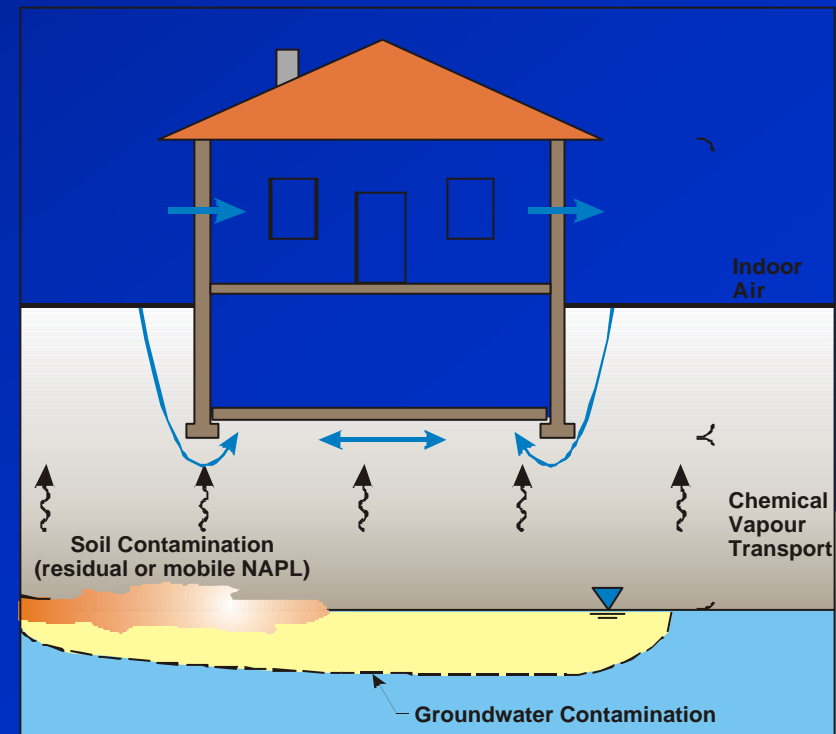


The Subsurface Vapour Intrusion Pathway: Recent Developments for Model Prediction and Empirical Site Data

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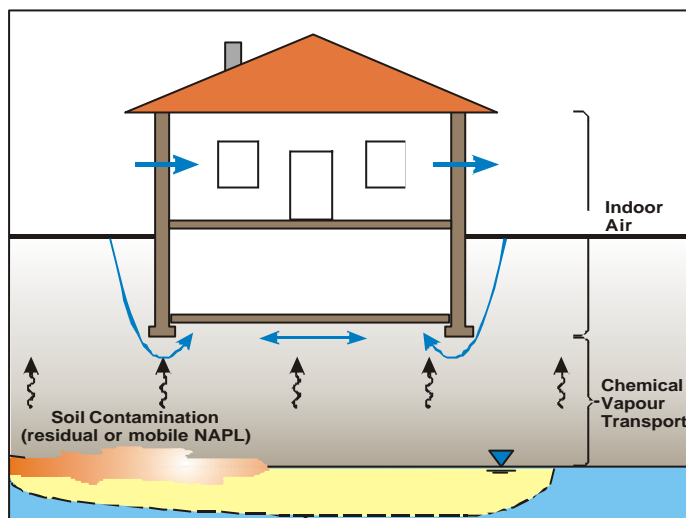
Presentation Outline

- Background Information
- Health Canada Screening Level Risk Assessment Vapour Intrusion Guidance (further to 2003 guidance)
 - Pathway Framework
 - Vapour attenuation factor charts (J&E model)
 - Critical inputs to J&E model (how derived)
 - Validation of model results using empirical data
 - Adjustments to attenuation factors (e.g., biodegradation)
- Conclusions

Background and Key Issues

- Common approach
 - Johnson & Ettinger (J&E) model used to derive regulatory criteria, and for site specific risk assessment
 - Biodegradation and source depletion have in some cases been added to J&E model framework
 - Historically there has been concern over possible conservatism associated with J&E model

Johnson & Ettinger Model



$a = \text{air conc. / vapour conc.}$

Primary Parameters

- D_{eff} = Effective diffusion coefficient
- L_T = Depth to source
- A_B = Building area in contact with soil
- Q_B = Building ventilation rate
- Q_{soil} = Soil gas convection rate
- D_{crack} = Eff. diff. coeff. through cracks
- L_{crack} = Crack thickness
- h = Building crack factor

$$a = \frac{\left[\frac{D_T^{\text{eff}} A_B}{Q_B L_T} \right] \exp\left(\frac{Q_{\text{soil}} L_{\text{crack}}}{D_{\text{crack}}^{\text{eff}} h A_B} \right)}{\exp\left(\frac{Q_{\text{soil}} L_{\text{crack}}}{D_{\text{crack}}^{\text{eff}} h A_B} \right) + \left[\frac{D_T^{\text{eff}} A_B}{Q_B L_T} \right] + \left[\frac{D_T^{\text{eff}} A_B}{Q_{\text{soil}} L_T} \right] \left(\exp\left(\frac{Q_{\text{soil}} L_{\text{crack}}}{D_{\text{crack}}^{\text{eff}} h A_B} \right) - 1 \right)}$$

Secondary Parameters

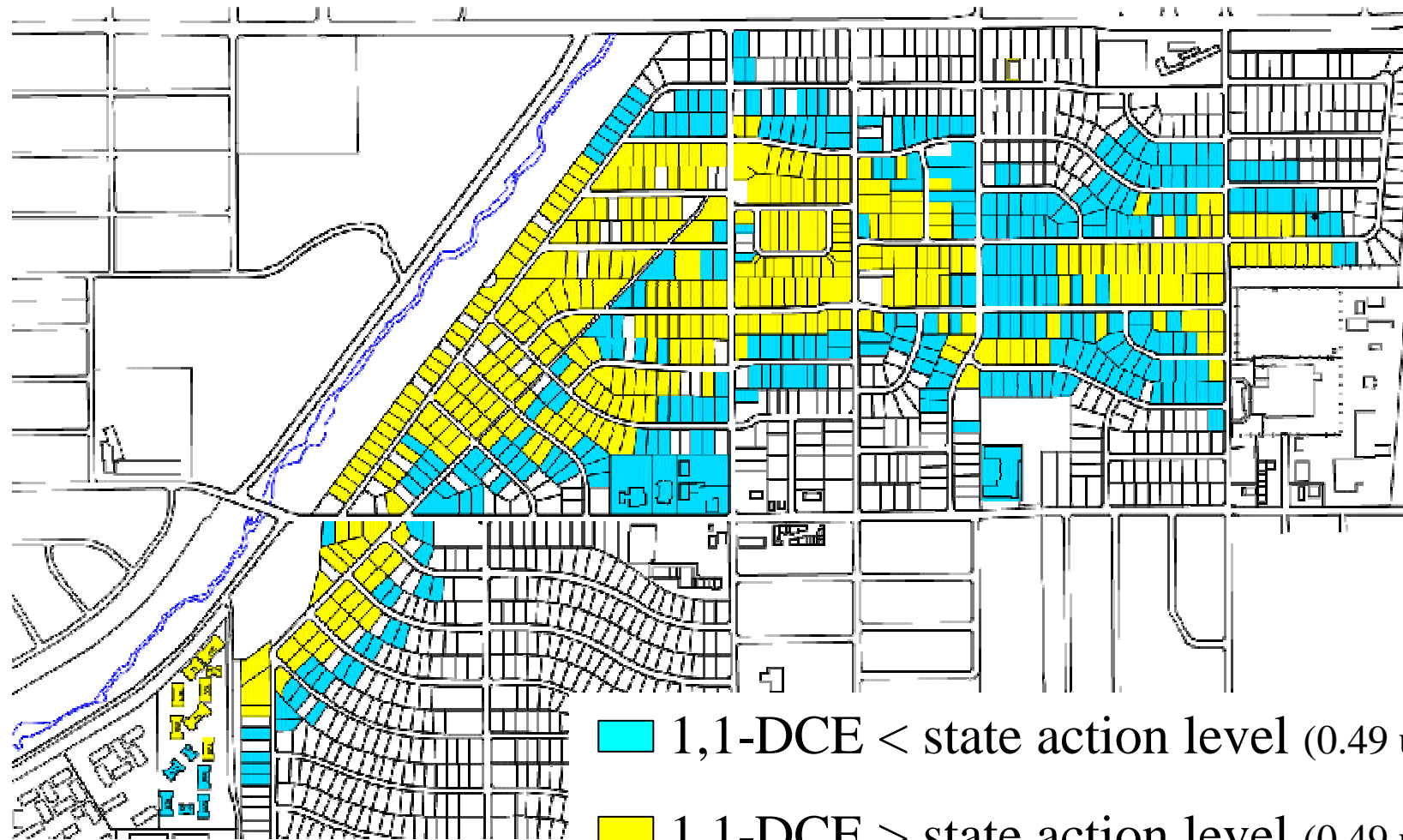
- $D_{\text{eff}} = \text{fn}(H, D_{\text{water}}, D_{\text{air}}, q_T, q_w)$
for each layer
- $L_T = S(L_i)$
- $Q_{\text{soil}} = \text{fn}(k, DP, r_{\text{crack}}, z_{\text{crack}}, x_{\text{crack}})$

$$Q_{\text{Soil}} = \frac{2p \cdot P \cdot k_v \cdot X_{\text{crack}}}{\mu \ln \left[\frac{2 Z_{\text{crack}}}{r_{\text{crack}}} \right]}$$

Background and Key Issues (cont)

- Recent Experience
 - Increasing number of sites where significant vapour intrusion impacts have been documented (the pathway is real!)
 - In a few cases has lead to severe consequences for public reaction, receptor relocation, and/or interim vapor mitigation measures when health risk demonstrated or perceived to be unacceptable
 - Increased regulatory and industry interest in this pathway!

Redfield Site, Denver CO

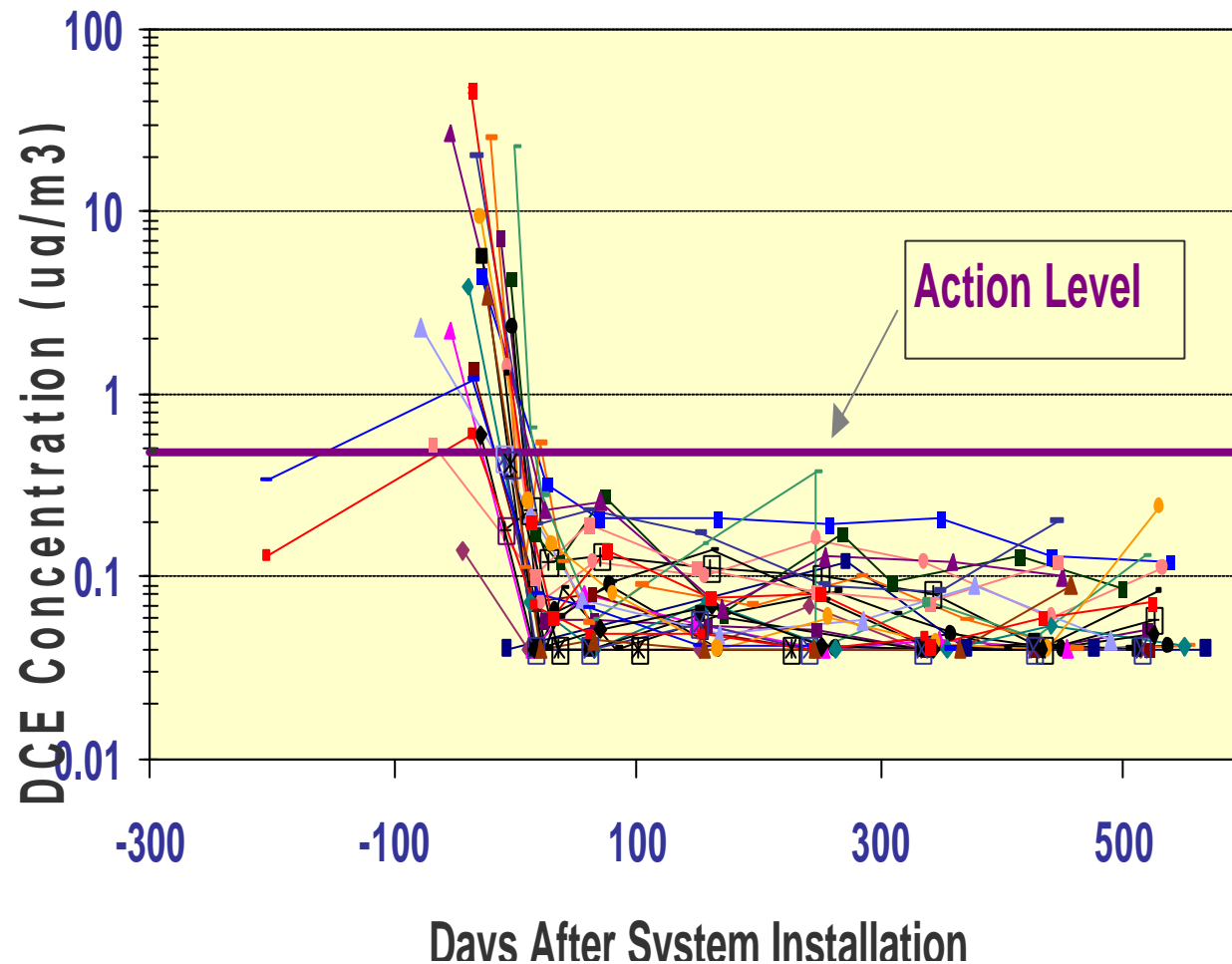


■ 1,1-DCE < state action level (0.49 ug/m³)

■ 1,1-DCE > state action level (0.49 ug/m³)

■ 1,1-DCE > EPA action level (200 ug/m³)

Redfield Site, Subslab Depressurization Performance



DCE_GROUNDWATER vs. DCE_INDOOR AIR (NEAR & MID PLUME APARTMENTS)

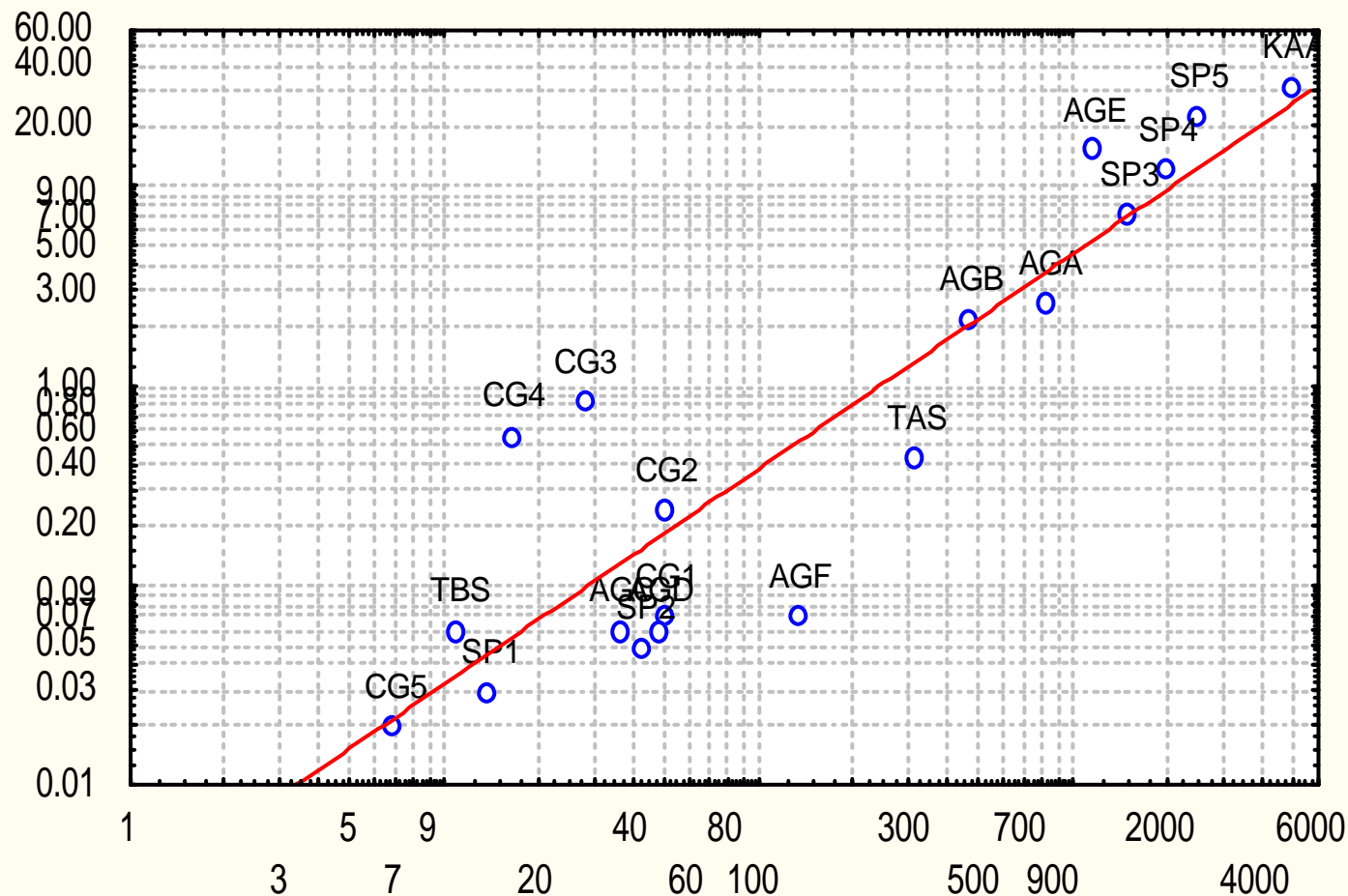
$$\text{DCE_IA} = -.0549 + .00705 * \text{DCE_GW}$$

Correlation: $r = .95977$

DATA THOUGH JAN 1998

CDOT HDQ Site, Denver, CO

DCE_INDOOR AIR (LOGNORMAL ARITH. MEAN) ug/m3



Background and Key Issues (cont)

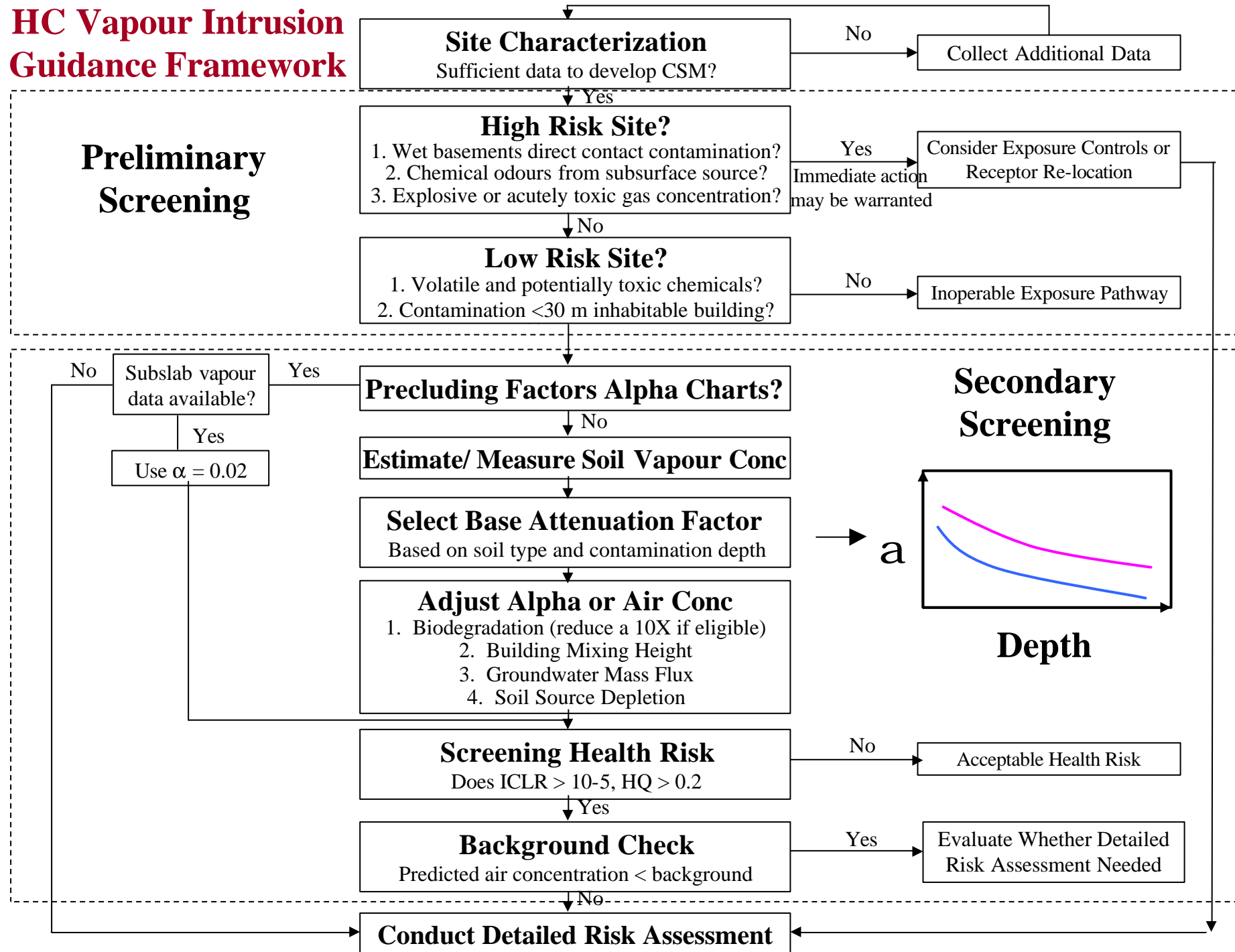
- Challenges
 - Pathway is complex, variable and difficult to model
 - Model predictions can vary several orders of magnitude
 - Model reliability not well characterized (but improving with recent studies)
 - Generic standards/criteria tend to be overly conservative for most sites
 - Site-specific use of model to derive criteria preferable but requires higher level modeling capabilities and appropriate input parameters

Background and Key Issues (cont)

- Recent Developments
 - Tiered framework for site screening using basic site data & modifying factors for more realistic evaluation of vapour intrusion combined with protocol for site-specific use of models (USEPA, Health Canada, BC SAB)
 - Increased use of empirical data to validate models & develop criteria
 - Use of soil vapour data as opposed to soil data
 - Recognition that in some cases subslab vapour and indoor air testing may be warranted
 - Supporting protocols (e.g, API Soil Gas Protocol)



HC Vapour Intrusion Guidance Framework



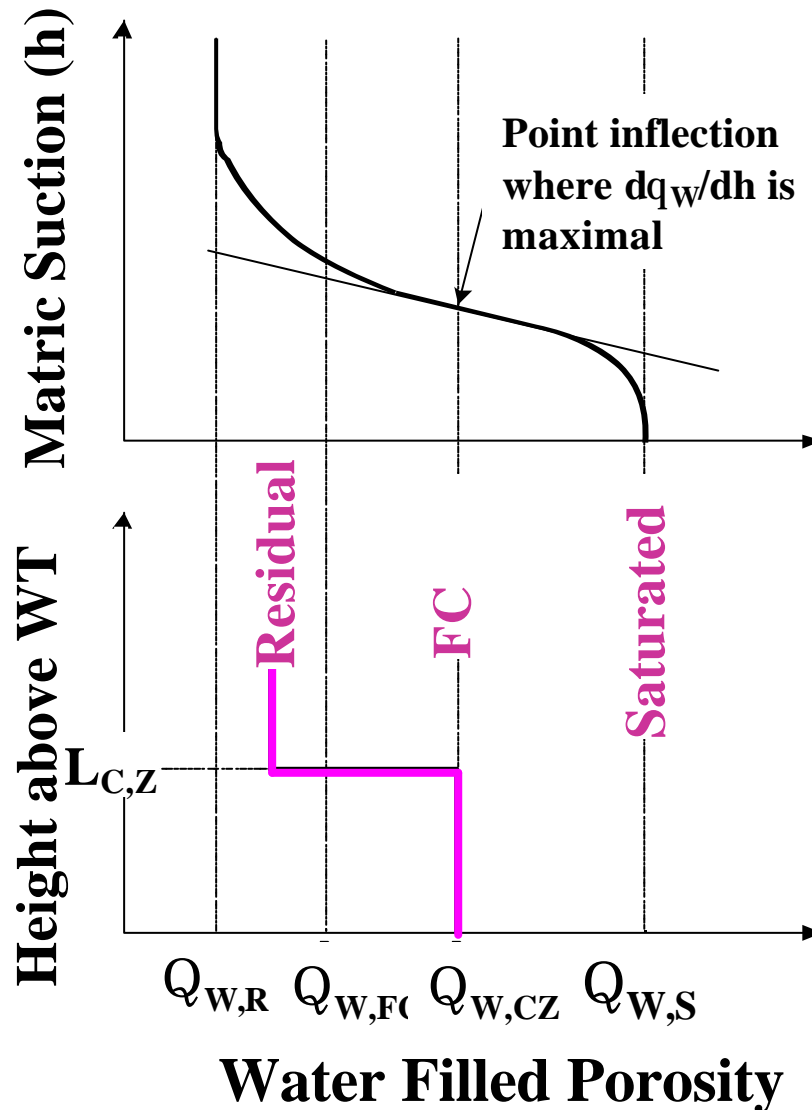
Attenuation Factor Charts

- Derived using J&E model for groundwater-to-indoor air (includes capillary transition zone) and soil vapour-to- indoor air pathways
- Fine- and coarse-grained soil and varying depth to contamination
- Residential (basement) & commercial scenarios (slab-at-grade)
- Factors are for benzene with assumption that properties most chemicals sufficiently similar to benzene
- Model inputs combination typical (average) and conservative values, based on latest science
- Base HC attenuation factors over one order-of-magnitude higher than CCME 2000 CWS-PHC values (why?)

Critical Input Parameters for J&E Attenuation Factor Charts

- Soil Moisture
- Soil Gas Advection (Q_{soil})
- Building air exchange and mixing height

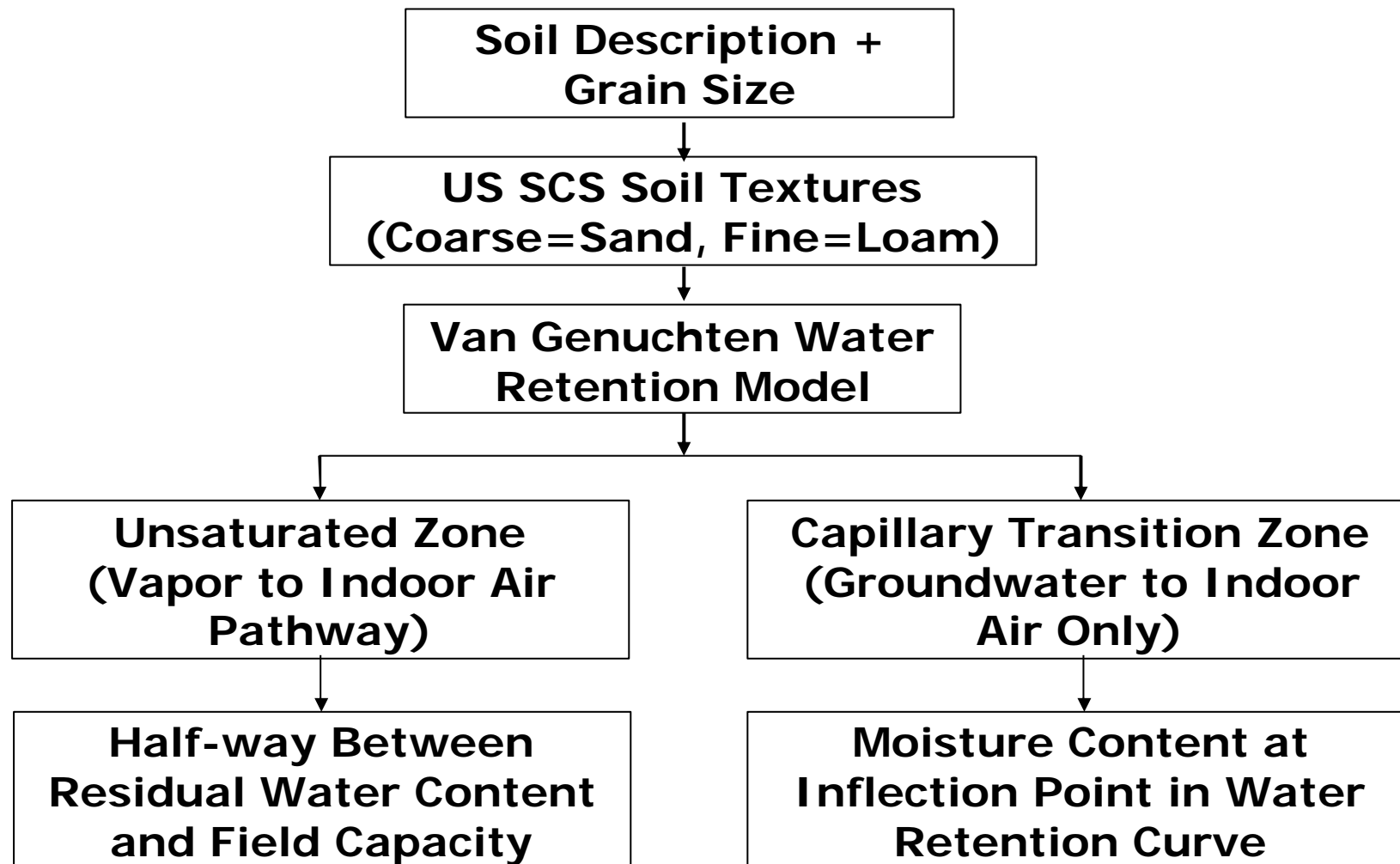
Soil Moisture



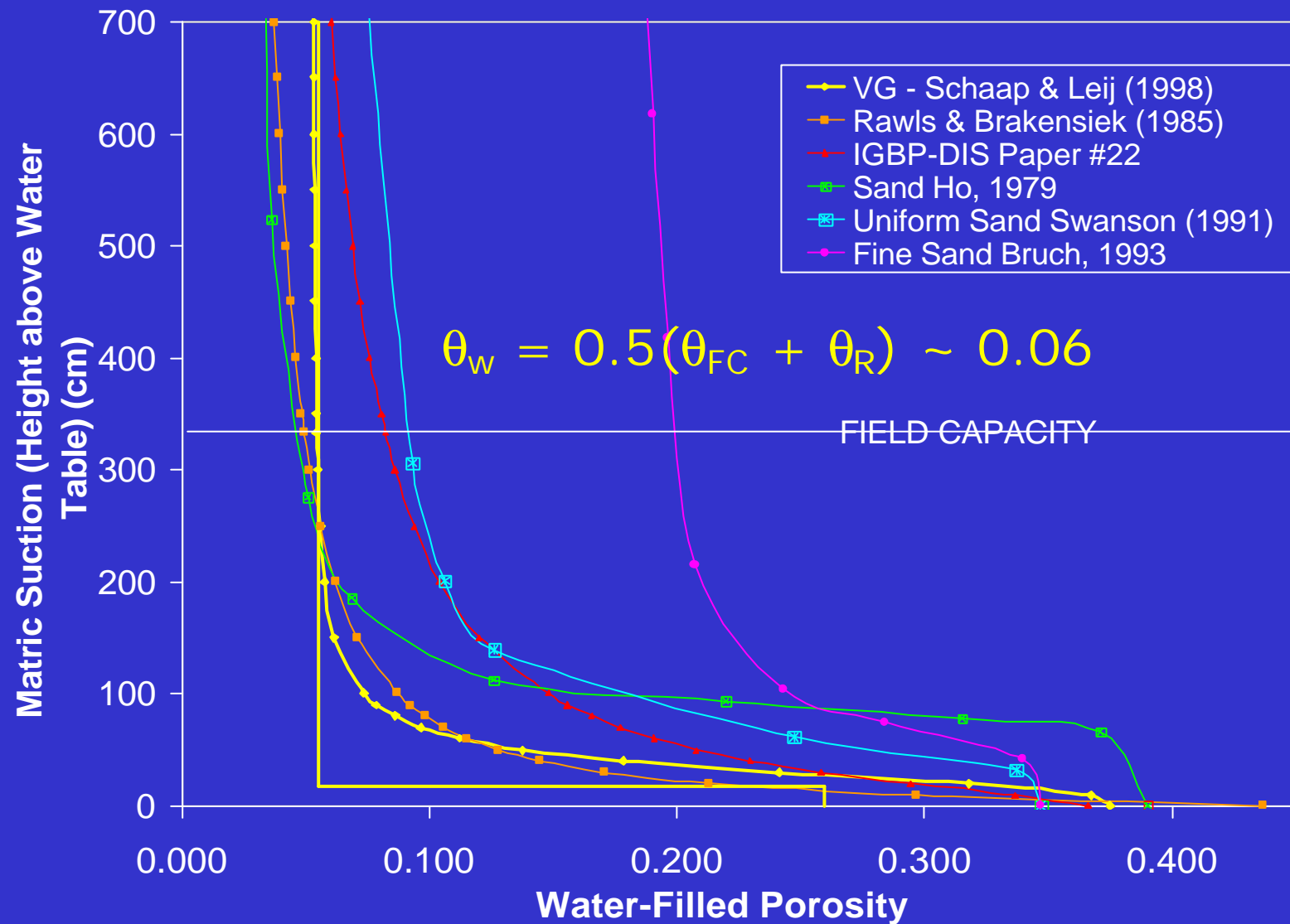
Water Retention Curves
(Van Genuchten model)
for Sand (Coarse-grained)
& Loam (Fine-Grained) -
US SCS Classification

Conceptual
Simplification

Soil Moisture



Comparison Water Retention Factors Sand



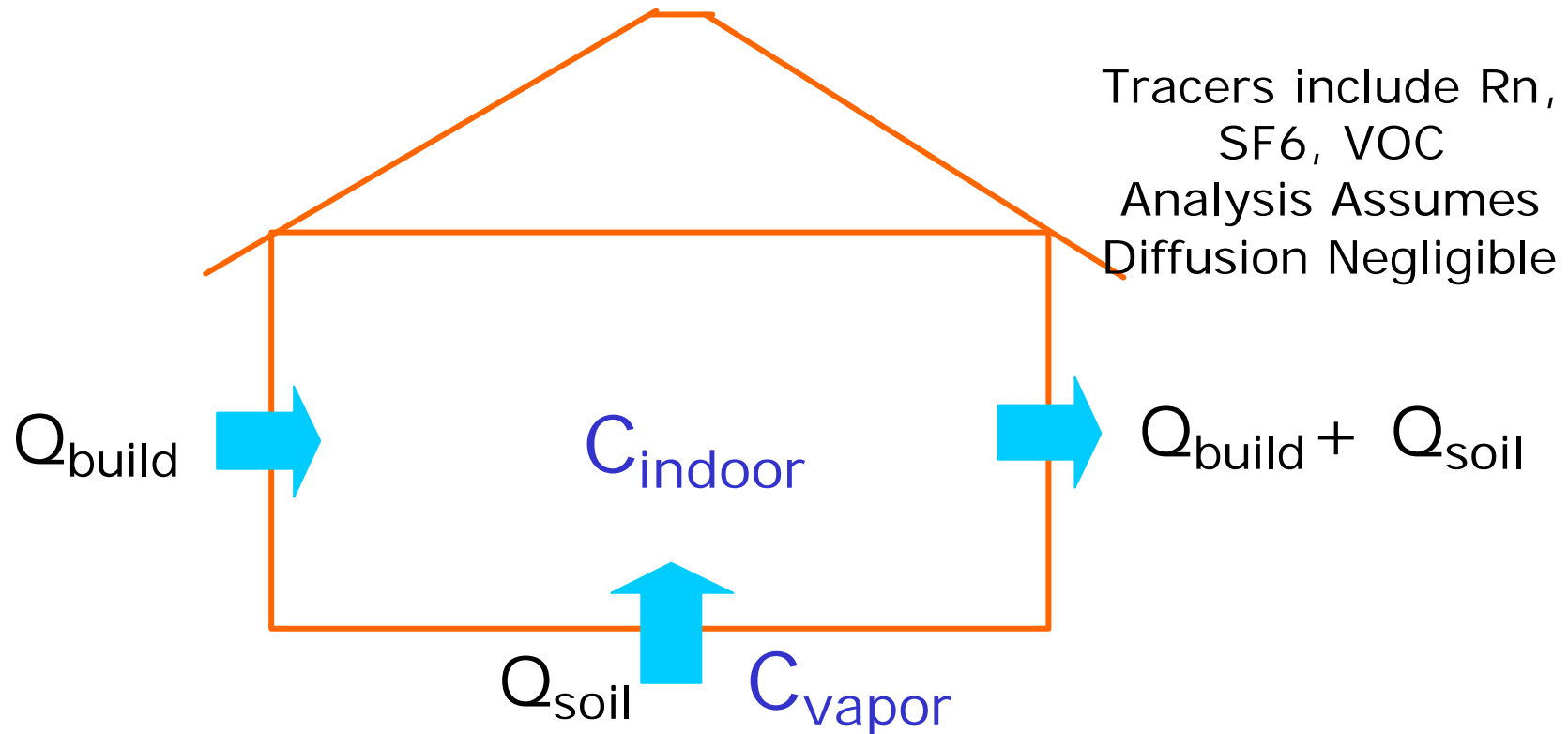
Soil Moisture

- Water retention model for capillary transition zone results in modeled moisture content (MC) that is lower than true MC
- But there is evidence for lateral groundwater flow in capillary fringe (tension saturated zone), also water table fluctuations, therefore upper contamination boundary is above water table
- Analysis involving integration of effective diffusion coefficient suggests effect of:
 - Conservative water retention model and non-contaminated capillary fringe is off-set by ...
 - True water retention model and contaminated capillary fringe & true water retention model off-set by (balancing effect)

Soil Gas Advection (Q_{soil})

- Function ΔP , soil properties (adjacent to foundation!), foundation properties
- ΔP depends on stack effect (indoor/outdoor temperature difference), wind, fan operation, unbalanced return air ducts, insufficient combustion air, fireplace use
- *Stack effect*: Inside building heated (furnace, sunlight on roof), hot air rises, leaves “top of building”, creates ΔP , air enter available openings, which can be doors, windows, subsurface foundation (soil gas!)
- ΔP varies depending on house construction, season and climatic region
- Can estimate Q_{soil} using perimeter crack model (reliability?) or from empirical data (tracer tests)

Q_{soil} Estimated Using Tracer Test



$$\alpha = C_{\text{indoor}}/C_{\text{vapor}} \sim Q_{\text{soil}}/(Q_{\text{soil}} + Q_{\text{build}}) \sim Q_{\text{soil}}/Q_{\text{build}}$$

If know Q_{build} , then can estimate Q_{soil}
Keep in mind tracer test α is for
source directly below building

HOUSE VAPOR INTRUSION TRACER STUDIES

Study	Building	Soil Type	Tracer	ΔP	Q_{soil}/Q_{build}	Q_{soil} (L/min)	$Q_{soil}/Area$ (L/m ²)	$Q_{soil}/Area \cdot \Delta P$ (L/m ² ·Pa)
Olson & Corsi (2001)	House w/basement Paulsboro	Sand, some silt	SF ₆	3.6 to 6.2	0.003 to 0.01	5.8 to 6.7	0.18 (6.2 Pa)	0.03
Mose & Mush- rush (1999)	Houses Virginia	N/A	Radon	N/A	0.003 to 0.02	N/A	N/A	N/A
Hers (Chatterton) (1998)	Experimental Greenhouse	M. Sand	BTX	10 to 30	0.0003 to 0.0006	2.7 to 4.2	N/A	0.005 to 0.01
Fischer et al. (1996)	Small Commercial Building	F. Sand	SF ₆	3	0.0002 to 0.0004	1.4 ¹	0.018	0.006
Garbesi et al. (1993)	Small Experimental Basement	F. Sand	N/A	10	N/A	9.7		0.04
Little et al. (1992)	Houses USA	N/A	Radon	N/A	0.0016 (Avg)	N/A	N/A	N/A
Garbesi & Sextro (1989)	House w/basement	Sandy Loam to Loamy Sand	SF ₆	30	~0.001	67 (Best)	N/A	0.01(Best)
Rezvan et al. (1989)	Houses	Gravel	Rn	N/A	0.0079 to 0.045	17 to 96 ²	N/A	N/A

1 Estimated by Fischer et al (1996) from wind-loading ($Q_{building}$ not available)

2 Estimated using assuming values for house volume (366 m³) and AEH (0.35/hr) ($Q_{building}$ not available)

3 Cyclohexane, MTBE, Pentane, 2,2,4-Trimethylpentane

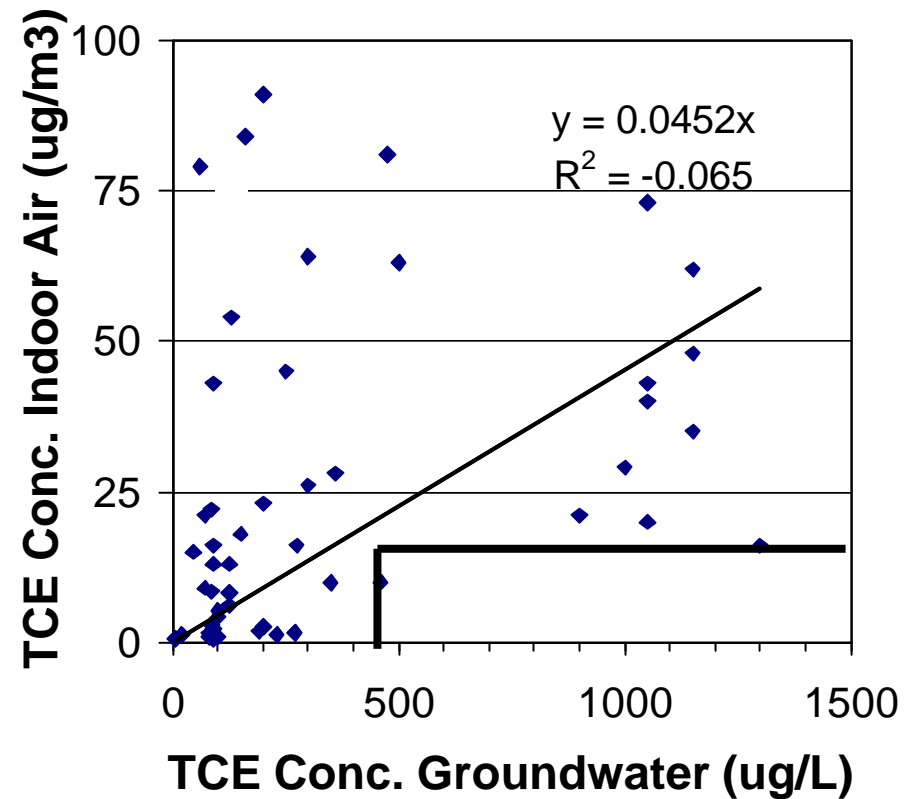
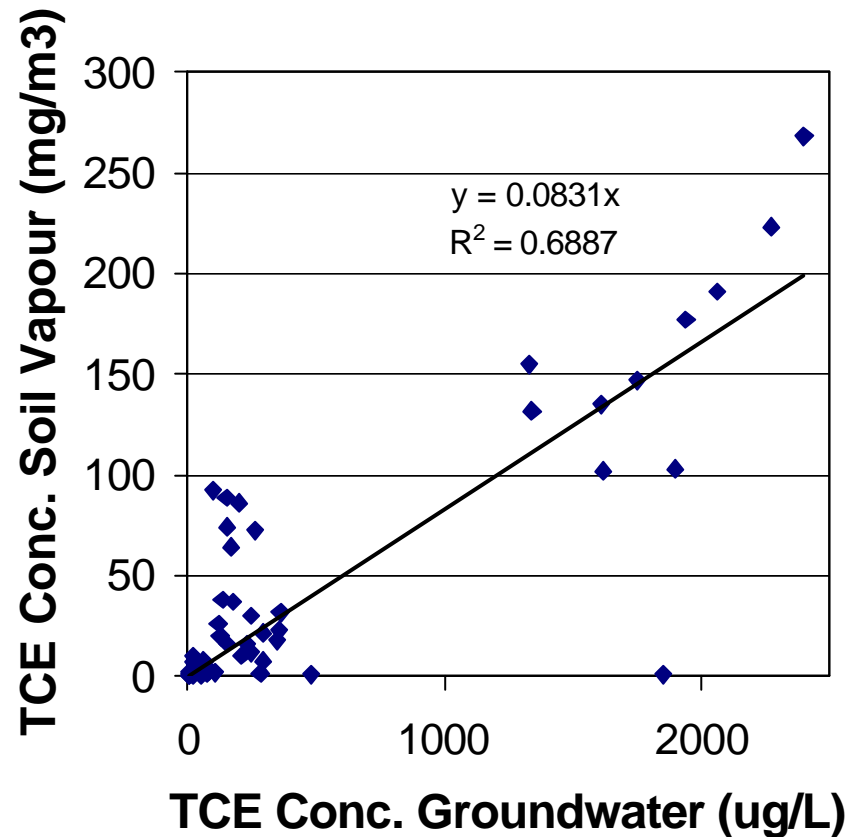
Soil Gas Advection (Q_{soil})

- Sites with coarse-grained soils
- $Q_{\text{soil}}/Q_{\text{build}}$: 0.0002 to 0.02
- Q_{soil} : 1 to 50 L/min (upper range is uncertain)
- $Q_{\text{soil}}/\text{Area} \cdot \Delta P$: 0.005 to 0.04 L/m²-Pa
- Health Canada Guidance
 - $Q_{\text{soil}} = 5 \text{ L/min}$
 - $Q_{\text{soil}}/Q_{\text{build}} = 0.003$

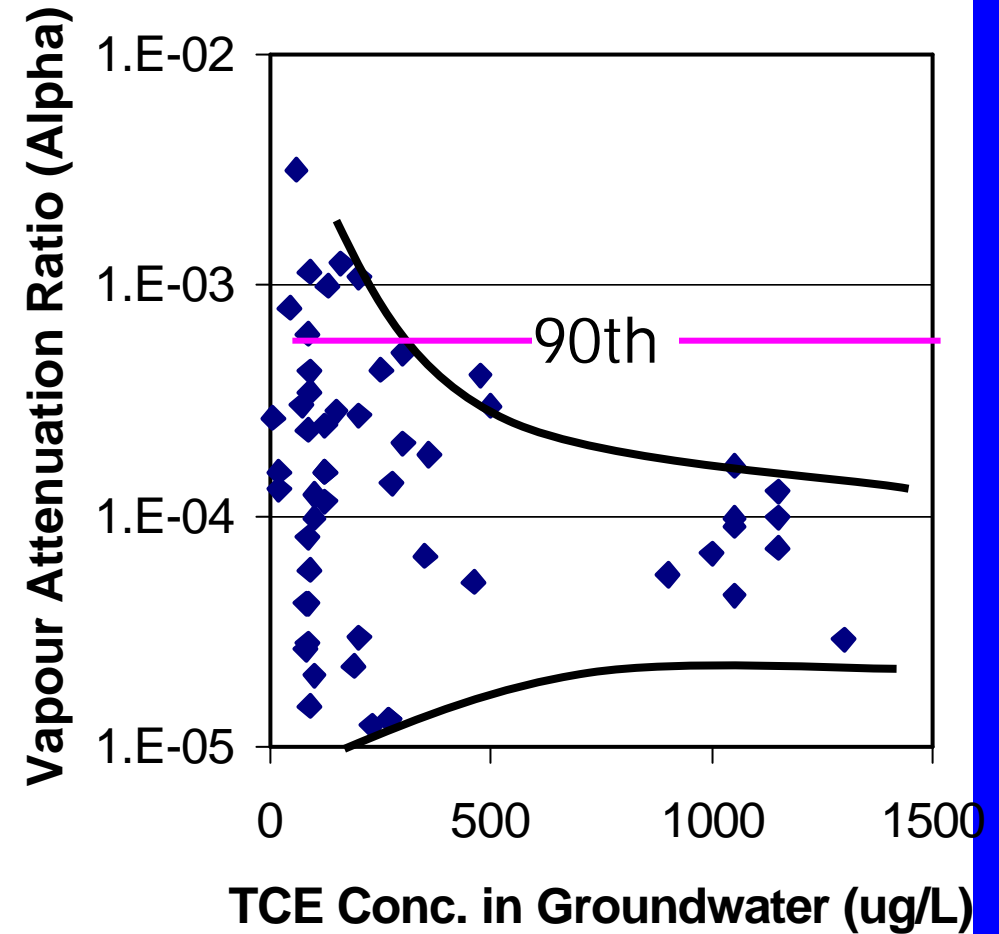
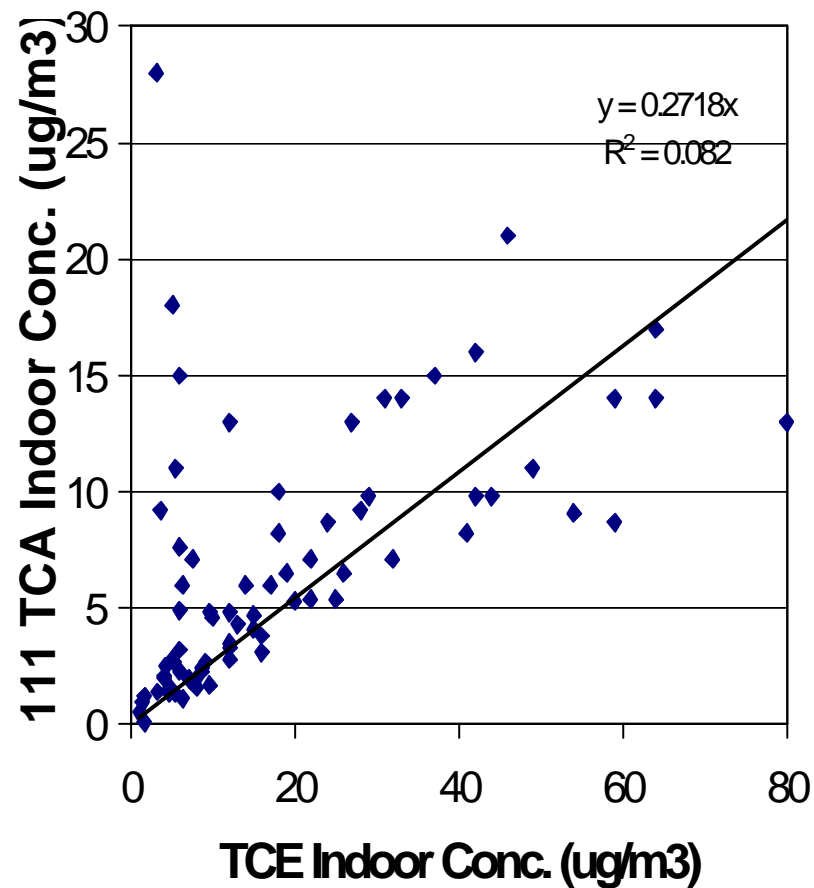
Model Validation Empirical Data

- Empirical evaluation of vapour attenuation factors was important part of guidance development process
- Empirical alpha = measured indoor concentration / interpolated groundwater or soil vapour concentration below house
- Empirical database 36 sites (research, USEPA, projects) ... data quantity & quality vary; several sources of uncertainty
- Prior to use, data was carefully evaluated and screened to remove less reliable data:
 - Evaluate data trends and correlations (“vapour pathway analysis”)
 - Evaluate effect of background VOCs
 - Remove low concentration data
- Use 90th percentile or maximum empirical alpha's for each site since goal is to be protective most sites

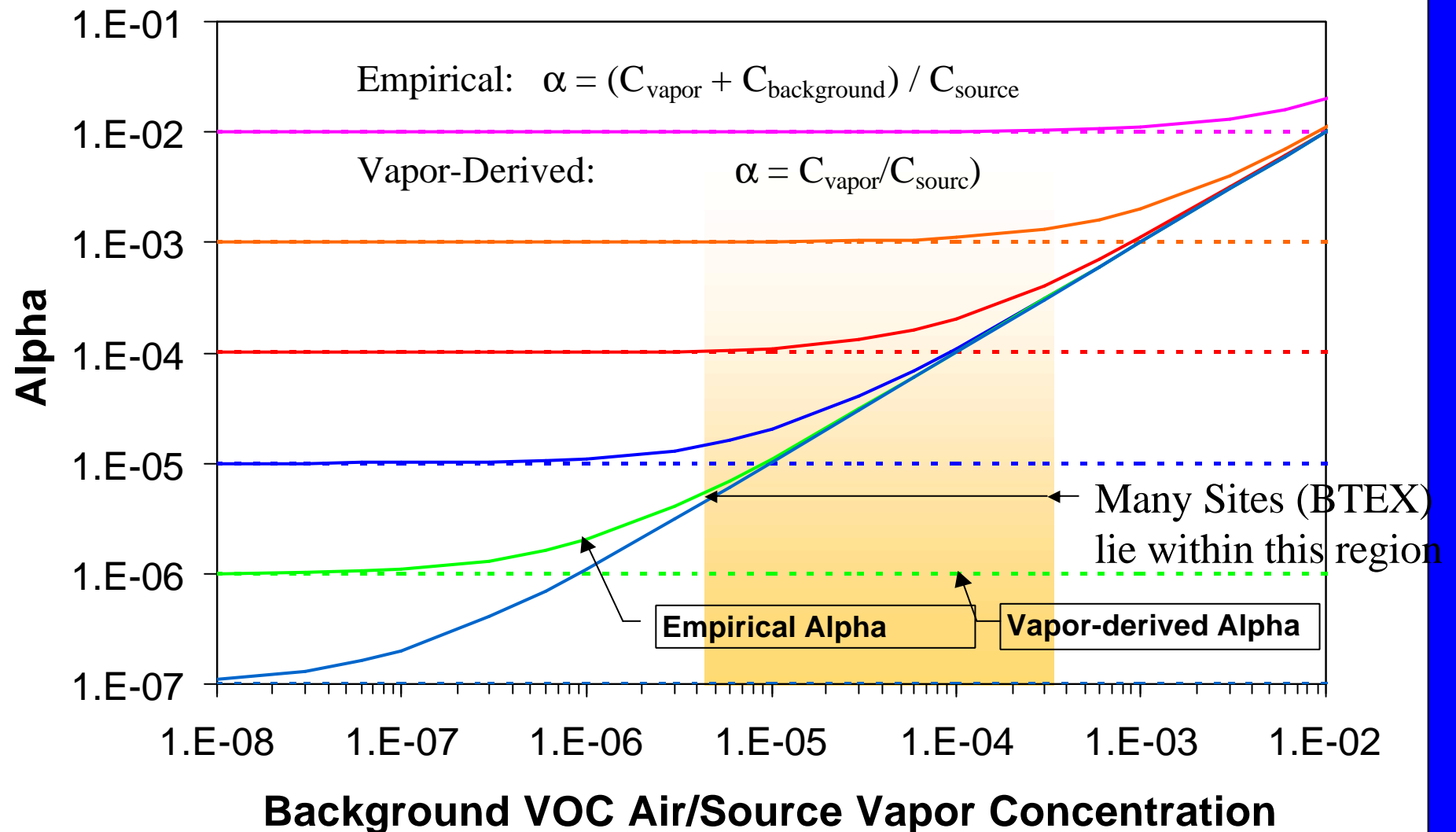
Example Pathway Analysis



Example Pathway Analysis (cont.)

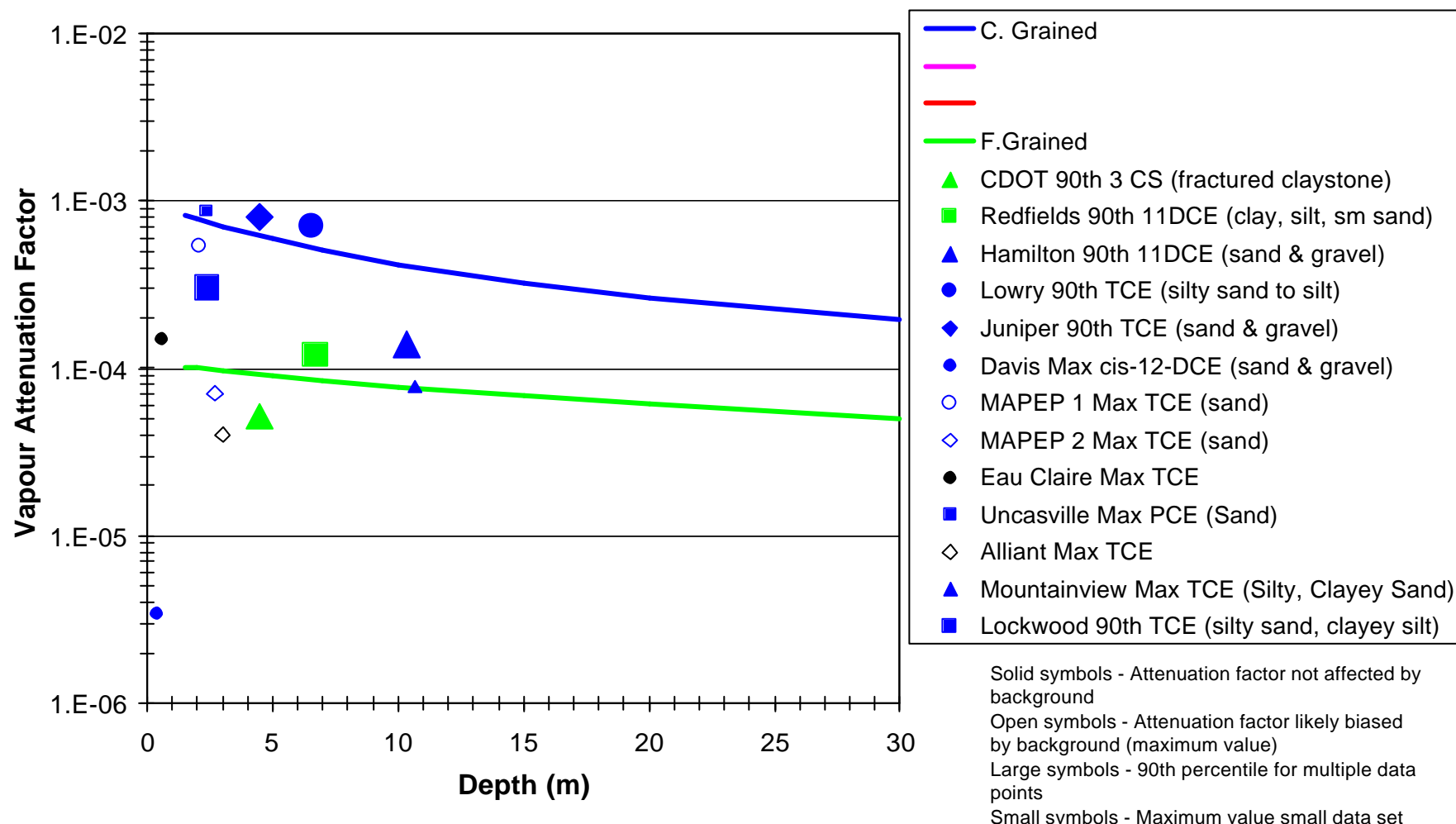


Influence Background VOC Concentration on Attenuation Factor



Groundwater-to-Indoor Air

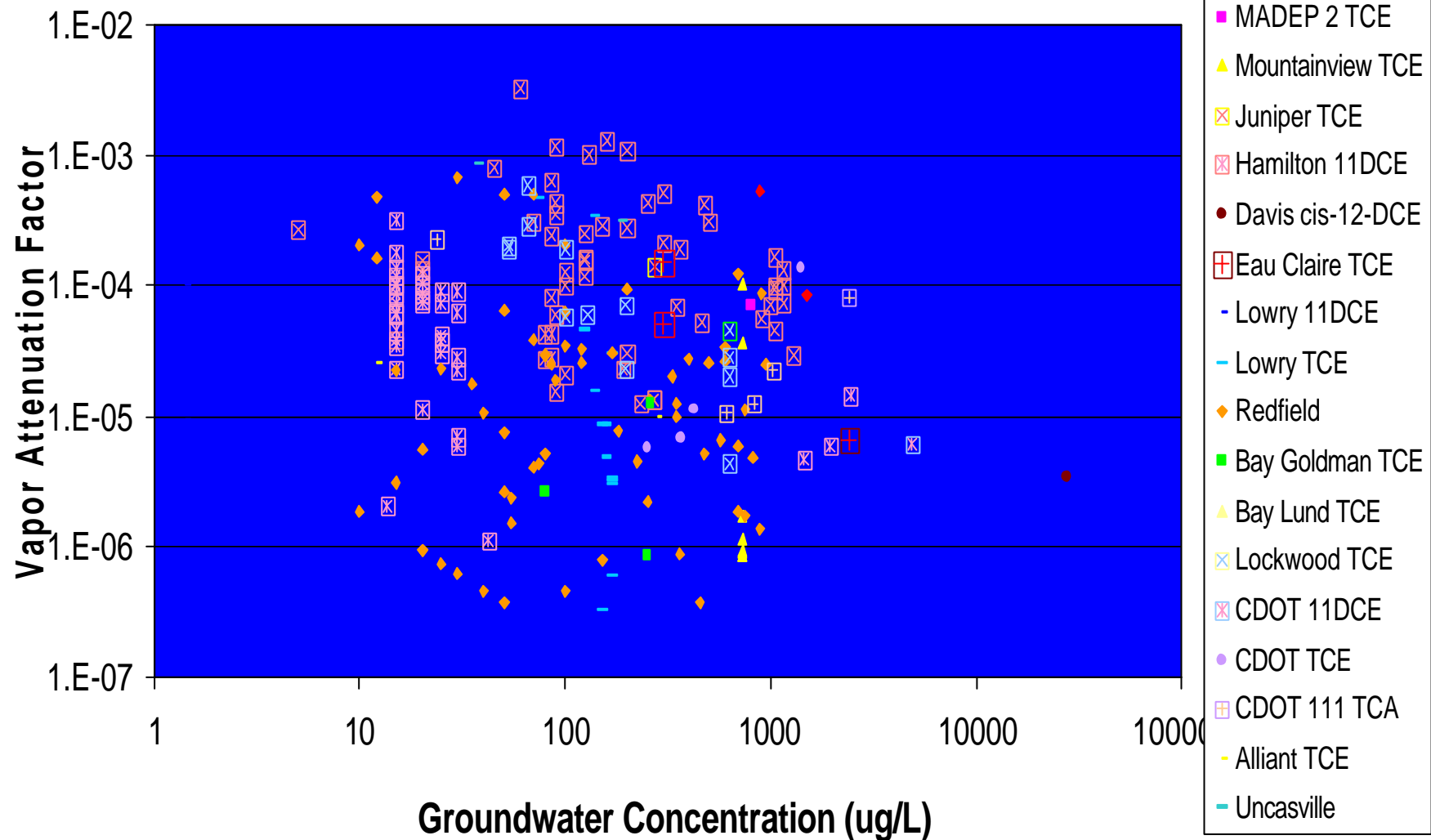
Chlorinated Solvents - Residential (HC Study)



Soil vapour concentrations predicted using Henry's Law Constant

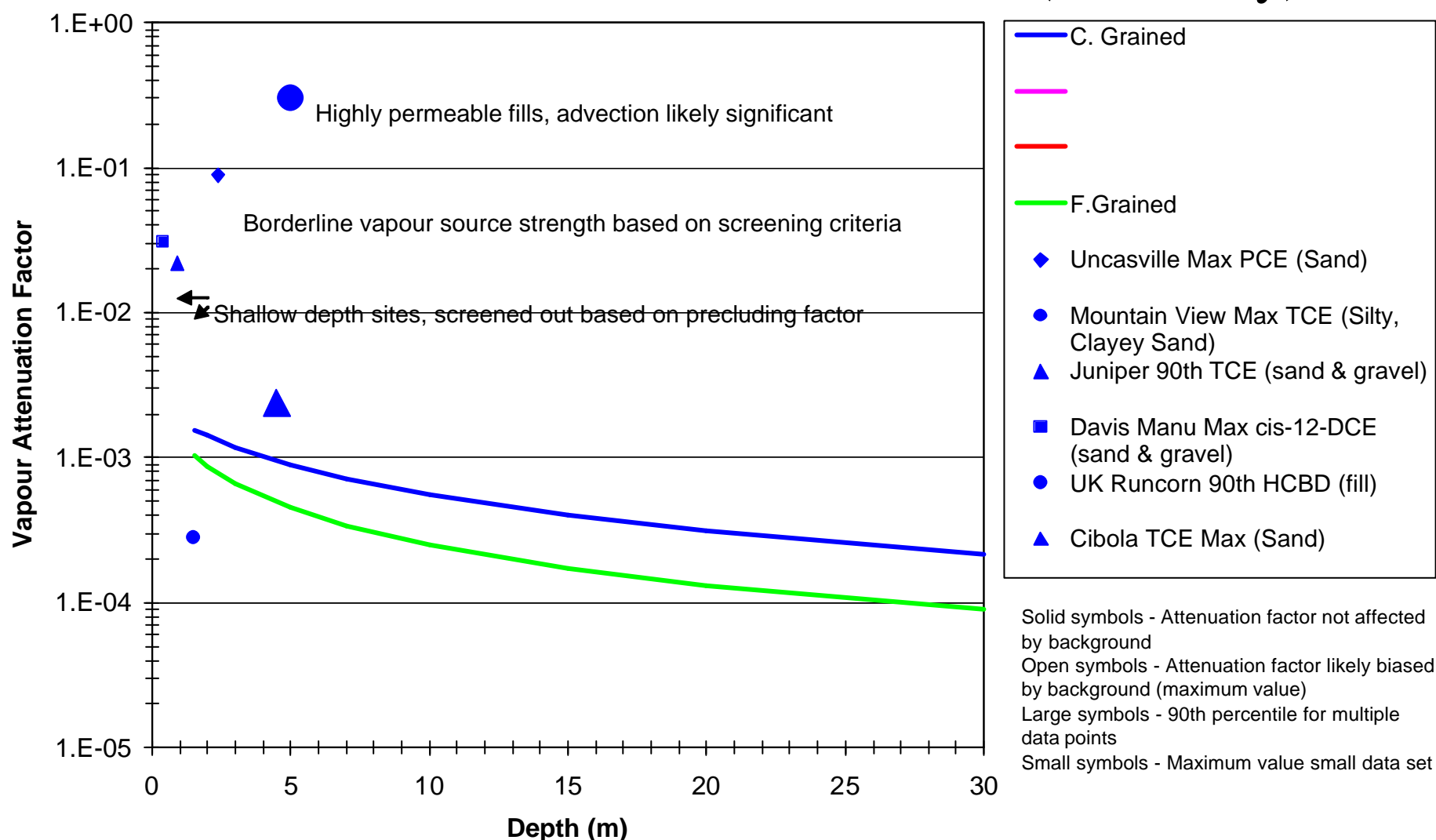
Groundwater-to-Indoor Air

Chlorinated Solvents - Residential (HC Study)



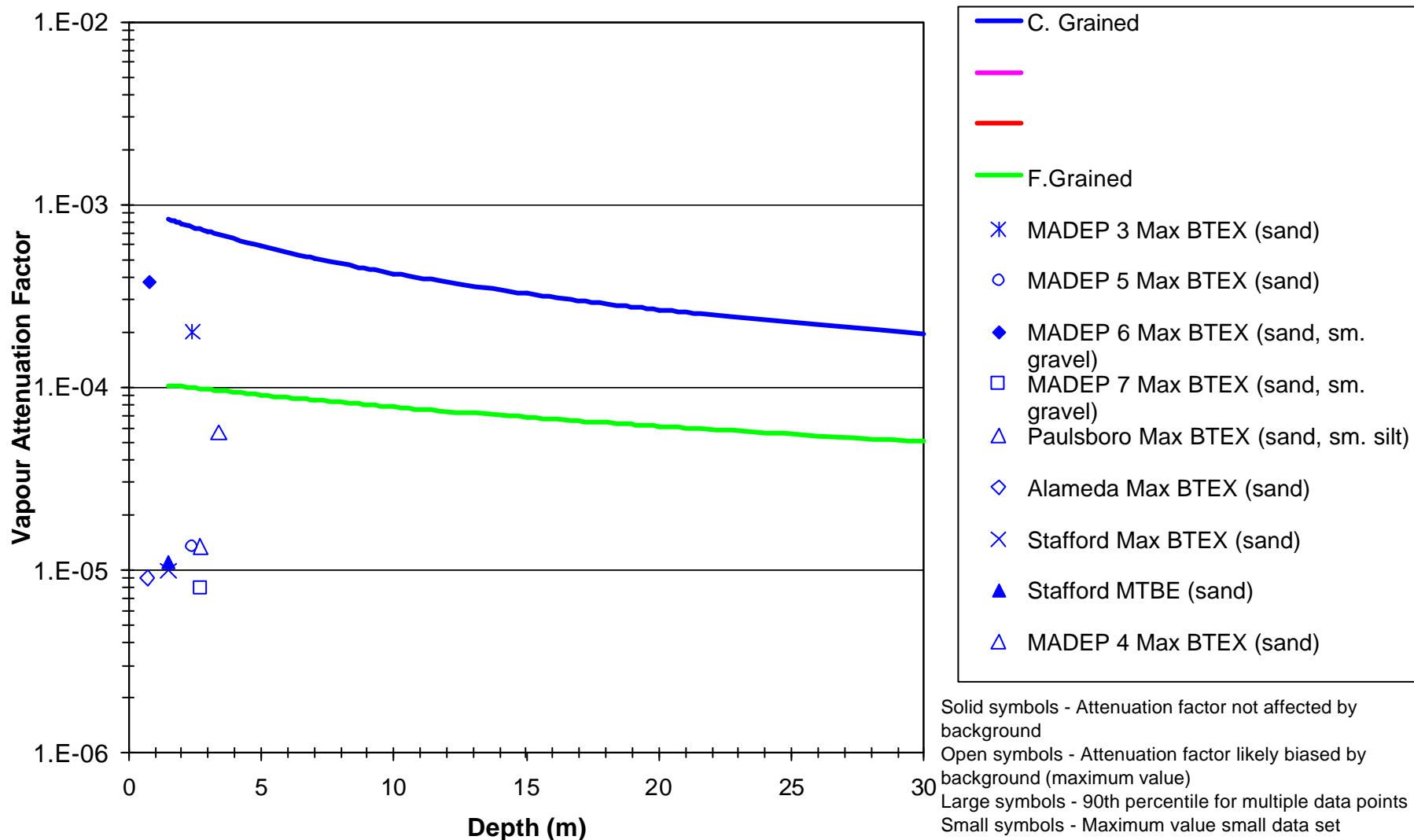
Soil Vapour-to-Indoor Air

Chlorinated Solvents - Residential (HC Study)



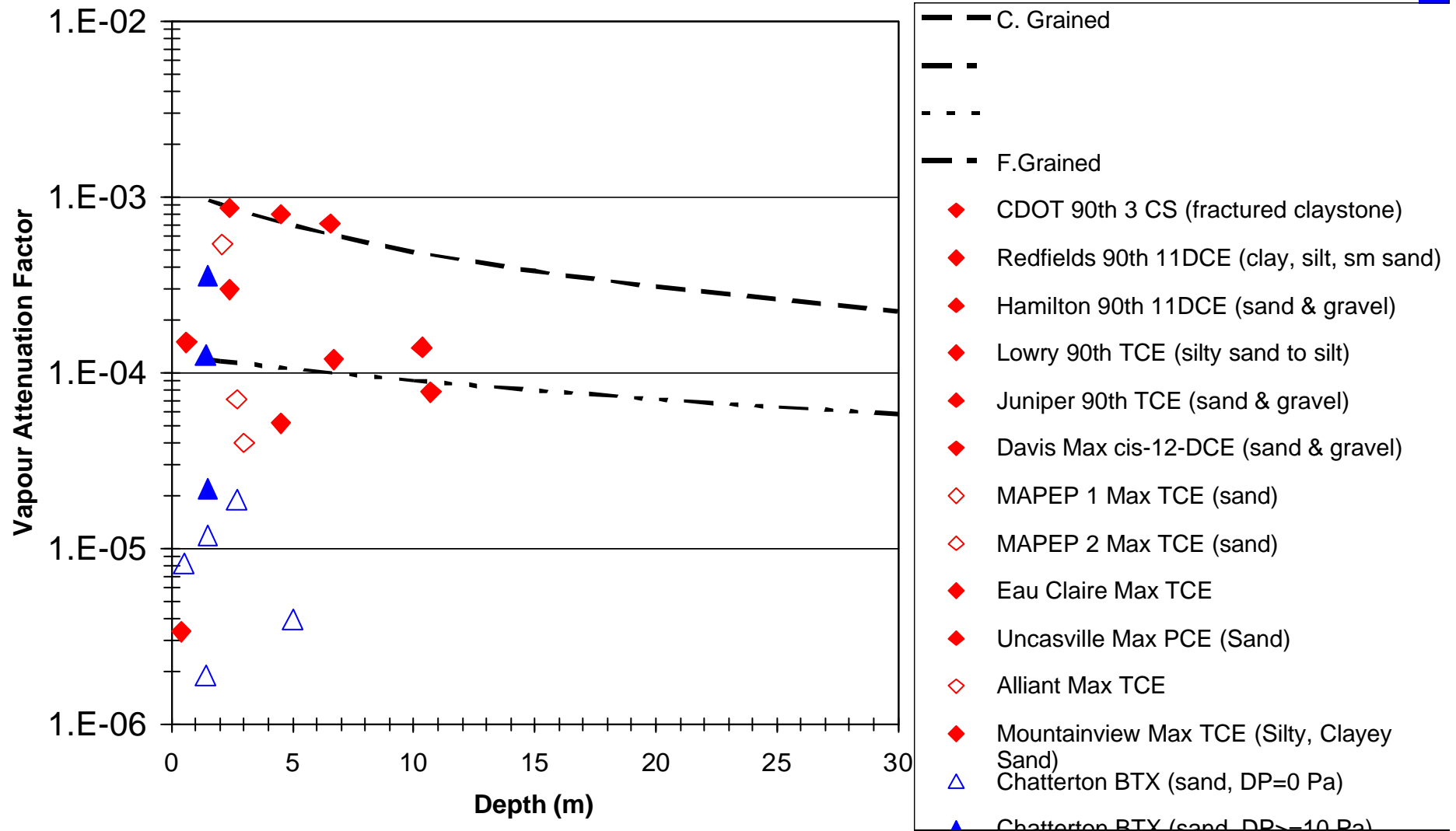
Groundwater -to-Indoor Air

Petroleum Hydrocarbons - Residential (HC Study)



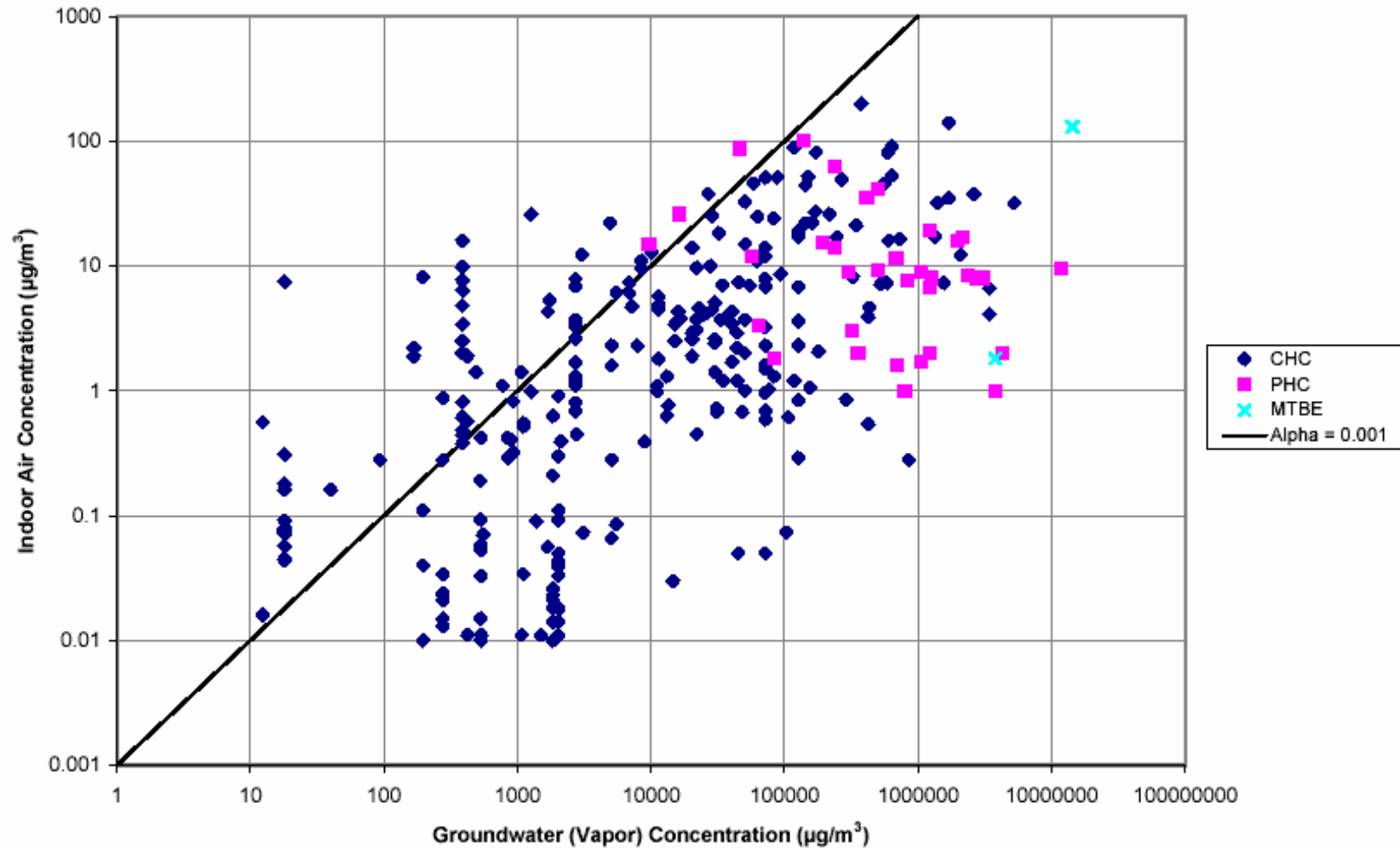
Groundwater -to-Indoor Air

All Data - Residential (HC Study)

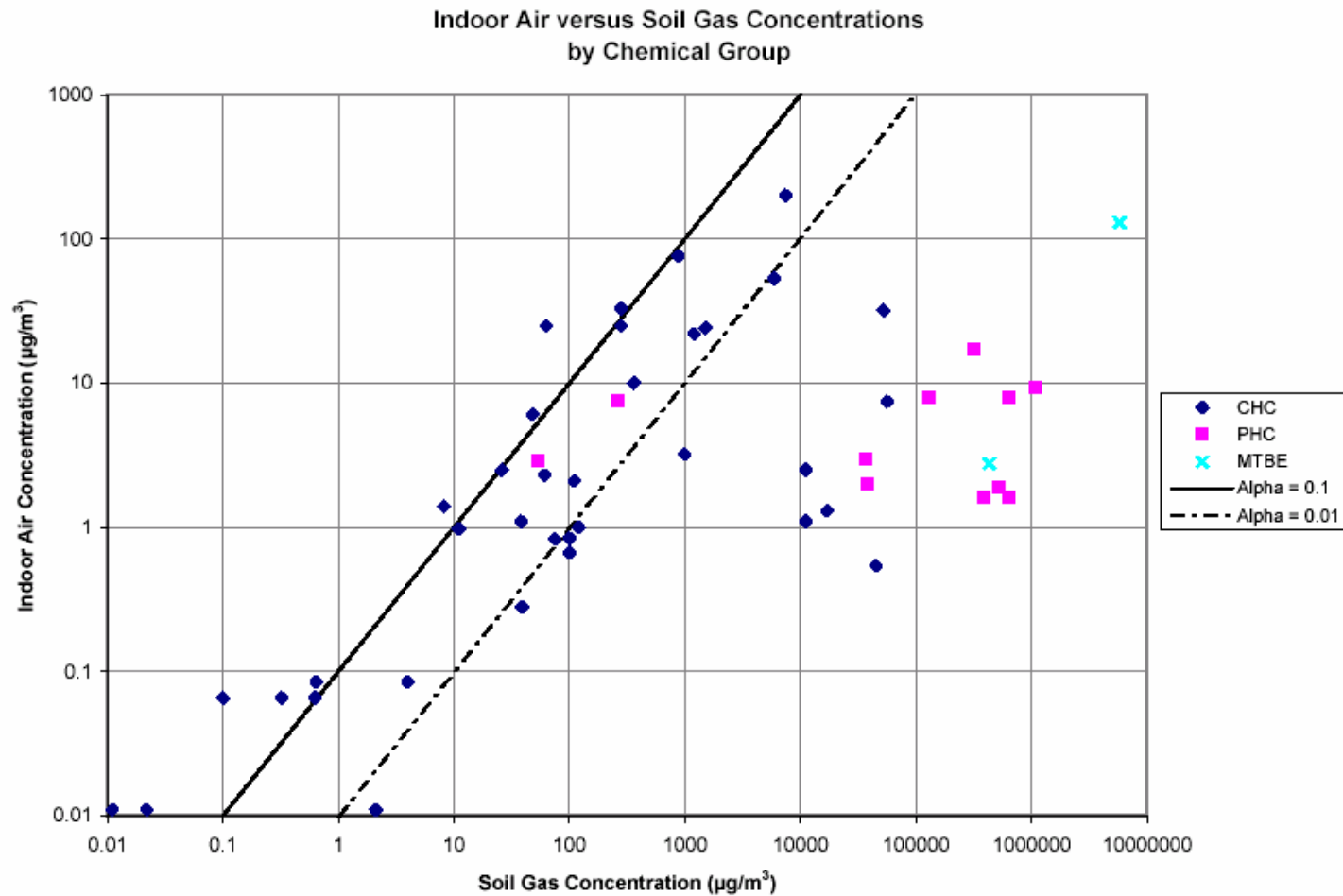


USEPA IAVI Database

Indoor Air versus Groundwater (Vapor) Concentrations
by Chemical Group

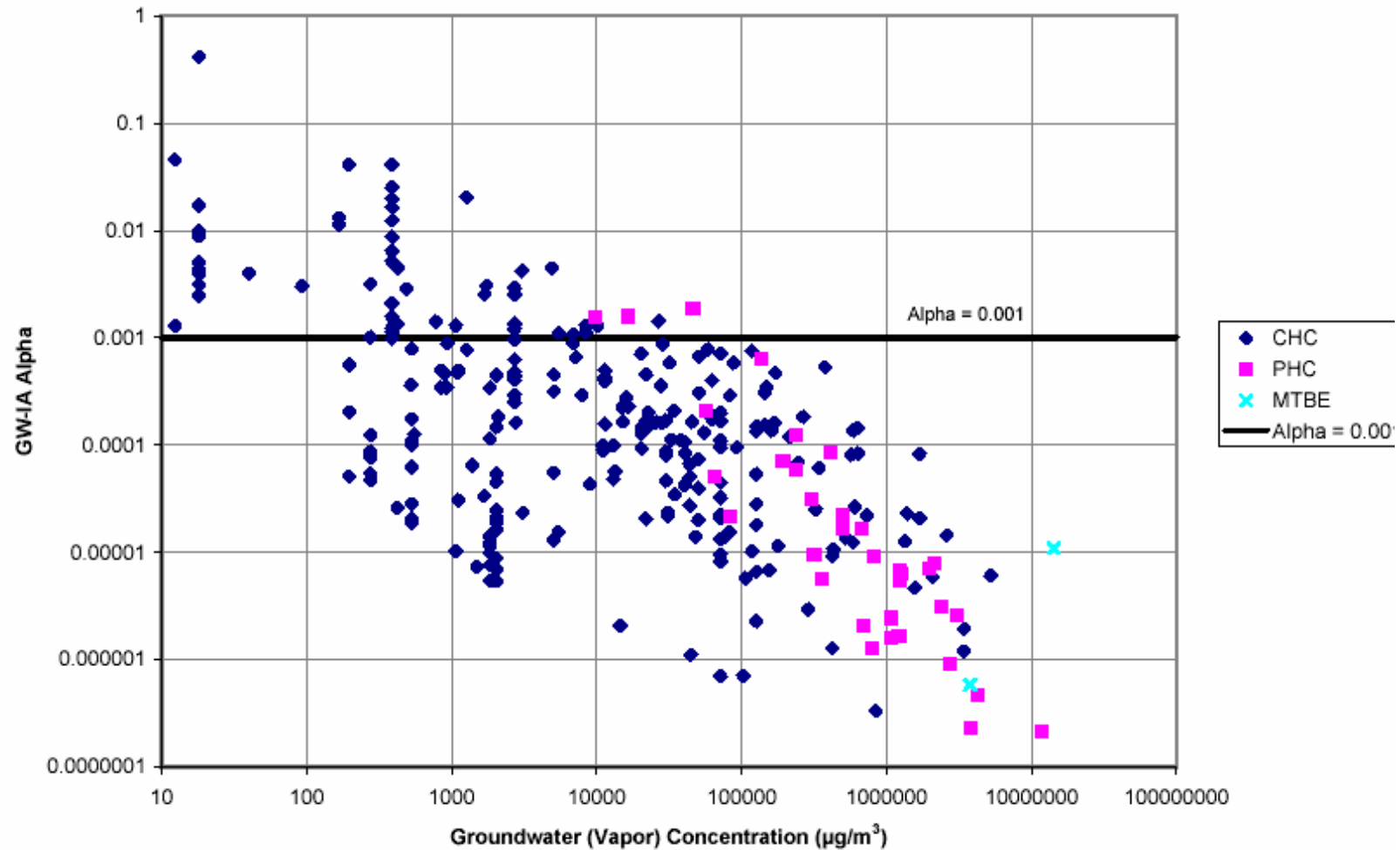


USEPA IAVI Database

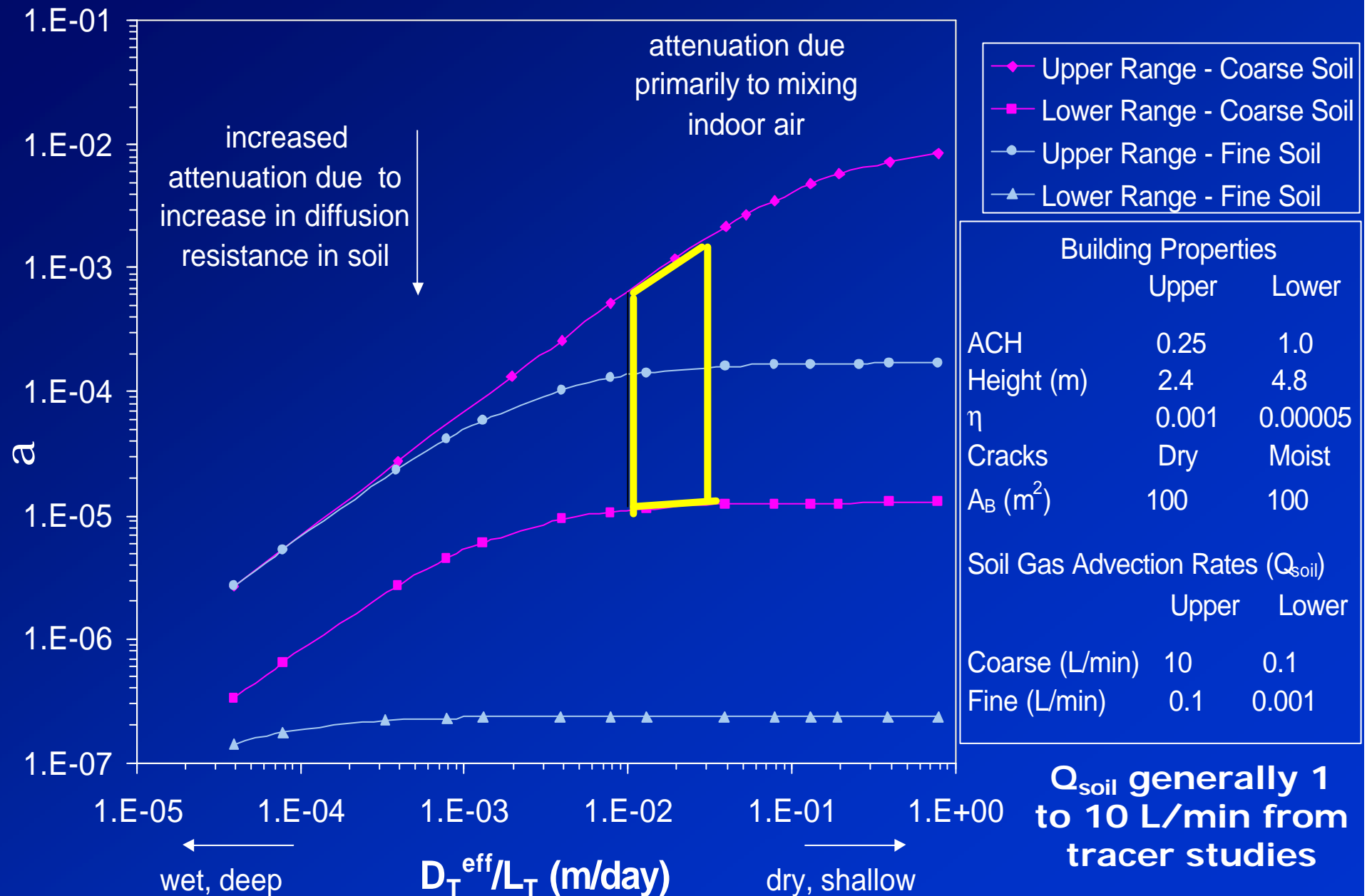


USEPA IAVI Database

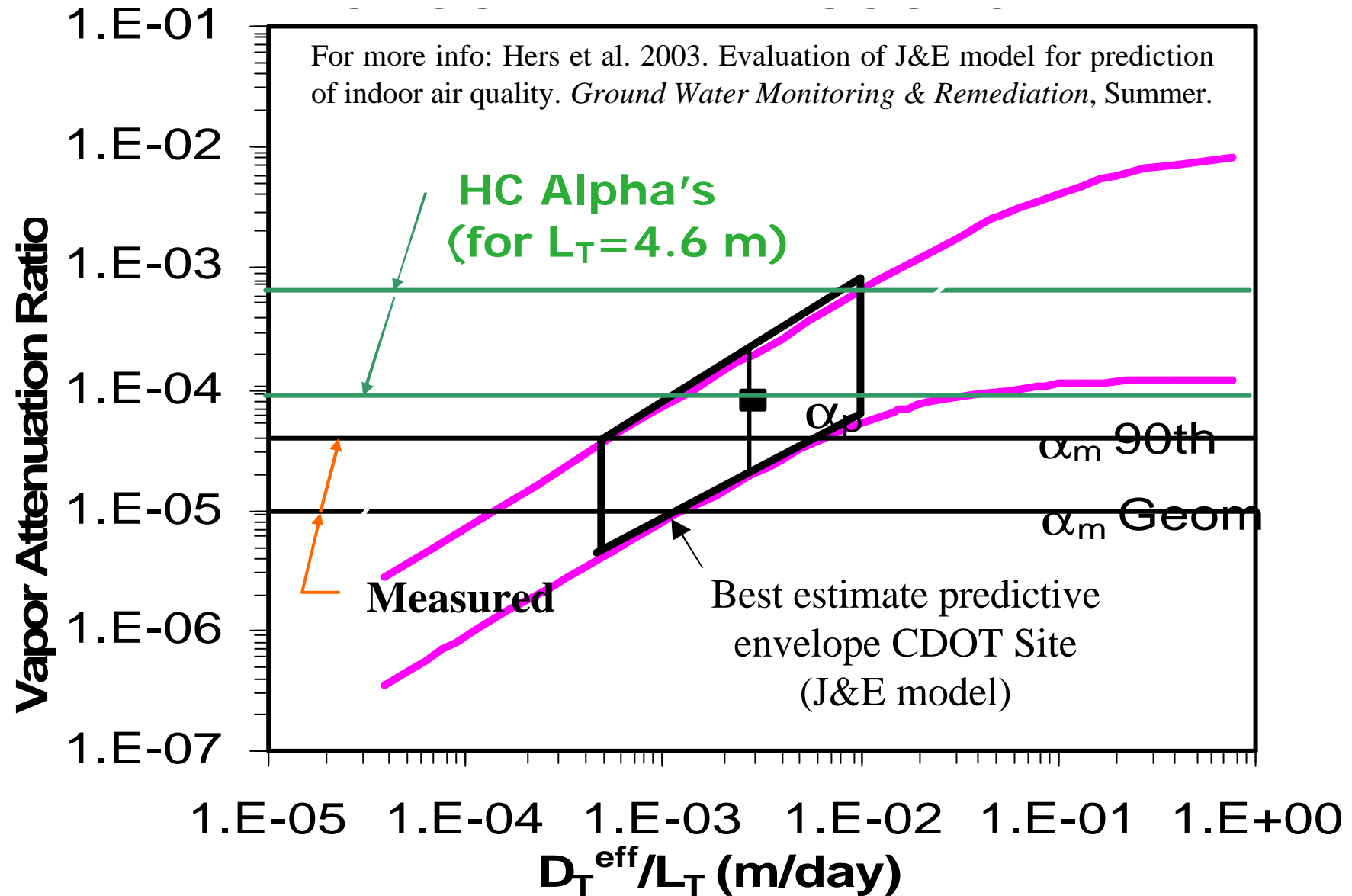
Groundwater-to-Indoor-Air Attenuation Factors



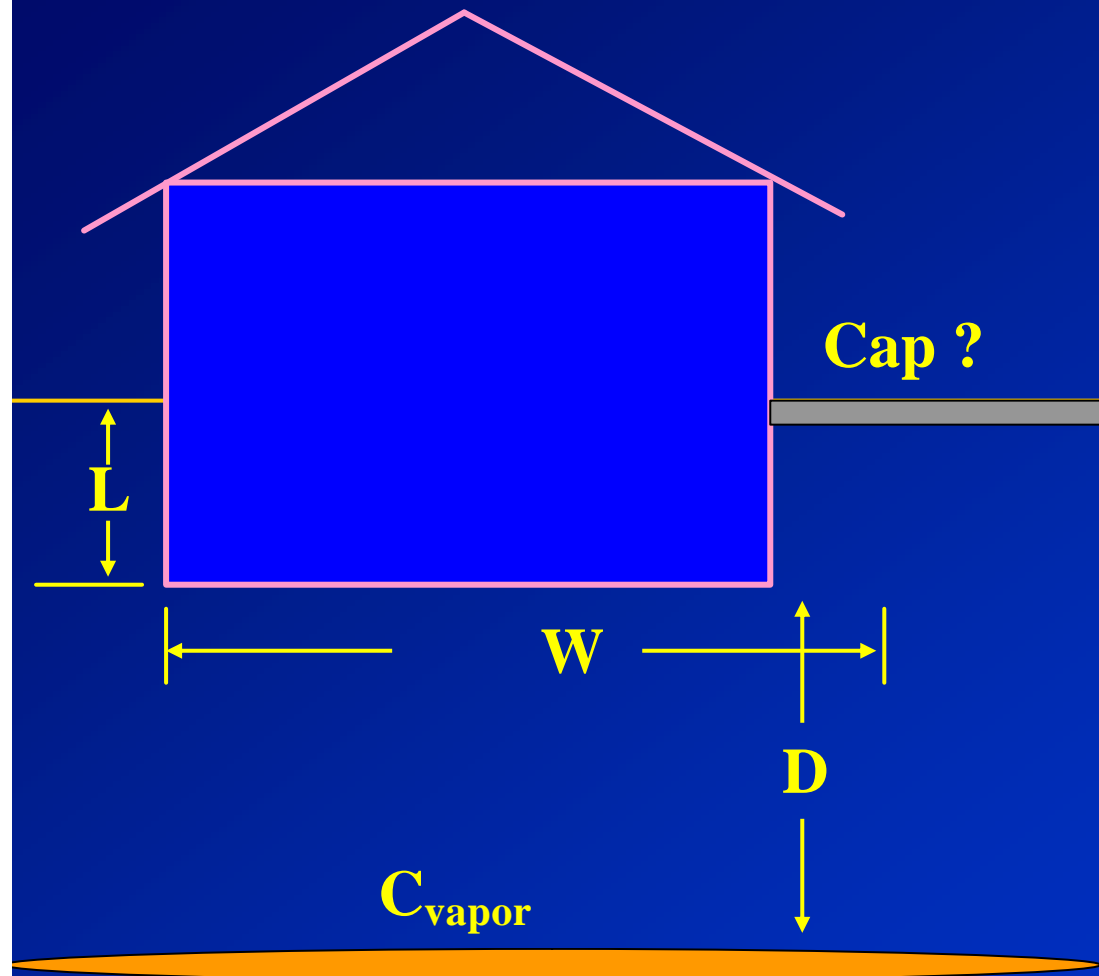
Validation J&E Model



CDOT HDQ Site, Colorado

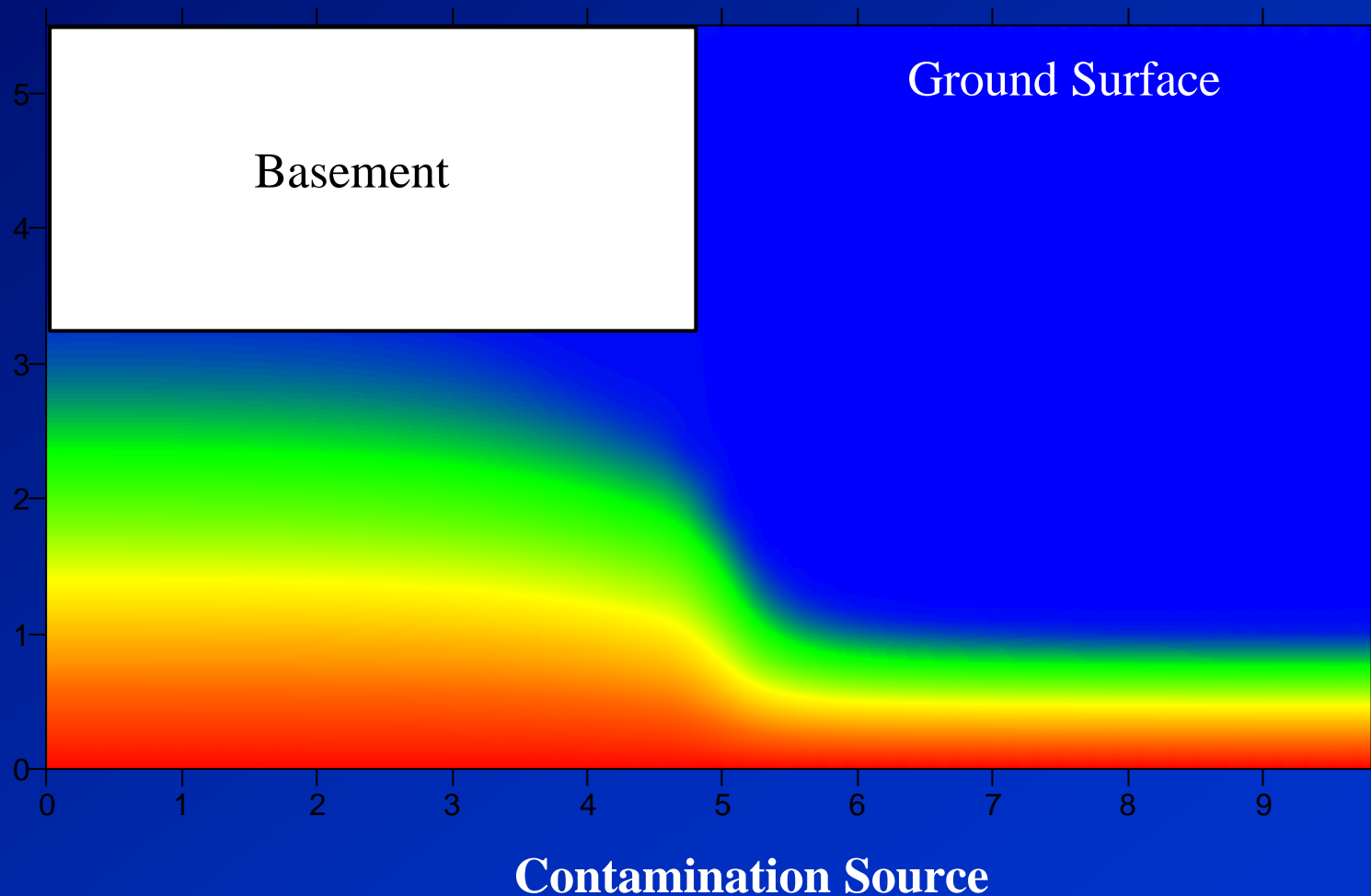


Biodegradation Adjustment (BTEX)

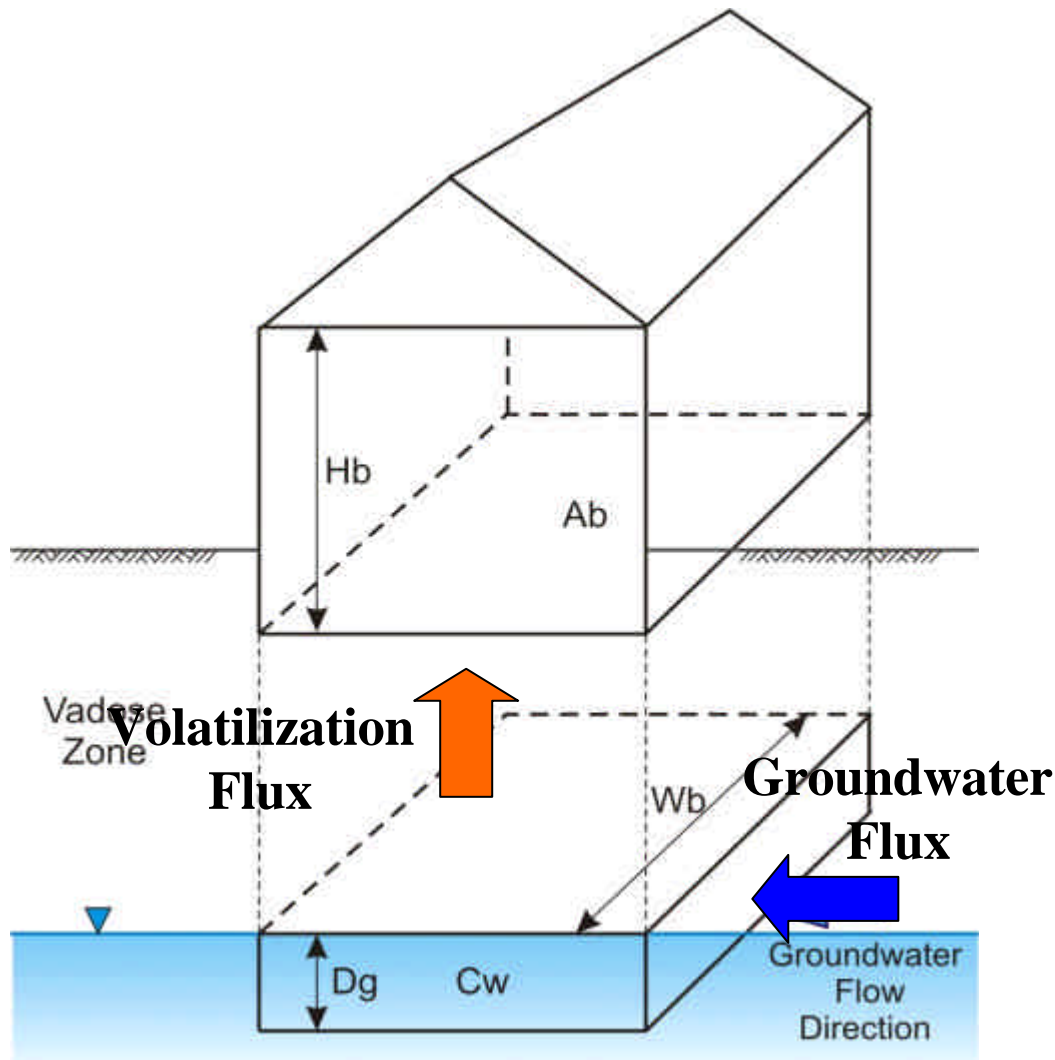


- Key biodegradation potential is O_2 transport below building
- Biodegradation potential affected by $D, L, W, C_{\text{vapor}}$, soil properties, capping effect
- Modeling study was conducted to evaluate above parameters for gasoline LNAPL source
- Guidance Criteria: $D > 4 \text{ m}$, no significant capping effect

Numerical Model Benzene Vapour Concentrations O₂-Limited Biodegradation



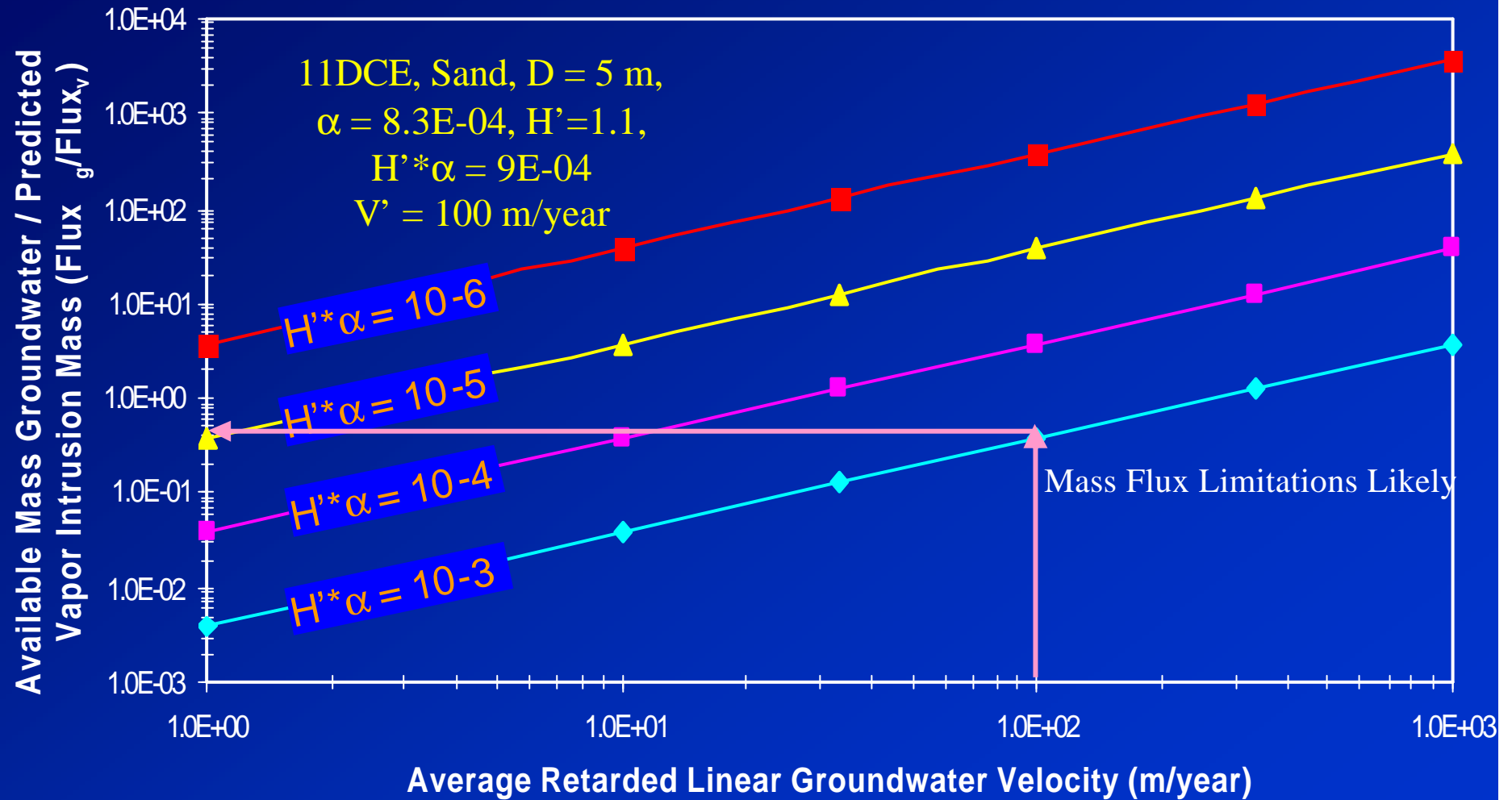
Groundwater Mass Flux Adjustment (Conceptual Model)



If Volatilization Mass Flux
(based on assumed α) $>$
Available Groundwater
Mass Flux, then Adjust Air
Concentration (α)

Relevant for more volatile
chemicals (vinyl chloride,
1,1 DCE) dimensionless
Henry's Law Constants > 1

Groundwater Mass Flux Check (Analytical Model)



Conclusions

- Sound framework for vapour pathway essential
- Health Canada alpha charts incorporate updated inputs based on recent science (different than CCME)
- Empirical validation models important part of process
- Wide variation in empirical alpha, for chlorinated solvents α ranged between $\sim 10^{-3}$ to less than 10^{-6} , for petroleum hydrocarbons α ranged between $\sim 10^{-4}$ and less than 10^{-6}
- 90th/Max measured alpha's for chlorinated solvent sites similar to or less than HC alpha's suggesting HC alpha's are reasonably protective, 90th/Max alpha's for petroleum sites about one order-of-magnitude less
- Adjustments for biodegradation, building height and mass flux important part of guidance