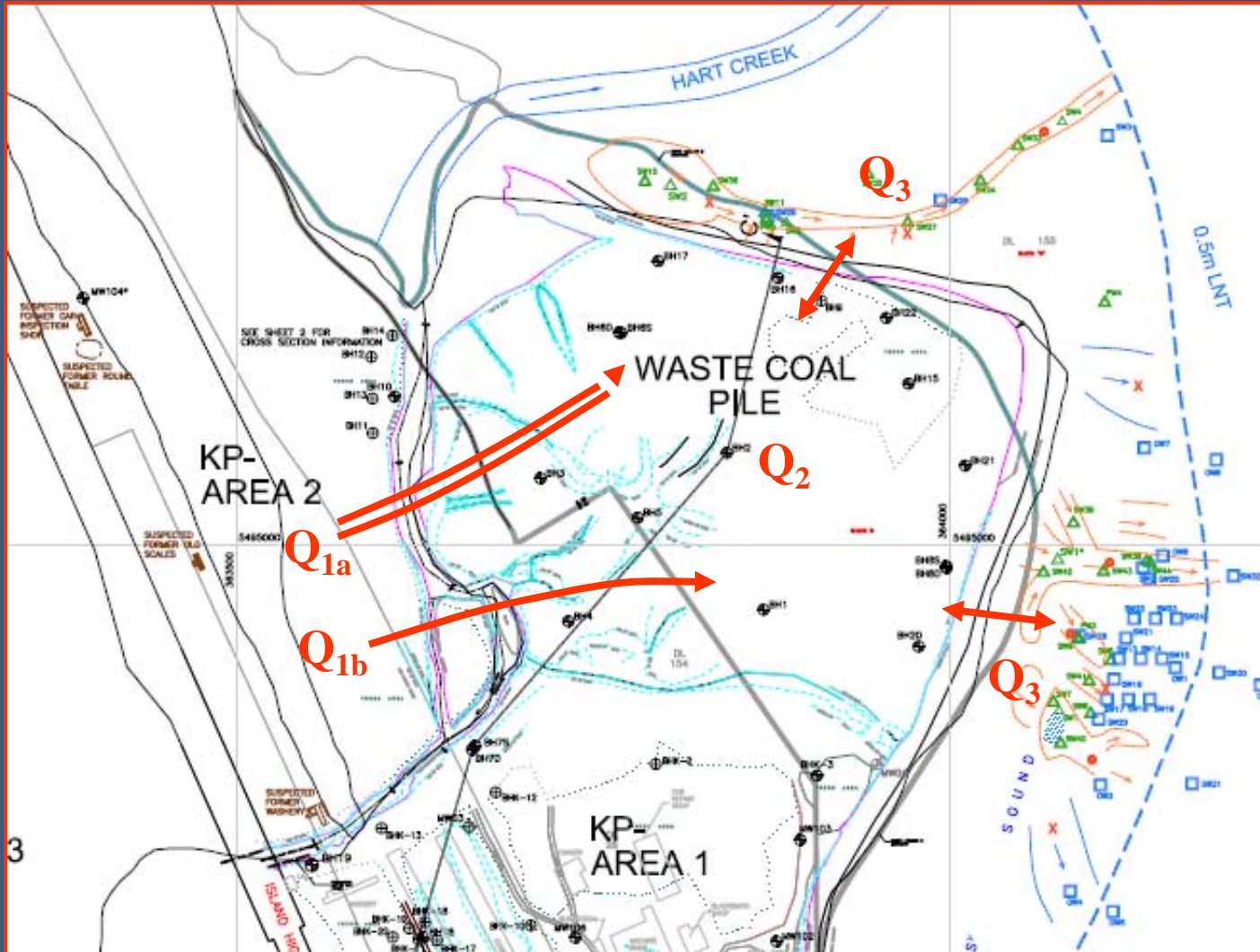
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Seawater Intrusion



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Seawater Intrusion



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Dilution Assessment

Estimated Average Seawater Dilution between Perimeter Wells and Seeps based on Iron Concentrations

Location	Dissolved Fe (mg/L)				
	September 2005	October 2005	December 2005	January 2006	February 2006
BH20	475	400	340	480	750
SW9	110	200	85	30	50
Approx.Dilution	77%	50%	75%	94%	93%
BH16	960	710	265	185	320
SW11	60	45	20	200	170
Approx.Dilution	94%	94%	93%	0%	47%

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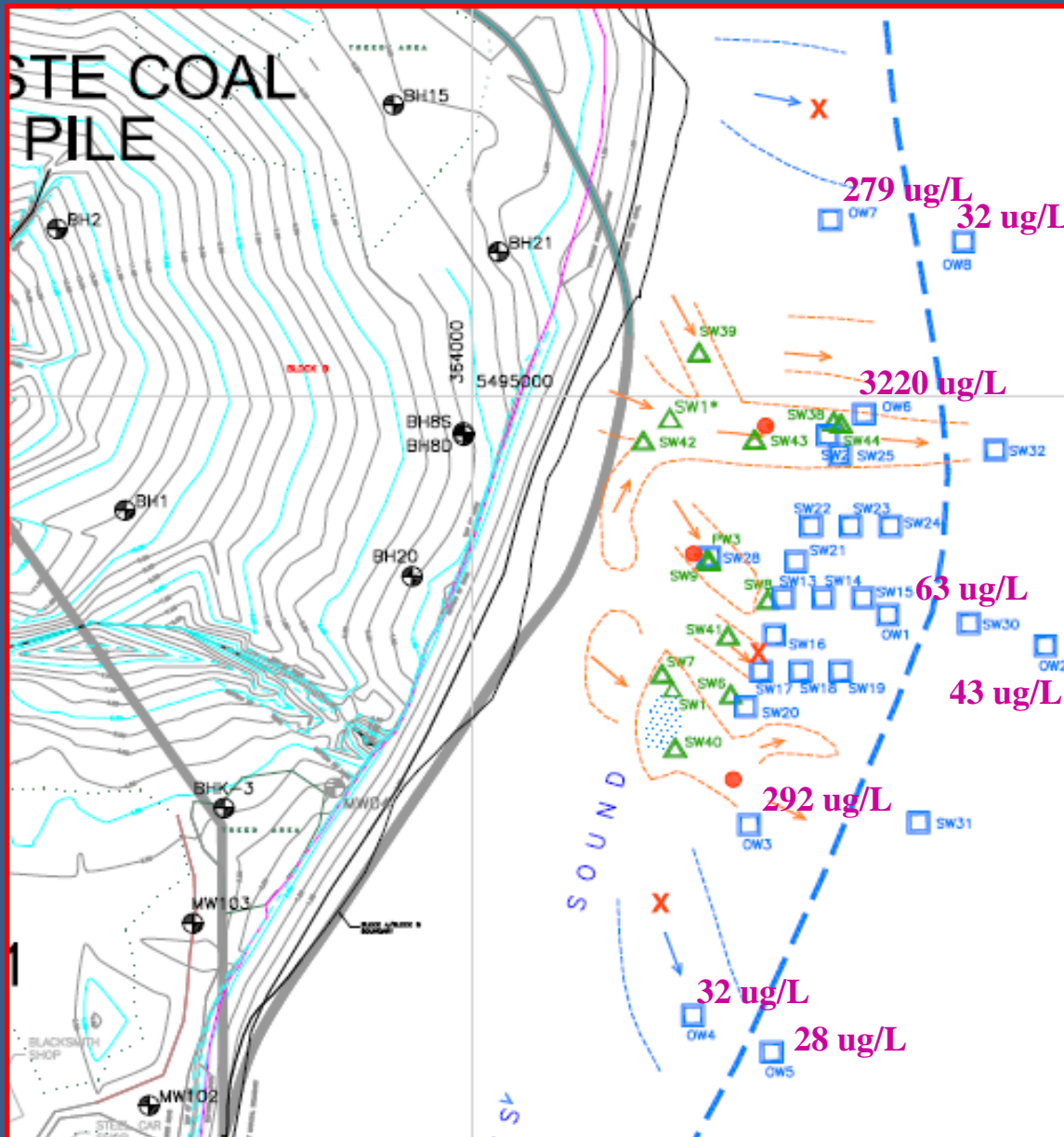
Dilution Assessment

Estimated Average Seawater Dilution between Pile and Seeps Based on Water Balance Method

Location	Combined Seepage Measured Flow Rates (L/sec)	Estimated Total Annual Seepage (m ³ /yr)	Estimated Pile Groundwater Discharge (m ³ /yr)	Approx. Dilution by Seawater
North Face	17.0	490,000	78,000	84%
East Face	9.2			
Spatially Distributed	5.0			

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Ocean Water Results – Feb 2006



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Coastal Dispersion Modeling

- Surface water dispersion model (Lam et al., 1994) used to examine behavior of Fe in Baynes Sound
 - Used to identify distance from and along shoreline from seepage discharges with Fe concentrations > 300 $\mu\text{g/L}$

Table A. Results of coastal dispersion model runs at Union Bay.

Parameter	Run 1	Run 2	Run 3
M_o ($\mu\text{g/s}$)	629,000	629,000	629,000
k (1/s)	0.00019	0.00019	0.00019
u (m/s)	0.01	0.1	1
E_z (m^2/s)	0.6	0.6	0.6
E_x (m^2/s)	0.2	0.2	0.2
D_x^a (m)	<50	<100	<100
D_z^b (m)	<100	<50	<50

^a Distance from shoreline (m) at which dissolved iron water column concentration falls below 300 $\mu\text{g/L}$.

^b Distance along shoreline (m) from the point of release at which dissolved iron water column concentration falls below 300 $\mu\text{g/L}$.

- Model results indicate rapid reduction of Fe concentrations within 50-100 m from point of discharge (in all directions)
- Close agreement between sampling results and model results

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Phase 2 Conclusions

- Groundwater discharge occurs primarily within the top 1 metre of saturated materials
- Seawater intrusion and mixing with groundwater is highly variable but causes approximately 90% dilution at the pile perimeter on a net annual basis
- Seep flowrate from SW9 and SW11 (combined) is about 6% of the observed seepage discharge
- Groundwater discharge at north side of the pile is approximately twice as high as the east side
- In general, dissolved iron is inversely proportional to chloride concentrations

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Remediation/Reclamation Plan

- Waste coal in 4 different zones:
 - Main pile (reclamation)
 - Hart Creek deposit (rechannelling)
 - Intertidal Zone deposit (no action)
 - Subtidal deposit (no action)



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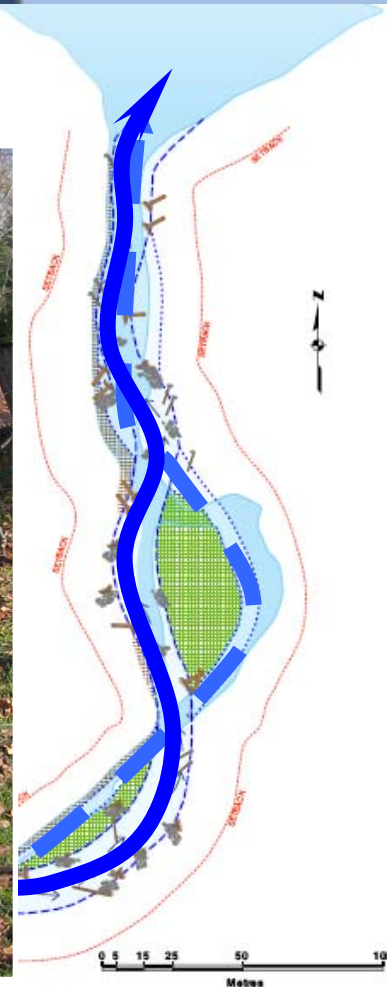
Remediation Plan

- Barrier wall installation around perimeter
- Contaminated soil relocation to pile
- Low permeability cover to reduce infiltration
- Groundwater and leachate treatment as part of ongoing sewage management



Hart Creek Realignment

- 2006 – Hart Creek realigned to reduce erosion of Waste Coal Pile into estuary



Conclusions

- Groundwater concentrations beneath the pile are expected to remain highly variable
- Seepage flow rates are not expected to be significantly reduced
- Seep locations and discharge characteristics may change over time
- To assess future loadings in a meaningful way, data must be evaluated based on net annual trends as opposed to isolated monitoring events so that short term variability is kept within context

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Conclusions

- Permanent remedial solution for Waste Coal Pile
- Greater than 90% reduction in annual contaminant loadings to the environment are expected
- Barrier wall insurable, reduces leachate migration to foreshore
- Deep soil mixing technology is proven on Vancouver Island and elsewhere for improving soil stability
- Post-remedial development will provide economic opportunities for local community

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Thank You

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